Radon soil gas in the Halifax Regional Municipality, Nova Scotia, Canada

Kelsey E. O'Brien^{1*}, Terry A. Goodwin² and David Risk³

Dalhousie University, Halifax, Nova Scotia B3H 4R2, Canada
 Nova Scotia Department of Natural Resources, Mineral Resources Branch, Halifax, Nova Scotia B3J 2T9, Canada
 St. Francis Xavier University, Antigonish, Nova Scotia B2G 2W5, Canada
 *Corresponding author <kelsey.obrien@dal.ca>

Date received: 31 August 2010 ¶ Date accepted 18 June 2011

ABSTRACT

Naturally occurring radon²²² is found in measurable quantities in soil gas across Nova Scotia. Next to smoking, exposure to radon is the leading cause of lung cancer. This study identifies relationships between the permeability and composition of the soil, and the geology of the respective bedrock types within Halifax Regional Municipality (HRM). Over 280 radon soil gas samples from 60 sites were collected and analyzed using protocols developed for the North American Soil Geochemical Landscapes Project. This study focused on soil developed on glacial till over three major bedrock types: the Cambrian-Ordovician Goldenville and Halifax groups, and Devonian granite of South Mountain Batholith. All samples contained radon soil gas. Fine-grained leucomonzogranite samples returned the highest mean radon concentration of 51.0 kBq m⁻³, followed by coarse-grained leucomonzogranite (50.2 kBq m⁻³), monzogranite (44.3 kBq m⁻³), slate (36.1 kBq m⁻³), and metasandstone and Lawrencetown till, respectively 22.5 kBq m⁻³ and 19.4 kBq m⁻³. Analysis of the permeability readings was done in four major till types in HRM: granite $(3.27 \times 10^{-12} \text{ m}^2)$, metasandstone $(5.84 \times 10^{-12} \text{ m}^2)$ 10^{-12} m²), and slate facies $(5.20 \times 10^{-12} \text{ m}^2)$ of the Beaver River Till (BRT), and Lawrencetown Till $(1.18 \times 10^{-12} \text{ m}^2)$. The soil radon potential index (SRP), which is used to correlate soil gas and permeability readings with indoor radon potential, was applied to data collected for the HRM study area, where over 40% of Nova Scotia's population resides. The SRP index results show the granite facies of BRT returning the highest mean value of 34.5, followed by the slate facies (27.2) and metasandstone facies (15.1) of the BRT, and Lawrencetown Till (9.1). 1D soil-gas modeling demonstrated that it is unlikely that bedrock radon transport from depth alone can contribute to the concentrations measured at 60 cm; the overlying tills must also be producing radon.

RÉSUMÉ

Du radon (Rn 222) à l'état naturel et en quantités mesurables est observé dans les gaz souterrains partout en Nouvelle-Écosse. Après le tabac, l'exposition au radon est la deuxième cause de cancer du poumon. Cette étude examine les liens entre la perméabilité et la composition du sol, ainsi que la géologie des divers types de substratum rocheux présents dans la Municipalité régionale d'Halifax (MRH). Plus de 280 échantillons de gaz souterrain de radon provenant de 60 endroits ont été recueillis et analysés selon des protocoles élaborés dans le cadre du projet des paysages géochimiques des sols d'Amérique du Nord. Cette étude a surtout porté sur le sol formé dans le till glaciaire de trois principaux genres de substratum rocheux: les groupes de Goldenville et d'Halifax du Cambrien-Ordovicien, et le granite du batholithe South Mountain, du Dévonien. Tous les échantillons contenaient du gaz de radon souterrain. Les échantillons de leucomonzogranite à grains fins ont produit la plus haute teneur moyenne de radon, soit 51,0 kBq m⁻³, suivis en cela par les échantillons à grains grossiers de leucomonzogranite (50,2 kBq m⁻³), de monzogranite (44,3 kBq m⁻³), d'ardoise (36,1 kBq m⁻³), et de métagrès et du till de Lawrencetown, dont les teneurs respectives étaient de 22,5 kBq m⁻³ et de 19,4 kBq m⁻³. Les valeurs de perméabilité ont été analysées dans les quatre principaux genres de till présents dans la MRH: le granite $(3,27 \times 10^{-12} \text{ m}^2)$, le métagrès $(5,84 \times 10^{-12} \text{ m}^2)$ et le faciès d'ardoise $(5,20 \times 10^{-12} \text{ m}^2)$ du till de la rivière Beaver (BRT), et le till de Lawrencetown (1,18 × 10⁻¹² m²). L'indice de teneur possible de radon dans le sol (SRP) sert à établir une corrélation entre le gaz souterrain et des valeurs de perméabilité, susceptibles de donner lieu à une présence de radon dans l'air intérieur. Cet indice a été utilisé pour l'analyse des données provenant de la zone d'étude de la MRH, où 40 p. 100 de la population de la Nouvelle-Écosse habite. L'analyse à l'aide de l'indice SRP a établi que le faciès de granite du till de la rivière Beaver présente la teneur moyenne la plus élevée, soit 34,5, suivi en cela par les faciès d'ardoise (27,2) et de métagrès (15,1) de ce till, puis par le till de Lawrencetown (9,1). La modélisation dimensionnelle des gaz souterrains a déterminé qu'il est peu vraisemblable que la seule migration du radon du substratum rocheux en profondeur serait à l'origine de teneurs lues à 60 cm de profondeur; les tills sus-jacents doivent également produire du radon.

[Traduit par la redaction]

INTRODUCTION

Radon²²² is a naturally occurring, invisible radioactive gas that is present in measurable quantities in all till and soil types in Nova Scotia (Goodwin et al. 2008). It is a daughter product of uranium²³⁸, and decays to polonium²¹⁸, releasing a potentially harmful alpha particle. High radon soil gas values are typically associated with granite and slate (Je 1998). Radon is a human health risk, as long-term exposure to high radon concentrations through inhalation is the second leading cause of lung cancer next to smoking (World Health Organization 2005). A radon potential map of Canada identified Nova Scotia and Winnipeg as the highest risk provinces (Chen 2009).

Previous radon soil gas (where soil refers to glacial till) testing completed in Nova Scotia (Goodwin et al. 2008) indicated measurable quantities of radon in all 72 sites across the province (sampling density of 1 sample ever 800 km²). Radon in Halifax Regional Municipality (HRM) has been previously identified as a potential health risk (Lewis et al. 1998; White et al. 2008). As over 40% of the provinces population resides in HRM, significant study has been focused on identifying and managing this potential risk to human health.

In order to better understand the radon soil gas distribution and risk across HRM, this study investigates the controls on radon soil gas in the major till units, and attempts to answer the following two questions: what are the major factors controlling the expression of radon, and how can soil gas modeling be used to predict a bedrock production value? The spatial distribution of radon with respect to bedrock and till units is mapped, and gas transport modeling is used to determine important controls influencing the high radon concentration prevalent in HRM tills. The controls on the concentration of radon gas measured in the till have not yet been well established. The previous radon study in HRM did not incorporate a model of radon gas transport from depth (Goodwin et al. 2009b). The present study incorporates soil gas modeling to understand the production of radon at depth and the diffusivity of the overlying tills.

BACKGROUND

A limited study focused on radon concentrations in surficial geological units of Halifax Regional Municipality (Goodwin et al. 2009b). Within HRM, 20 sample sites from four specific glacial till types were sampled. The granite facies of the Beaver River Till returned the highest mean radon concentration of $54.1\,\mathrm{kBq}\,\mathrm{m}^{-3}$, followed by the Lawrencetown Till with $28.3\,\mathrm{kBq}\,\mathrm{m}^{-3}$, and the metasandstone and slate facies of the BRT with $26.2\,\mathrm{kBq}\,\mathrm{m}^{-3}$ and $25.4\,\mathrm{kBq}\,\mathrm{m}^{-3}$, respectively.

Permeability plays an important role in the expression of soil gas (in this case, the soil is till), as it is a proxy for the diffusion of gas transport. Coarser soil tends to have higher permeability relative to clay rich soil (Freeze and Cherry 1979). The higher the permeability, the easier soil gas can pass through the pore

spaces and be detected. Soil gas transport is diffusive. Previous work (Ball $et\ al.$ 1999) showed that the production, consumption, and transport of CO₂ and N₂O were strongly influenced by changes in soil structural quality and water content associated with tillage and compaction. A primary soil quality component influencing the soil transport of a gas is the gas diffusivity. As diffusivity is linked to permeability, it is a key component in this study. The contribution of radon from the bedrock is also important.

The concentration of radon in soil gas and the permeability of the soil are two important factors that affect the movement of radon to the surface. The soil radon potential (SRP) index helps quantify the radon gas to soil permeability relationship. The higher the SRP value, the greater the potential for radon to migrate through the soil and enter a home to levels that exceed the guideline of 200 Bq m $^{-3}$ (Health Canada 2009). The SRP index has previously been used by Goodwin et al. (2009a, b), however a brief explanation is given here. The SRP index is defined (Neznal et al. 2004) as:

$$SRP = \frac{C - C_0}{-\log(P) + \log(P_0)}$$

Where C is the radon soil gas concentration for a field sample site in kBq m⁻³, and P is the soil permeability of the field site in m². C_0 and P_0 are set constants, respectively, 1 kBq m⁻³ and 1×10^{-10} m².

