# TAUT WIRE AND SUN AZIMUTH TRAVERSE COMPUTATION 

by<br>G.L. ANDERSON, Lieutenant, U.S. Coast and Geodetic Survey. (Extract from Field Engineers Bulletin, No 11, Washington, December 1937).

The hydrographic surveys executed by the ship Hydrographer during the 1936 field season were in an area in which it was necessary to use surveying buoys for the major part of the control. Lines of buoys were established normal to the shore line from the limit of visibility of shore signals out to the 11 fathom curve, a distance of about twenty miles. The buoys at the inshore end of each line were located by sextant angles to three or more shore signals and their positions were determined graphically on aluminum sheets on a scale of $1: 40,000$. Closed traverse loops were formed by two adjacent lines of buoys and the connection at the outer ends. The corrected taut-wire distances and sun-azimuths between adjacent buoys were computed in a plane traverse to give the positions of the buoys in these loops. All except the outer two lines of buoys are used in the computations of two traverse loops, each line of buoys being used with the adjacent line on each side to form a traverse loop. The final positions of these buoys are the mean values obtained from the two traverse loops.

Plate I, Control for Hydrographic Surveys, shows the relative positions and the method of location of all buoys used during the season.

The computation and adjustment of two adjacent traverses are given in detail. In the form, Computation of Traverse, in columns No. 2 and 3 are entered the corrected sun azimuths and taut-wire distances between adjacent buoys. The sines and cosines of the sun azimuths are entered in columns No. 4 and 5. The latitude differences and departures in columns No. 6, 8, 10 and 12 are obtained by multiplying the taut-wire distances by the sines and cosines of the sun azimuths. The loop closures are determined by taking the difference between the totals of the north and south columns for latitude and the like difference of the east and west columns for longitude. These are then compared with the differences between the geographic positions of the two fixed inshore buoys as scaled from the 1:40,000 scale aluminum sheets. To the differences of longitude it is necessary to apply a correction for the convergence of meridians before the loop closures can be determined. This correction is obtained by multiplying the difference between the values of one minute of longitude at the north end and at the south end of the loop by the longitude difference between the two inshore fixed buoys. After the latitude and longitude closures are determined, the loop adjustment corrections are applicd to the latitude differences and departures as entered in columns No. 7, 9, 11 and 13. The corrected differences of latitude and longitude in meters are entered in columns 14 and 17. These corrected differences of latitude and longitude are then applied to the geographic position of the fixed buoy and the adjusted latitudes in minutes and meters are entered in columns 15 and 16 , and the adjusted longitudes in columns 18 and 19.

The final positions of the buoys in the line PIE-UKE are obtained by taking the means of the positions from the two traverses of which the line of buoys forms a part.

It is believed that the above described method of obtaining buoy positions is superior to other methods for similar areas. For the data available this method is believed to give more accurate positions than any graphic method and the resulting positions are obtained more quickly. The motion and vibration of the ship at sea make accurate location by graphical means very difficult whereas they do not interfere with computations.

At the beginning of the season graphic methods were used to locate the control buoys. A projection, scale $1: 80,000$, had been constructed on an aluminum sheet and this scale was necessary in order to include sufficient area of the working ground. The positions scaled from this sheet were to be used in hydrographic surveys, scale $1: 40,000$. Since the enlargement of the scale of a control survey is extremely undesirable, other possible methods were considered. An excessive number of aluminum sheets would have been required to cover the area on a scale of $1: 40,000$. The method finally adopted and which is described herein requires a series of aluminum sheets, scale 1:40,000, which include the shore control and the buoys along the shore at the inshore end of the traverses; and an offshore aluminum sheet at the scale of the R.A.R. survey for the graphic location of the offshore R.A.R. buoys.

## COMPUTATION OF TRAVERSE <br> PIE to BIT


*LOOP closure adJustuent

In the Computation of Traverse the Monroe computing machine was used to advantage. The taut-wire distance was multiplied on the machine by the natural sine or cosine to obtain respectively the difference in latitude and departure. At first a table was computed from which the difference in latitude and departure were taken directly, but the use of the table was abandoned in favor of direct computation when the extent of the necessary table was learned. The computing machine was used also to obtain the final position in minutes and meters of latitude and longitude by applying the corrected differences to the values for the preceding buoy in the traverse.


## adjusted positions of buoys on line pie-Uke

| LATITUDE |  |  |  | LONGTTUDE |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trav. m. | Trav. 2 m. | Mean <br> m. |  | Trav. 1 m. | Trav. 2 m. | $\begin{gathered} \text { Mean } \\ \text { m. } \end{gathered}$ |
| 645 | 652 | 648 | $90^{\circ} 22^{\prime}$ | 748 | 747 | 748 |
| 156 | 169 | 163 | 9022 | 712 | 710 | 711 |
| 1312 | 1332 | 1322 | 9022 | 401 | 398 | 400 |
| 409 | 435 | 422 | 9022 | 253 | 249 | 250 |
| 1072 | 1105 | 1088 | 9022 | 97 | 92 | 94 |
| 75 | 114 | 95 | 9021 | 1575 | 1569 | 1572 |
| 1031 | 1077 | 1054 | 9021 | 1414 | 1406 | 1410 |
| 103 | 155 | 129 | 9021 | 1287 | 1277 | 1282 |

The computed positions of the buoys at the offshore ends of the traverses were plotted on an aluminum sheet, scale $1: 80,000$, and from them the positions of offshore R.A.R. buoys were obtained graphically on the sheet.

The approximate lengths and closing errors of the computed traverses are as follows :

| KEY - TON | 40 miles, Lat. | -115 m. | Long. | -48 m. |
| :--- | :--- | :--- | :--- | :--- |
| TON - GEM | 39 miles, Lat. | -45 m. | Long. | -84 m. |
| GEM - VIM | 41 miles, Lat. | +10 m. | Long. | +29 m. |
| VIM - BIT | 42 miles, Lat. | -61 m. | Long. | -128 m. |
| BTT - PIE | 47 miles, Lat. | +52 m. | Long. | -57 m. |
| PIE - HIP | 43 miles, Lat. | -84 m. | Long. | -42 m. |
| JET - TAB | 22 miles, Lat. | +7 m. | Long. | +11 m |
| PAR - DAY | 30 miles, Lat. | +11 m. | Long. | -135 m. |

Average closing error per mile, Lat. $1.2 \mathrm{~m} .$, Long. 1.8 m .