Previous SRP work has been completed for parts of southern Ontario (Chen et al. 2008) when the Ottawa-Sarnia transect was analyzed for the radon potential. Natural soil gas radon variability and background concentrations were determined at 32 sites between Ottawa and Sarnia. The measured soil gas radon concentrations varied significantly from 4 to 116 kBq m $^{-3}$. The SRP results ranged from 1 to 80 at the same sites; areas of high potential risk were identified (Chen 2009). Radon soil gas testing was done in southern Ontario previously (Je 1998). Natural background was found to be 3.7–7.4 kBq m $^{-3}$, with anomalies found near the extensively fractured black shales around the Greater Toronto Area (GTA). These anomalous concentrations peaked at 37 kBq m $^{-3}$.

The SRP index helps determine which till (and bedrock) types will have the highest potential for accumulation of indoor soil gas (and exceed the 200 Bq m⁻³ indoor guideline). Approximately 40% of the study area (Fig. 2) is covered with granite facies till, 10% with clay-rich Lawrencetown Till (mostly drumlinized), 25% with slate facies till, and 25% with metasandstone facies till (Stea and Fowler 1981). In this paper, the SRP values are calculated for each surficial unit to determine the relative ranking of the radon potential. In situ gamma ray spectrometry measurements are also collected at each site to determine the concentration of equivalent uranium (eU) (as well as equivalent thorium, and potassium). This uranium data may be used to further asses the radon potential, though it is important to note that eU is only a proxy of uranium (U), as it is measuring bismuth²¹⁴.

METHODS

For this study, all sample sites were located within Halifax Regional Municipality. A total of 200 measurements from 40 sites were collected and analyzed during the 2009 field season (and combined with the 20 sites from 2008) using protocols developed for the North American Soil Geochemical Landscapes Project (Friske *et al.*, 2010). A detailed methodology has been previously described (Goodwin 2008; Goodwin *et al.* 2008, 2009a, 2009b), but a brief summary is given below.

Field sites

Individual sample sites (Fig. 1) were chosen and subdivided based on the surficial geology (till) units. The sites were biased by the existing road network (for example, along Highway 103). Also, the 2009 samples were in natural undisturbed sites (sites from 2008 were taken in parks).

Radon equipment and sampling procedure

At each sample site, five hollow probes were hammered into the till to a depth of 60 cm. A spacer and thin rod were then used to punch out a tapered tip, creating a fixed head space. Soil permeability was determined for each probe, using the Radon-JOK portable permeability instrument. If, after 10 minutes, the instrument did not move (low permeability), that probe was assigned a value of 2.0×10^{-14} m² (Friske *et al.* 2010). Once the permeability readings were taken, 150 mL of soil gas was extracted from each probe. This gas was transferred into IK-250 sampling ionization chambers, held for approximately 15 minutes, after which radon concentrations were measured. The arithmetic mean of the five probes was calculated, and this value was assigned the concentration of the radon soil gas used for the site.

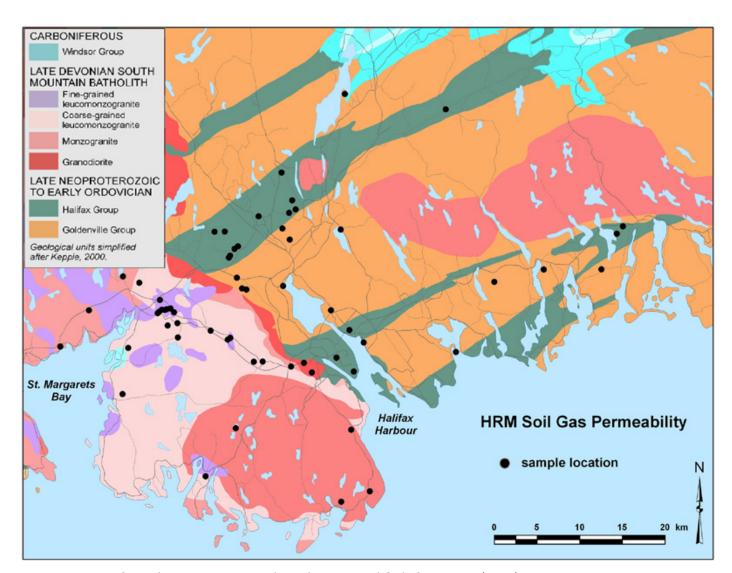


Fig. 1. Location of sample sites in HRM. Geological map is modified after Keppie (2000).

Table 1. Solved soil gas equations results.

| Diffusivity (m²/s) | Production (Bq/m³/s) | Concentration (0.6 m) |
|--------------------|----------------------|-----------------------|
| 4.00E-07 | 10 | 2.39E+04 |
| 4.00E-07 | 25 | 5.98E+04 |
| 3.00E-07 | 50 | 2.14E+04 |
| 3.00E-07 | 100 | 4.28E+04 |
| 3.00E-07 | 1000 | 1.31E+04 |

Soil gas modeling

In order to take an analytical look at the radon soil gas, the diffusivity equation (No. 2) (Nazaroff 1992) is used to help model the radon concentration with depth. The bulk distribution coefficient was modified (Penman 1940; Washington *et al.*

1994), resulting in equation 3. This now represents a time independent formula; the data collected in the field is also time independent. One of the major assumptions using this model is that till is not producing radon, and that it is being emitted from the bedrock only.

Soil gas transport is primarily diffusive; non-diffusive transport is typically a very near-surface phenomenon. Permeability is a measure of transport driven by pressure gradients imposed by wind, while diffusivity is a measure of molecular flow driven by concentration gradients, and has been measured recently with isotope signatures (Kayler *et al.* 2010). Therefore, for the soil gas modeling, diffusivity is used instead of permeability. It is a more common way of modeling the gas mobility, and can be correlated more easily with other soil gas model results.

If soil gas transport is diffusive, why is the permeability tested on site? There are two reasons for this; first, in the field it is much easier to measure permeability than it is to measure diffusivity (Risk *et al.* 2008). Secondly, permeability and dif-

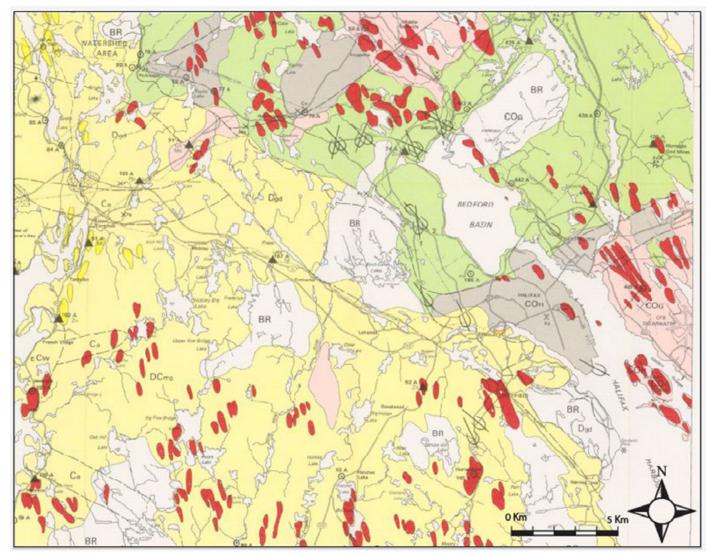


Fig. 2. Pleistocene geology and till geochemistry of part of the HRM area, modified after Stea and Fowler (1981). Legend: yellow = granite till; green = quartzite (metasandstone) till; grey = slate till; pink and red (drumlins) = Lawrencetown Till

fusivity are both controlled by similar factors such as porosity, water filled pore space, etc (Washington *et al.* 1994). Both are similar, so permeability is used as a proxy for diffusion.

(2)
$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial z^2} - \lambda C$$

Where C is radon soil gas concentration in Bq m⁻³, t is time, D is the diffusivity of radon in the soil in m² s⁻¹, and z is depth in meters.

Assuming that the soil does not produce radon, which it is in a steady state and does not change over time (for the sake of the model), the right side of that equation is equal to zero. The solution is seen in equation 3:

(3)
$$\frac{\lambda C}{D} = D \frac{\partial^2 C}{\partial z^2}$$

Integrating once, the solution is shown in equation 4, where A is the constant of integration and z is depth.

$$\frac{\partial C}{\partial z} = A e^{\frac{\lambda z}{D}}$$

Integrating a second time, the solution is found in equation 5, where *B* is a second constant of integration.

(5)
$$C(z) = \frac{AD}{\lambda} e^{\frac{\lambda z}{D}} + B$$

Two boundary conditions are shown in equations 6 and 7. Substituting equation 7 back into equation 5 allows one to solve for A, while the flux at L is equal to the constant F_0 . Substituting equation 7 back into equation 4, shows the solution for I.

$$(6) C(0) = C_{atm}$$

$$D\frac{\partial C}{\partial z}\big|_{z=L} = F_0$$

The final solution is:

(8)
$$C(0) = \frac{F_0}{De^{\frac{\lambda L}{D}}} \frac{D}{\lambda} e^{\frac{\lambda z}{D}} + \left[C_{atm} - \frac{F_0}{De^{\frac{\lambda L}{D}}} \right]$$

Where C is the depth dependant concentration in Bq m⁻³, F_0 is the flux of radon from the bedrock in Bq m⁻³ s⁻¹, z is the depth in meters, D is the diffusivity of radon in the soil in m² s⁻¹, λ is the radon decay constant and is unitless, C_{atm} is the atmospheric radon concentration in Bq m⁻³.

The radon concentration was calculated for a sampling depth of 60 cm. Using Graham's Law of Effusion with respect to CO_2 (Mason and Kronstadt 1967), the diffusivity of radon in water is calculated to be 2×10^{-10} m² s⁻¹, and using Fick's Law, in free air it is approximately 7.1×10^{-6} m² s⁻¹. This means that the lowest possible diffusivity of radon in the soil is assumed to be around 2×10^{-11} m² s⁻¹, and the highest possible diffusivity must be slower than 10^{-5} m² s⁻¹, because radon in free air is 1.62×10^{-5} m² s⁻¹ (Davidson and Trumbore 1995). Because the granite facies (which also had the highest soil permeability) was used for the model the lowest value was ruled out. The

model was run to determine the diffusivity of the till and the production of radon from the bedrock that would be required to achieve the measured field concentration of radon in soil gas. Diffusivities ranged from 10^{-7} m² s⁻¹ (fastest) to 10^{-10} m² s⁻¹ (slowest), and production rates ranged from 1 to 1000 Bq m⁻³. The depth to the bedrock was set at 1.6 m because the till thickness was generally thin, therefore, the bedrock on average is assumed to be one meter below sampling depth for the model, except where drumlins were present.

BEDROCK GEOLOGY

Within the Halifax Regional Municipality sample area, three dominant geologic units are of interest (Fig. 1). The study focused on soil (glacial till is the parent material) developed over these three major bedrock types: the Cambrian-Ordovician Goldenville and Halifax groups, and Devonian granite of the South Mountain Batholith. The Goldenville and Halifax groups consist of, primarily, metasandstone and slate, respectively (White *et al.* 2008). Devonian granite intruded both the Goldenville and Halifax groups. The granite has been subdivided, based on its composition and cooling history, into primitive monzogranite, middle stage coarse-grained leucomonzogranite, and evolved fine-grained leucomonzogranite (MacDonald and Horne 1987).

SURFICIAL GEOLOGY

Within HRM, two glacially derived till units dominate the surficial geology and associated landforms (Fig. 2). One is the locally derived Beaver River Till that has been subdivided into three mappable units based on a number of different criteria including dominant clast type, matrix composition/texture, and geochemistry: (1) slate facies; (2) metasandstone facies; and (3) granite facies (Stea and Finck 2001). The three informal sub-units of the South Mountain Batholith granite till include: (1) early granite till, derived from relatively primitive granite including granodiorite and monzogranite; (2) middle granite till, derived from a relatively moderately evolved coarsegrained leucomonzogranite; and (3) late granite till derived from relatively highly evolved fine-grained leucomonzogranite (MacDonald and Horne 1987).

The second dominant till type is the distally derived Lawrencetown Till (Stea and Fowler 1981). This till unit is distinct from the Beaver River Till because (1) it contains clasts from as far away as the Cobequid Highlands (100 km to the north), (2) the matrix is (commonly) finer grained than in the Beaver River Till, and (3) it has a relatively distinct brick-red color. The distribution of the till facies mimics that of the underlying bedrock (Fig 2 versus Fig. 1).

Beaver River Till - granite facies

The clasts of the granite till facies are comprised of angu-

lar, local monzogranite, granodiorite, and leucomonzogranite set in a granite-derived sandy till (Stea and Fowler 1981). It is commonly yellow-brown to yellow-grey. Granite till commonly gives rise to a hummocky terrain with an average thickness of 2 m and a maximum of 5 m. Commonly, the granite till facies forms a thin veneer (<1 m) in areas of abundant granite bedrock.

Beaver River Till - slate facies

The slate till facies of the Beaver River Till is derived from Halifax Group slate and the till contains clasts of slate (Stea and Fowler 1981). The sandy matrix is commonly light olive brown. The slate facies till forms a thin (<4 m) sheet over polished slate bedrock.

Beaver River Till - metasandstone faces

The metasandstone facies till (formerly quartzite till of Stea and Fowler 1981) is light bluish grey and contains loose, angular metasandstone and metasiltstone clasts, largely cobble sized, set in a silt-sand matrix. The till sheet averages 3 m in thickness but can be up to 20 m thick in drumlins.

Lawrencetown Till

The Lawrencetown Till is distinct from the Beaver River Till because it is a distally derived till unit that is characterized by its generally high clay and clast content. This till was derived from tens of kilometers up-ice, and does not reflect the underlying bedrock geology; it has a distinct brick red to crimson-ochre red color. The Lawrencetown Till has a higher effective cohesion and tends to retain moisture compared to Beaver River Till (Lewis *et al.* 1998). The Lawrencetown Till is commonly found in drumlins up to 25 m thick.

RESULTS

All field sites sampled had measurable radon soil gas present in kBq m $^{-3}$ (detection limit of 0.02 kBq m $^{-3}$); raw data are available in the appendix. The radon concentrations collected for the HRM surficial geology units are highly variable (Fig. 3). The highest variability is in the BRT granite facies. This could be due, in part, to soil heterogeneity, exemplified in the unsorted nature and large variable size and composition of the clasts in the granite till.

The highest concentrations of mean radon soil gas based on field results (Fig. 4) are generally found in till developed over the South Mountain Batholith. This includes the BRT monzogranite, and the coarse-and fine-grained leucomonzogranite.

A box and whisker plot (Fig. 5) shows one of the most important aspects of the permeability data: the high variability within units. Large differences in permeability values were noted from within a single site. At some sites, five probes within 10 m of each other produced five drastically different values. One pos-

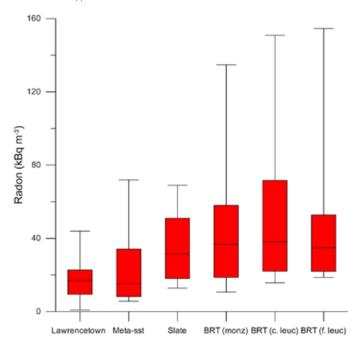


Fig. 3. Box and whisker plot showing range of radon soil gas concentrations in the surficial geology units of the HRM area: the Lawrencetown Till and the Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse-grained leucomonzogranite facies, and fine-grained leucomonzogranite facies). The bottom and top of the box represent 25th and 75th percentiles. The band near the middle represents the median, and the ends of the whiskers are the minimum and maximum values.

sible explanation for the variability in Lawrencetown Till may be due to the presence of sand pockets within the clay rich till.

The permeability values presented in the box and whisker plot (Fig. 5) represent all the data (i.e., 5 probes from each site, total 200), and show the trends and variability. The geometric mean is typically used to estimate effective permeability from small-scale samples (Jensen 1991). The geometric mean was chosen to determine if there was a large discrepancy between the mean values and the geometric mean values. Although the absolute values were different between the two, overall, the geometric mean values in Figure 6 follow the same trend as shown by the arithmetic mean values in Figure 5. Lawrencetown Till had the lowest permeability followed by the granite facies, slate facies, and finally the metasandstone facies had the highest permeability. Subdividing the granite facies the monzogranite has a low geometric mean, similar to Lawrencetown Till. Conversely, the coarse-grained leucomonzogranite has the highest permeability of the granite-derived till, approximately equivalent to the permeability of the slate till facies. The stony metasandstone till facies has the highest permeability.

Figure 7 shows the eU concentrations measured for each surficial geology unit. As with the radon and permeability values, the radioactivity was measured at 5 probes at each site, and then averaged for each site. The eU values follow the same

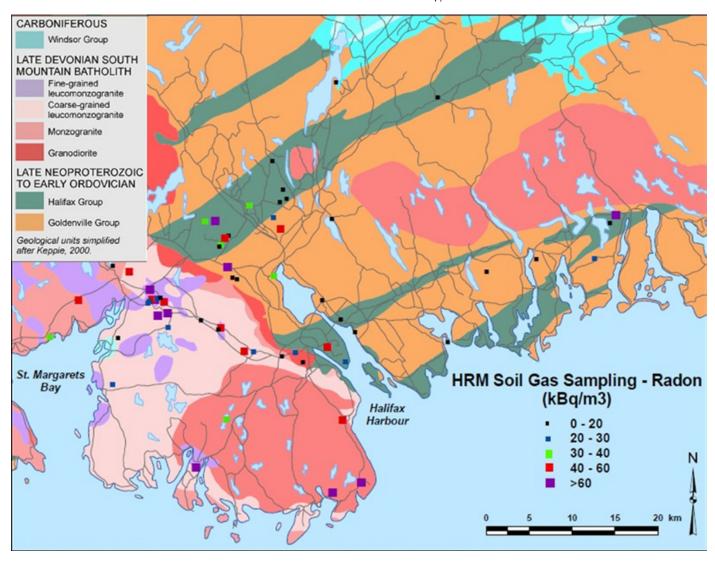
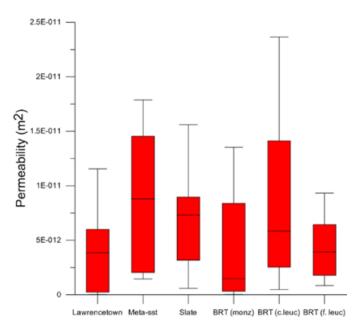


Fig. 4. Variation in mean radon soil gas concentrations ($kBq m^{-3}$) for the HRM area. Geological base map is modified after Keppie (2000).

Fig. 5. Box and whisker plot showing the range of permeability in the surficial geology units: Lawrencetown Till and Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse-grained leucomonzogranite facies, and fine-grained leucomonzogranite facies). The bottom and top of the box represent 25th and 75th percentiles. The band near the middle represents the median, and the ends of the whiskers are the minimum and maximum values.



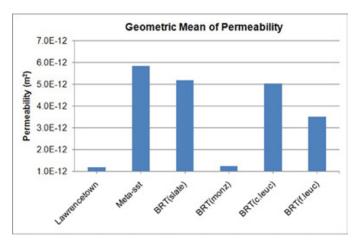


Fig. 6. Variation in the geometric mean permeability values of the different surficial geology units: Lawrencetown Till and Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse grained leucomonzogranites facies, and fine-grained leucomonzogranites facies).

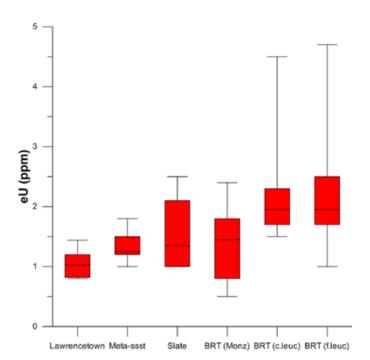


Fig. 7. Summary of equivalent uranium (eU) and equivalent thorium (eTh) concentrations (ppm) by surficial geology units: Lawrencetown Till and Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse-grained leucomonzogranites facies, and fine-grained leucomonzogranites facies). The bottom and top of the box represent 25th and 75th percentile. The band near the middle represents the median, and the ends of the whiskers are the minimum and maximum values.

trend as increasing average radon, with the Lawrencetown Till returning the lowest average values, then the metasandstone and slate facies, and finally the granite facies with the highest uranium concentration.

Figure 8 shows the eTh concentrations measured for each surficial geology unit. Again, the radioactivity was measured from 5 probes at each site, and then averaged for each site. Equivalent thorium (eTh) follows a slightly different trend than eU (Fig. 7), with the Lawrencetown Till showing the lowest average values, followed by granite and metasandstone facies. The slate facies returns the highest average eTh concentrations.

The potassium concentrations (Fig. 9) have the same general trend as eU. The lowest average concentrations were seen in Lawrencetown Till, and the highest associated with the granite facies. In relation to radon and radioactivity, the units are not statistically different, but the trends are still important. This result is not uncommon in radon soil gas studies; soil radon values are very erratic over short distances in the order of a few metres (Durrani and Badr 1995); however, statistical analyses have shown that the larger scale variations in radon soil gas are determined by the underlying geology.

Figure 10 presents the SRP value for each of the surficial geology units tested. The granite facies of Beaver River Till,

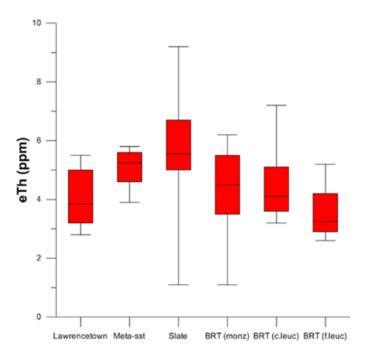


Fig. 8. Summary of equivalent thorium (eTh) concentrations (ppm) by surficial geology units: Lawrencetown Till and Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse-grained leucomonzogranite facies). The bottom and top of the box represent 25th and 75th percentile. The band near the middle represents the median, and the ends of the whiskers are the minimum and maximum values.

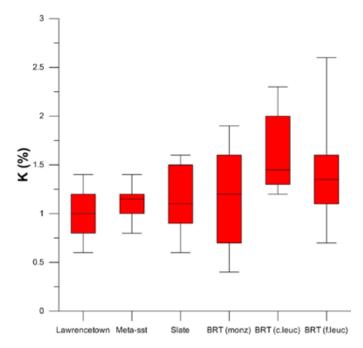


Fig. 9. Summary of potassium concentrations (pct) by surficial geology units: Lawrencetown Till and Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse-grained leucomonzogranite facies, and fine-grained leucomonzogranite facies). The bottom and top of the box represent 25th and 75th percentile. The band near the middle represents the median, and the ends of the whiskers are the minimum and maximum values.

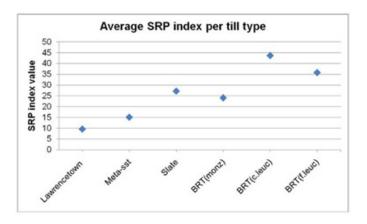


Fig. 10. Variation in soil radon potential (SRP) index results by surficial geology units: Lawrencetown Till and Beaver River Till (metasandstone facies, slate facies, monzogranite facies, coarse-grained leucomonzogranite facies).

which has the highest radon average, also has the highest SRP, and Lawrencetown Till, which has the lowest radon average (as well as the lowest permeability average), has the smallest SRP. A negative minimum SRP value (-0.1) is calculated for one Lawrencetown Till sample site. At this specific site, the perme-

ability apparatus showed no movement after 10 minutes, and was assigned the 'low permeability' value of 2.0×10^{-14} m². At the same site soil gas was also difficult to extract, and returned a low radon soil gas concentration of 0.3 kBq m⁻³. When these two values are put into the SRP equation, it yields a negative value. However, this does not show up at other sites where there is a 'low permeability' value assigned because the radon soil gas values are high enough to compensate for the 'low permeability' number. This negative site value was included in the average Lawrencetown Till SRP index, shown in Fig. 10, though the SRP does not change drastically if this negative site is excluded (from 9.6 to 10.6).

The analytical gas transport equation (equation 8) results for radon, using specific diffusivities (10^{-7} to 10^{-10} m² s $^{-1}$) and production rates (1 to 1000 Bq m $^{-3}$) are presented in Table 1. It shows the diffusivities and production rates that are required to achieve the soil radon concentrations found, assuming gas transport from bedrock across 1 m of inert soil between production and detection depth.

DISCUSSION

Field work

Determining the sensitivity of the SRP index is important in understanding the relative importance of permeability and radon production rate values. In equation 1, the radon concentration is linearly related to the SRP, and the permeability is related to the SRP by:

This shows that the SRP equation is ten times more sensitive to changes in concentration than permeability, meaning in the equation, permeability is a much less important determinant of SRP.

The permeability (Fig. 5) between units varies approximately one order of magnitude. Although the SRP equation is ten times less sensitive to permeability changes, there is an approximately ten times higher variation in permeability amongst the field sites making both variables yield approximate equal weighting in the SRP. Therefore, both seem roughly equal as determinants of SRP in Halifax Regional Municipality, and should both be considered important factors to measure.

One of the original hypotheses dealt with using eU values as a proxy for radon soil gas concentration. Based on the eU concentrations measured, this assumption is somewhat reasonable, but there will always be exceptions. The eU does follow the same trend as radon, the higher the eU at a site, the higher the radon soil gas concentration.

One of the main issues when collecting soil gas radon is site variance. Most of the variability is due to heterogeneity of the till; in particular the grain size. This study has shown that the till derived from the bedrock must contribute significantly more radon soil gas than the actual bedrock at depth. Gener-

ally within HRM, the surficial unit on top of the bedrock is thin, typically only a few meters thick; with the bedrock, even at 1 m below detection depth, the decay rate acts faster than the gas can realistically travel.

Soil gas modeling

In order to yield a concentration of $\sim 10-60~kBq~m^{-3}$ at 60 cm depth, a diffusivity of $10^{-7}~m^2~s^{-1}$ is needed over a wide array of productions (Table 1). The calculated concentrations are similar to the average concentrations in the granite facies till. The model allows the testing of the assumption of distant transport from the bedrock; assuming the soil does not emit any radon, the production of radon from the bedrock can be tracked through depth with different diffusivities. The till is assumed to be inert in order to test the transport and decay systems, which will not be complicated by local production of radon in the overlying till: transit time and decay time are the two major factors. As it is an analytical measurement, there is no error in these calculations.

For example, if 25 Bq m⁻³ s⁻¹ was produced from the bedrock, a diffusivity of 4×10^{-7} m² s⁻¹ would be needed to detect a similar concentration of radon with 60 cm of overlying granite facies till. This is not measured data: it is a test of an assumption in a purely homogenous and perfect virtual setting as described by physical laws. The diffusivities calculated are reasonable for this till type, especially because they are partially saturated; water-filled pore spaces yield lower gas permeability (Fujiyoshi et al. 2005), and inhomogenous in a non-perfect setting. It is likely that the diffusivity values of 10^{-7} m² s⁻¹ are much too high for a granite-derived till in HRM, as it is very close to that of radon in free air (10^{-6} m² s⁻¹); therefore, the till would have to be extremely arid and open to the atmosphere. A probable diffusivity would be in the 10^{-8} to 10^{-10} m² s⁻¹ range, where till may be more saturated and less homogenous.

By testing the modeling process, it is unlikely that radon transport from depth alone (bedrock) can contribute to the concentrations measured at 60 cm. Therefore, radon soil gas must come predominantly from the till, near the site of sampling. The production of radon from within the till plays a bigger role than the transient time - it is unlikely that transport can allow radon to reach the surface from a bedrock source before it decays unless the glacially derived soil is extremely thin, or absent. Soil gas modeling work in this study concludes that soil is likely the major contributor of radon gas.

Overall, this study is useful to help understand the transport of radon soil gas in HRM and elsewhere in Nova Scotia. The SRP equation has been used to assess areas of potential risk. Radon is a daughter product of uranium and site specific spectrometer measurements show a broader estimate of radon potentials as well. Future soil gas modeling should concentrate on the rate of production and diffusivity of the various soil types within HRM.

CONCLUSIONS

The calculated SRP index indicates the BRT granite facies returned the highest mean value of 34.5, followed by the slate facies (27.2), and metasandstone (15.1). The distally derived clay-rich Lawrencetown Till shows very low permeability and radon soil gas concentrations, which is reflected in the lowest SRP index value of 9.1. Soil gas modeling was used to show the potential productivities and diffusivities needed to see the field concentration. Using a modified diffusivity equation, possible diffusivities and production rates of radon at a bedrock depth of 1.6 m were calculated. A diffusivity of 10-7 m² s⁻¹ was needed with a production of 10–1000 Bq m⁻³ at depth, in order to get radon concentrations similar to the arithmetic mean. This is very fast diffusivity, and highly unlikely in the granite facies. Large variations are seen in radon concentrations and permeability values within each unit. Further testing to potentially resolve some of the variability issues would be important in understanding more about the radon soil gas concentrations in HRM, and the health implications surrounding it.

ACKNOWLEDGEMENTS

This paper was the basis of a B.Sc. thesis at Saint Francis Xavier University by Kelsey O'Brien. Nick Nickerson is thanked for his knowledge and calculus manipulation in soil gas modeling. Geologists at the Nova Scotia Department of Natural Resources provided data, employment and experience. Earth Sciences Research Centre students at Saint Francis Xavier University are thanked for their help. Nova Scotia Department of Natural Resources Mineral Resources Branch, Health Canada, Geological Survey of Canada, and Natural Sciences and Engineering Research Council of Canada contributed funding for this study. We thank journal reviewers Michael Parkhill, Ken Ford, and co-editors Ian Spooner and Daniel Utting for their constructive comments and edits.

REFERENCES

Ball, B., Scott, A., and Parker, J. 1999. Field N₂O, CO₂ and CH₄ fluxes in relation to tillage, compaction and soil quality in Scotland. Soil and Tillage Research, 53, pp. 29–39. doi:10.1016/S0167-1987(99)00074-4

Chen, J., Ly, J., Bergman, L., Wierdsma, J., and Klassen, R.A. 2008. Variation of soil radon concentrations in Southern Ontario. Radiation Protection Dosimetry, 131, pp. 385–389. doi:10.1093/rpd/ncn192

Chen, J. 2009. A preliminary design of a radon potential map for Canada: a multi-tier approach. Environmental Earth Sciences, 58, p.775–782. doi:10.1007/s12665-009-0073-x Davidson, E. A., and Trumbore, S. E. 1995. Gas diffusivity and

- production of CO₂ in deep soils of the eastern Amazon. Tellus, 47B, pp. 550–565.
- Durrani, S. A., and Badr, I. 1995. Geostatistically controlled field study of radon levels and the analysis of their spatial variation. Radiation Measurements, 25, pp. 565–572. doi:10.1016/1350-4487(95)00185-H
- Freeze, R.A., and Cherry, J.A. 1979. Groundwater. Prentice-Hall, Inc., New Jersey, 604 p.
- Friske, P.W.B., Ford, K.L, Kettles, I.M., McCurdy, M.W., McNeil, R.J., and Harvey, B.A. 2010. North American Soil Geochemical Landscapes Project: Canadian field protocols for collecting mineral soils and measuring soil gas radon and natural radioactivity. Geological Survey of Canada. Open File 6282, 177p.
- Fujiyoshi, R., Kinoshita, M., and Sawamura, S. 2005. Variation of ²²²Rn activity concentration in soil gas at a site in Sapporo, Japan. Environmental Geochemistry and Health, 27, pp. 539–547. doi:10.1007/s10653-005-7569-4
- Goodwin, T.A. 2008. Nova Scotia's involvement in the North American Soil Geochemical Landscapes Project. *In* Mineral Resources Branch, Report of Activities 2007. *Edited by* D. R. MacDonald. Nova Scotia Department of Natural Resources, Report ME 2008-1, pp. 29–33.
- Goodwin, T. A., Ford, K. L., Friske, P. W. B., and McIsaac, E. M. 2008. Radon Soil Gas in Nova Scotia. *In* Mineral Resources Branch, Report of Activities 2008. *Edited by* D. R. MacDonald. Nova Scotia Department of Natural Resources, Report ME 2008-1, p. 25.
- Goodwin, T. A, Ford, K.L., Friske, P.W.B., and McIsaac, E.M. 2009a. Radon soil gas in Nova Scotia. *In Mineral Resources* Branch, Report of Activities 2008. *Edited by*. D. R. MacDonald and K. A. Mills. Nova Scotia Department of Natural Resources, Report ME 2009-1, pp. 25–34.
- Goodwin, T. A, Ford, K.L., Friske, P.W.B., and McIsaac, E.M. 2009b. Radon soil gas in the Halifax Regional Municipality: should we be concerned? *In* Mineral Resources Branch, Report of Activities 2008. *Edited by* D. R. MacDonald and K. A. Mills. Nova Scotia Department of Natural Resources, Report ME 2009-1, p.35–43.
- Health Canada 2009. Environmental and workplace health, Government of Canada radon guideline. URL http://www.hc-sc.gc.ca/ewh-semt/radiation/radon/guidelines_lignes_directrice-eng.php> July 2010.
- Je, I. 1998. Bedrock structure control on soil-gas radon²²² anomalies in the Toronto Area, Ontario, Canada. Environmental and Engineering Geoscience, 4, pp. 445–454.
- Jensen, J. L. 1991. Use of the Geometric Average for Effective Permeability Estimation. Mathematical Geology, 23, pp. 833–840. doi:10.1007/BF02068778
- Kayler, Z., Sulzman, E., Rugh, W., Mix, A., and Bond, B. 2010. Characterizing the impact of diffusive and advective soil gas transport on the measurement and interpretation of the isotopic signal of soil respiration. Soil Biology and Biochemistry, 42, p. 435–444. doi:10.1016/j.soilbio.2009.11.022

- Keppie, J. D. 2000. Geological Map of the Province of Nova Scotia; Nova Scotia Department of Natural Resources, Mines and Energy Branch, Map ME 2000-1, scale 1:500 000.
- Lewis, C.F.M., Taylor, B.B., Stea, R.R., Fader, G.B.J., Horne, R.J., MacNeill, S.G. and Moore, J.G. 1998. Earth science and engineering: urban development in the metropolitan Halifax region. In Urban Geology of Canadian Cities, Edited by. P.F. Karrow and O.L. White. Geological Association of Canada, Special Paper 42, pp. 409–444.
- MacDonald, M., and Horne, R. 1987. Geological map of Halifax and Sambro (NTS sheets 11 D/12 and 11 D/05), Nova Scotia. Nova Scotia Department of Mines and Energy, Map 87-6, scale 1:50 000.
- Mason, E. A. and Kronstadt, B. 1967. Graham's Laws of Diffusion and Effusion. Journal of Chemical Education, 44, pp. 740–744.
- Nazaroff, W. W. 1992. Radon transport from soil to air. Reviews of Geophysics, 92, pp. 137–160. doi:10.1029/92RG00055
- Neznal, M., Neznal, M., Matolin, I. B., Barnet, I., and Miksova, J. 2004. The new method for assessing the radon risk of building sites; Czech Geological Survey Special Papers 16, pp. 1–48 p.
- Penman, H. 1940. Gas and vapour movements in soil: The diffusion of vapors through porous solid. Journal of Agricultural. Science, 30, pp. 437–462. doi:10.1017/S0021859600048164
- Risk, D., Kellman, L., and Beltrami, H. 2008. A new method for in situ soil gas diffusivity measurement and applications in the monitoring of subsurface CO₂ production. Journal of Geophysical Research, 113, pp. 1–9. doi:10.1029/2007JG000445
- Stea, R.R., and Fowler, J.H. 1981. Pleistocene geology and till geochemistry of central Nova Scotia (sheet 4), 1980. Nova Scotia Department of Mines and Energy, Map 81-1, Scale 1:100 000.
- Stea, R., and Finck, P. 2001. An evolutionary model of glacial dispersal and till genesis in Maritime Canada. *In* Drift Exploration in Glaciated Terrain. *Edited by* M. B. McClenaghan, P. T. Bobrowsky, G. E. M. Hall, and S. J. Cook. Geological Society of London Special Publication 185, pp. 237–265.
- Washington, J., Rose, A., Ciolkosz, J., and Dobos, R. 1994. Gaseous diffusion and permeability in four soil profiles in central Pennsylvania. Soil Science, 157, pp 65–76. doi:10.1097/00010694-199402000-00001
- White, C. E., Bell, J. A., McLeish, D. F., MacDonald, M. A., Goodwin, T. A., and MacNeil, J. D. 2008. Geology of the Halifax Regional Municipality. *In* Mineral Resources Branch Report of Activities 2007. *Edited by* D. R. MacDonald; Nova Scotia Department of Natural Resources, Report ME 2008-001, pp. 125–139.
- World Health Organization 2005. Fact Sheet No. 291: Radon and cancer, June 2005. URL http://www.who.int/mediacentre/factsheets/fs291/en/index.html January 2011.

Editorial responsibility Daniel J. Utting

Appendix. Radon soil gas results from HRM.

| Lawrenceown III | Site ID | Till Sheet Name | Dominant Clast Type | utmE83 | utmN83 | Rn (kBa/m ³) | Permeability (m ²) | K (nct) | eU(nnm) | eTh(ppm) | SRP Index |
|--|-----------|-------------------|---------------------|--------|---------|--------------------------|--------------------------------|---------|---------|----------|-----------|
| Lawrenceown Till wurded dass* 446745 4958841 23,7 13,65E.12 13,13 13,13 13,13 Lawrenceown Till wurded dass* 446742 495783 15,9 6.00E.12 13,13 13,13 13,13 Lawrenceown Till wurded dass* 445761 495783 39,1 2.38E.13 1,0 1,0 1,0 1,0 Lawrenceown Till wurded dass* 44587 4967268 39,1 2.38E.13 1,0 1,0 1,0 1,0 Lawrenceown Till wurded dass* 44587 4967268 39,2 5.00E.14 0.0 0.8 2.8 Lawrenceown Till wurded dass* 44587 496725 79 5.00E.14 0.8 0.8 3.2 Lawrenceown Till wurded dass* 44787 496023 1,2 5.8 4.08E.12 0.8 0.8 3.2 Lawrenceown Till wurded dass* 44787 496023 1,2 5.8 4.08E.12 0.8 0.8 3.2 Lawrenceown Till wurded dass* 44787 496023 1,2 1,2 1,2 1.2 1.2 1.2 Beaver River Till metasandstone 44557 496023 1,2 1,2 1,2 1.2 1.2 1.2 1.2 Beaver River Till metasandstone 44558 4951268 1,3 1,2 1,2 1.2 1.2 1.2 1.2 1.2 Beaver River Till metasandstone 44752 495248 1,3 1,2 1,2 1.2 1.2 1.2 1.2 1.2 1.2 Beaver River Till metasandstone 44752 495248 1,3 1,2 1.1 1.1 1.1 1.2 1 | | | - A(| | | / I | () (| (ind) | (/L-L) | (FF) | |
| Lawrenceown TIII varied class* 456.27 495.887 14 13 5.0 Lawrenceown TIII varied class* 445.941 495.883 39.1 2.38E-13 1.4 14 5.5 Lawrenceown TIII varied class* 443.941 495.883 39.1 1.38E-13 1.0 1.0 5.2 Lawrenceown TIII varied class* 443.941 495.883 39.1 1.0 1.0 1.0 5.2 Lawrenceown TIII varied class* 446.52 495.949 1.6 3.8E-12 0.0 0.8 0.8 0.8 2.8 Lawrenceown TIII varied class* 446.52 496.93 1.6 4.6E-1 0.8 0.8 0.8 2.8 Lawrenceown TIII varied class* 446.52 496.93 1.2 4.6E-1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 <t< td=""><td>HRM08-001</td><td>Lawrencetown Till</td><td>varied clasts*</td><td>446745</td><td>4958417</td><td>22.7</td><td>3.62E-12</td><td>1.2</td><td>1.2</td><td>3.4</td><td>14.6</td></t<> | HRM08-001 | Lawrencetown Till | varied clasts* | 446745 | 4958417 | 22.7 | 3.62E-12 | 1.2 | 1.2 | 3.4 | 14.6 |
| Lawrencetown III varied class* 447612 497513 44 6.88E-13 114 1.5 Lawrencetown III varied class* 44901 497439 9.9 1.16E11 11 11 5.5 Lawrencetown III varied class* 45906 497258 9.9 6.08E-1 0.0 8.8 2.8 Lawrencetown III varied class* 44787 49023 7.9 5.08E-1 1.0 1.0 1.0 2.8 Lawrencetown III varied class* 44787 49023 7.9 5.08E-1 0.8 0.8 2.8 Lawrencetown III varied class* 44753 49023 1.78 4.08E-1 0.8 0.8 2.8 Lawrencetown III varied class* 44753 495127 1.1 1.2 1.2 1.4 5.5 Lawrencetown III varied class* 44753 495127 1.1 1.2 1.2 1.2 1.4 4.4 Beaver Reer III metasandsone 44524 495283< | HRM08-009 | Lawrencetown Till | varied clasts* | 456276 | 4945087 | 15.9 | 6.00E-12 | 1.3 | 1.3 | 5.0 | 11.8 |
| Lawrenceown Till varied class* 44594 457368 39.1 2.28B-13 1.0 1.0 5.2 Lawrenceown Till varied class* 456879 457268 9.8 1.16E-11 1.1 1.1 5.2 Lawrenceown Till varied class* 466879 457246 9.8 2.00E-14 0.6 0.8 2.8 Lawrenceown Till varied class* 44682 496490 16.3 5.54E-14 0.6 0.8 2.8 Lawrenceown Till varied class* 44682 496490 16.3 5.54E-14 0.8 0.8 2.8 Lawrenceown Till varied class* 44763 496490 16.3 5.54E-14 0.8 2.8 2.8 Beaver Row Till mecasandsone 44753 495168 5.7 1.3EE-1 1.1 1.0 5.2 Beaver Row Till mecasandsone 447544 495268 1.1 1.2 1.4 5.5 Beaver Row Till mecasandsone 447536 495266 1.1 | HRM08-012 | Lawrencetown Till | varied clasts* | 447612 | 4957131 | 44 | 6.38E-13 | 1.4 | 1.4 | 5.5 | 19.2 |
| Lawrencetown Till varied class* 45.00f 4974179 19.8 LifeFil 1.1 4.1 Lawrencetown Till varied class* 468879 4972368 19.8 2.00E:14 0.6 0.8 2.8 Lawrencetown Till varied class* 448304 4960653 7.9 5.03E-12 1.0 1.0 3.5 Lawrencetown Till varied class* 44787 496028 1.73 4.08E-12 0.8 0.8 2.8 Lawrencetown Till varied class* 447537 4960253 1.78 4.08E-12 0.8 0.8 2.8 Beaver River Till metasandstone 443734 495127 1.17E-11 1.2 1.2 1.2 5.8 Beaver River Till metasandstone 47354 495265 7.1 1.79E-11 1.0 1.3 4.6 Beaver River Till metasandstone 47364 455265 7.1 1.79E-11 1.1 1.1 4.1 Beaver River Till metasandstone 47364 455265< | HRM08-013 | Lawrencetown Till | varied clasts* | 443941 | 4959838 | 39.1 | 2.38E-13 | 1.0 | 1.0 | 5.2 | 14.3 |
| Lawrenceown Till varied class** 465879 4772468 0.8 200E-14 0.6 0.8 2.8 Lawrenceown Till varied class** 445874 4960453 7.9 5.08E-12 1.0 0.8 2.8 Lawrenceown Till varied class** 44757 4960459 16.3 5.4E-14 0.8 0.8 2.8 Lawrenceown Till varied class** 446621 466496 16.3 5.4E-14 0.8 0.8 2.8 Beaver ReverTill metasandsone 435768 345187 1.7 1.48E-12 1.2 1.4 5.5 Beaver ReverTill metasandsone 445314 455885 1.9 1.4 1.5 5.4 Beaver ReverTill metasandsone 445244 455885 1.9 1.4 1.3 5.4 Beaver ReverTill metasandsone 447349 455885 1.9 1.1 1.1 1.1 1.5 5.5 Beaver ReverTill metasandsone 44730 495362 1.1 | HRM08-016 | Lawrencetown Till | varied clasts* | 454061 | 4974179 | 19.8 | 1.16E-11 | 1.1 | 1.1 | 4.1 | 2.6 |
| Lawrenceown III varied clasts* 48334 4960633 7.9 5.03E-12 1.0 1.0 3.6 Lawrenceown III varied clasts* 447877 4967266 16.3 5.54E-14 0.8 0.8 2.3 Lawrenceown III varied clasts* 447537 4960253 17.8 408E-12 0.8 0.8 2.8 Beaver River III metasandstone 447537 4960488 3.5 145E-1 1.2 1.2 5.8 Beaver River III metasandstone 453527 435127 1.1 1.9E-1 1.2 1.2 5.8 Beaver River III metasandstone 45327 435285 1.9 1.4E-1 1.2 1.2 5.8 Beaver River III metasandstone 453242 495285 1.9 1.4E-1 1.3 4.6 Beaver River III metasandstone 457368 495265 1.0 1.0 1.1 1.0 1.0 3.6 Beaver River III metasandstone 457368 495265 </td <td>HRM09-018</td> <td>Lawrencetown Till</td> <td>varied clasts*</td> <td>465879</td> <td>4972368</td> <td>8.0</td> <td>2.00E-14</td> <td>9.0</td> <td>8.0</td> <td>2.8</td> <td>-0.1</td> | HRM09-018 | Lawrencetown Till | varied clasts* | 465879 | 4972368 | 8.0 | 2.00E-14 | 9.0 | 8.0 | 2.8 | -0.1 |
| Lawrenceown TIII varied class* 447827 4961726 9.4 6.03E-12 0.8 0.8 3.2 Lawrenceown TIII varied class* 447537 4960253 17.8 6.08E-12 0.8 0.8 3.2 Lawrenceown TIII varied class* 447537 4958048 35.2 1.45E-11 1.2 1.2 2.8 Beaver River TIII metasandstone 44537 4958248 3.5 1.45E-11 1.1 1.5 5.5 Beaver River TIII metasandstone 443727 495828 1.9 1.45E-12 1.1 1.5 5.5 Beaver River TIII metasandstone 44373.4 495828 1.9 1.45E-12 1.1 1.5 5.6 Beaver River TIII metasandstone 447174 4958265 1.0 1.130E-1 1.1 1.5 5.6 Beaver River TIII metasandstone 447103 4957655 1.0 1.130E-1 1.1 1.1 4.6 Beaver River TIII metasandstone 447164 </td <td>HRM09-019</td> <td>Lawrencetown Till</td> <td>varied clasts*</td> <td>448304</td> <td>4960653</td> <td>7.9</td> <td>5.03E-12</td> <td>1.0</td> <td>1.0</td> <td>3.6</td> <td>5.2</td> | HRM09-019 | Lawrencetown Till | varied clasts* | 448304 | 4960653 | 7.9 | 5.03E-12 | 1.0 | 1.0 | 3.6 | 5.2 |
| Lawrenceown TIII varied clasts* 446652 4964969 16.3 5.5E-H 0.8 0.8 2.8 Lawrencecown TIII varied clasts* 446537 4964968 16.3 5.5E-H 0.8 0.8 2.8 Beaver River TIII metasandsone 446821 4951678 3.41 1.82E+12 1.2 1.4 5.5 Beaver River TIII metasandsone 45372 495283 5.8 1.45E+12 1.2 1.4 5.5 Beaver River TIII metasandsone 44113 495286 7.1 1.9E+12 1.2 1.5 5.8 Beaver River TIII metasandsone 471054 495865 1.9 1.45E+12 1.1 1.2 5.8 Beaver River TIII metasandsone 47154 495865 1.9 1.45E+12 1.1 1.1 4.6 Beaver River TIII metasandsone 47154 495865 1.9 1.1 1.1 1.1 4.6 Beaver River TIII metasandsone 471654 494 | HRM09-020 | Lawrencetown Till | varied clasts* | 447877 | 4961726 | 9.4 | 6.03E-12 | 8.0 | 8.0 | 3.2 | 6.7 |
| Lawrencerown TIII varied class* 447537 4900253 17.8 4.08E-12 0.8 4.4 Beaver River TIII metasandstone 44871 957848 35.2 1.45E-11 1.2 1.2 5.8 Beaver River TIII metasandstone 446821 9578281 3.7 1.57E-11 1.1 1.5 5.6 Beaver River TIII metasandstone 445242 4958281 8.7 1.57E-11 1.1 1.5 5.6 Beaver River TIII metasandstone 441413 495266 71.9 2.05E-12 1.2 1.2 5.8 Beaver River TIII metasandstone 447143 495266 71.9 2.05E-12 1.1 1.3 4.6 Beaver River TIII metasandstone 447163 2.2 2.05E-12 1.0 1.2 3.9 Beaver River TIII metasandstone 447163 495463 2.0 2.05E-12 1.0 1.1 4.6 Beaver River TIII metasandstone 447163 495623 8.1< | HRM09-021 | Lawrencetown Till | varied clasts* | 446652 | 4964969 | 16.3 | 5.54E-14 | 8.0 | 0.8 | 2.8 | 4.6 |
| Beaver River Till metasandstone 438778 4958048 35.2 145E-11 1.2 1.2 1.8 5.5 Beaver River Till metasandstone 445.24 49516.78 34.1 182E-12 1.2 1.4 5.5 Beaver River Till metasandstone 455.24 495835 18.9 1.45E-11 1.1 1.5 5.6 Beaver River Till metasandstone 452.24 495835 18.9 1.45E-12 1.1 1.5 5.6 Beaver River Till metasandstone 447154 6.2 9.91E-12 1.0 1.2 4.6 Beaver River Till metasandstone 447155 495349 6.2 9.91E-12 1.0 1.2 4.6 Beaver River Till metasandstone 447152 495349 45.8 2.2 1.1E-12 1.1 4.6 5.8 Beaver River Till alate 455063 4944683 2.2 2.1E-12 1.1 4.6 1.1 4.6 Beaver River Till slate <td>HRM09-041</td> <td>Lawrencetown Till</td> <td>varied clasts*</td> <td>447537</td> <td>4960253</td> <td>17.8</td> <td>4.08E-12</td> <td>8.0</td> <td>8.0</td> <td>4.4</td> <td>11.7</td> | HRM09-041 | Lawrencetown Till | varied clasts* | 447537 | 4960253 | 17.8 | 4.08E-12 | 8.0 | 8.0 | 4.4 | 11.7 |
| Beaver River Till metasandstone 446821 4951678 34.1 1182E12 1.2 1.4 5.5 Beaver River Till metasandstone 45253 4951271 11.7 1.79E-11 1.9 1.8 5.1 Beaver River Till metasandstone 45244 4958835 18.9 1.45E-12 1.2 1.5 5.4 Beaver River Till metasandstone 447243 495865 7.9 2.0EE-12 1.2 1.5 5.4 Beaver River Till metasandstone 477568 495265 1.9 2.0EE-12 1.2 1.5 5.4 Beaver River Till metasandstone 477564 495265 1.0 1.0EE-12 1.2 1.5 5.4 Beaver River Till metasandstone 477564 495364 2.2 2.0EE-12 1.1 1.1 4.6 Beaver River Till slate 454033 494528 1.2 1.1EE-12 1.3 4.0 Beaver River Till slate 440622 495533 <th< td=""><td>HRM08-018</td><td>Beaver River Till</td><td>metasandstone</td><td>438778</td><td>4958048</td><td>35.2</td><td>1.45E-11</td><td>1.2</td><td>1.2</td><td>5.8</td><td>9.5</td></th<> | HRM08-018 | Beaver River Till | metasandstone | 438778 | 4958048 | 35.2 | 1.45E-11 | 1.2 | 1.2 | 5.8 | 9.5 |
| Beaver River Till metasandstone 44255 4951271 11.7 1.79E-11 0.9 1.8 5.1 Beaver River Till metasandstone 453244 498281 8.7 1.57E-11 1.1 1.5 5.4 Beaver River Till metasandstone 441413 4952656 71.9 2.05E-12 1.2 1.2 5.8 Beaver River Till metasandstone 441413 4952656 71.9 2.05E-12 1.2 1.2 5.8 Beaver River Till metasandstone 471554 4952165 8.2 7.70E-12 0.8 1.0 1.2 5.8 Beaver River Till metasandstone 471554 4952165 8.2 7.70E-12 0.8 1.0 3.9 Beaver River Till slate 454063 494528 1.2 5.2E-12 1.1 1.1 4.6 Beaver River Till slate 441527 495634 1.2 1.1E-12 1.1 1.0 1.2 2.1 2.2 Beaver River Till | HRM08-003 | Beaver River Till | metasandstone | 446821 | 4951678 | 34.1 | 1.82E-12 | 1.2 | 1.4 | 5.5 | 37.7 |
| Beaver River Till metasandstone 433572 4958283 5.7 1.57E-11 1.1 1.5 5.4 Beaver River Till metasandstone 453-42 495885 18.9 1.45E-12 1.2 1.5 5.6 Beaver River Till metasandstone 477364 495149 6.2 9.91E-12 1.0 1.2 5.6 Beaver River Till metasandstone 477364 495163 8.2 7.70E-12 1.0 1.3 4.6 Beaver River Till metasandstone 471544 4952163 8.2 7.70E-12 1.1 1.1 4.6 Beaver River Till metasandstone 471564 4952163 8.2 7.70E-12 1.1 1.1 4.6 Beaver River Till slate 455005 4941639 2.7 6.2E-12 1.1 1.1 5.6 Beaver River Till slate 455005 494628 3.7 6.2E-12 1.1 1.5 5.1 Beaver River Till slate 440622 495502 <td>HRM08-004</td> <td>Beaver River Till</td> <td>metasandstone</td> <td>442536</td> <td>4951271</td> <td>11.7</td> <td>1.79E-11</td> <td>6.0</td> <td>1.8</td> <td>5.1</td> <td>0.9</td> | HRM08-004 | Beaver River Till | metasandstone | 442536 | 4951271 | 11.7 | 1.79E-11 | 6.0 | 1.8 | 5.1 | 0.9 |
| Beaver River Till metasandstone 452424 4958835 18.9 145E-12 1.5 5.6 Beaver River Till metasandstone 44413 4952656 1.9 2.05E-12 1.5 1.5 5.8 Beaver River Till metasandstone 477368 4953625 10.1 1.30E-11 1.0 1.2 5.8 Beaver River Till metasandstone 477368 495362 10.1 1.30E-11 1.4 1.3 4.0 Beaver River Till metasandstone 477368 495364 2.2 7.70E-12 0.8 1.0 1.3 4.0 Beaver River Till slate 457603 4941683 2.7 6.29E-12 0.8 1.0 1.3 4.6 Beaver River Till slate 454603 494628 1.2 6.29E-12 0.9 1.1 1.0 1.2 5.9 Beaver River Till slate 440622 4956203 5.0 5.91E-13 1.0 1.1 1.1 1.2 5.8 | HRM08-007 | Beaver River Till | metasandstone | 453572 | 4958281 | 5.7 | 1.57E-11 | 1.1 | 1.5 | 5.4 | 0.9 |
| Beaver River Till metasandstone 441413 4952656 71.9 2.05E-12 1.2 5.8 Beaver River Till metasandstone 472033 4951419 6.2 9.91E-12 1.0 1.2 5.8 Beaver River Till metasandstone 477554 4953625 10.1 1.30E-12 1.0 1.2 4.6 Beaver River Till metasandstone 473683 4953644 2.2 2.11E-12 1.1 1.1 4.6 Beaver River Till slate 455095 4946384 2.2 2.11E-12 1.1 1.1 4.6 Beaver River Till slate 445063 4946384 1.2 6.3E-12 1.1 1.1 4.6 Beaver River Till slate 44052 4956020 5.1 8.9E-12 1.0 5.7 Beaver River Till slate 440459 4955020 5.1 1.3E-11 1.0 5.7 Beaver River Till slate 430624 435 495803 6.2 5.9E-13 | HRM08-015 | Beaver River Till | metasandstone | 452424 | 4958835 | 18.9 | 1.45E-12 | 1.2 | 1.5 | 5.6 | 21.1 |
| Beaver River Till metasandstone 442023 4951419 6.2 9.91E-12 1.0 1.2 4.6 Beaver River Till metasandstone 477564 4953645 10.1 1.30E-11 1.4 1.3 4.0 Beaver River Till metasandstone 477564 4953644 2.2 7.70E-12 0.8 1.0 3.9 Beaver River Till slate 455095 4941883 2.7.1 6.29E-12 0.6 2.5 8.2 Beaver River Till slate 455095 4941883 2.7.1 6.29E-12 1.6 2.1 9.0 Beaver River Till slate 444062 495642 1.0 1.5 2.1 9.0 1.1 1.0 3.5 Beaver River Till slate 44062 495502 1.8 6.45E-12 1.0 1.5 5.0 6.7 Beaver River Till slate 44045 495802 6.5 1.45E-11 1.5 1.1 1.1 1.0 1.5 6.7 | HRM08-017 | Beaver River Till | metasandstone | 441413 | 4952656 | 71.9 | 2.05E-12 | 1.2 | 1.2 | 5.8 | 37.7 |
| Beaver River Till metasandstone 477368 4953625 10.1 1.30E-II 1.4 1.3 4.0 Beaver River Till metasandstone 471554 4922163 8.2 7.70E-I2 0.8 1.0 3.9 Beaver River Till slate 453063 4943304 45.8 8.2BE-I2 1.6 2.5 8.2 Beaver River Till slate 455095 4941683 27.1 6.2BE-I2 1.6 2.5 8.2 Beaver River Till slate 441167 4956341 16.0 1.56E-I1 1.2 5.4 Beaver River Till slate 440622 18.1 1.45E-I1 1.6 2.5 8.2 Beaver River Till slate 440620 18.1 1.45E-I1 1.0 3.4 Beaver River Till slate 440459 4955026 18.1 1.45E-I1 1.0 1.1 Beaver River Till monzogranite 420725 494507 2.2 1.3EE-I2 1.6 1.5 5.5 | HRM08-019 | Beaver River Till | metasandstone | 442023 | 4951419 | 6.2 | 9.91E-12 | 1.0 | 1.2 | 4.6 | 5.0 |
| Beaver River Till metasandstone 471554 4952163 8.2 7.70E-12 0.8 1.0 3.9 Beaver River Till metasandstone 484103 4935644 22.2 2.11E-12 1.1 1.1 46 Beaver River Till slate 453095 4941683 2.7 6.29E-12 1.6 2.5 8.2 Beaver River Till slate 441527 4956341 16.0 1.56E-11 1.5 2.0 6.7 Beaver River Till slate 44162 495602 51.0 8.96E-12 1.0 5.0 6.7 Beaver River Till slate 440459 495602 51.0 8.96E-12 1.0 5.0 6.7 Beaver River Till slate 440459 495802 6.1 3.4 6.7 1.0 1.1 5.0 6.7 Beaver River Till monzogranite 485042 495802 6.0 1.3EE-12 1.1 1.0 1.1 5.0 6.7 9.2 9.2 9.2 | HRM09-014 | Beaver River Till | metasandstone | 477368 | 4953625 | 10.1 | 1.30E-11 | 1.4 | 1.3 | 4.0 | 8.6 |
| Beaver River Till metasandstone 484103 4953644 22.2 2.11E-12 1.1 1.1 4.6 Beaver River Till slate 453063 494309 45.8 8.28E-12 1.6 2.5 8.2 Beaver River Till slate 455093 4941683 27.1 6.29E-12 1.6 2.1 9.2 Beaver River Till slate 444622 4956324 1.6 1.6 1.1 1.1 5.4 Beaver River Till slate 440622 4955026 18.1 1.45E-11 1.0 1.5 5.0 Beaver River Till slate 440459 4955026 18.1 1.45E-11 1.0 1.5 5.0 Beaver River Till slate 485807 65.1 1.3E-12 1.0 1.5 5.0 Beaver River Till monzogranite 492669 494 6.9 1.3E-12 1.0 1.5 5.2 Beaver River Till monzogranite 440756 494 6.9 1.3E-12 | HRM09-015 | Beaver River Till | metasandstone | 471554 | 4952163 | 8.2 | 7.70E-12 | 8.0 | 1.0 | 3.9 | 6.3 |
| Beaver River Till slate 453063 4943309 45.8 8.28E-12 1.6 5.5 8.2 Beaver River Till slate 455095 4941683 27.1 6.29E-12 1.6 2.1 9.2 Beaver River Till slate 44452 495534 16.0 1.56E-11 1.5 2.0 6.7 Beaver River Till slate 441140 4956341 16.0 1.56E-11 1.5 2.0 6.7 Beaver River Till slate 440459 4955233 3.1 1.46E-12 0.9 1.1 5.0 Beaver River Till slate 440459 4955026 18.1 1.45E-11 0.6 1.0 3.4 Beaver River Till slate 488912 495867 65.1 1.3E-12 1.0 5.7 Beaver River Till monzogranite 42075 4944607 3.4 1.3E-13 1.6 0.8 5.2 Beaver River Till monzogranite 447766 494262 1.3E-12 0.7 | HRM09-017 | Beaver River Till | metasandstone | 484103 | 4953644 | 22.2 | 2.11E-12 | 1.1 | 1.1 | 4.6 | 12.3 |
| Beaver River Till slate 455095 4941683 27.1 6.29E-12 1.6 2.1 9.2 Beaver River Till slate 454603 494628 12.8 6.35E-12 1.1 1.2 5.4 Beaver River Till slate 441140 4956200 5.10 8.96E-12 0.9 1.1 5.0 Beaver River Till slate 44042 4955205 18.1 1.46E-11 1.0 5.0 Beaver River Till slate 485912 4957806 5.0 1.1 1.0 5.0 Beaver River Till monzogranite 485912 4957807 5.0 1.3E-12 1.1 1.0 5.7 Beaver River Till monzogranite 450191 495869 69.0 1.3EE-13 1.3 1.1 1.0 5.7 Beaver River Till monzogranite 450191 4941885 1.0 3.2EE-13 1.3 1.4 6.2 Beaver River Till monzogranite 45042 494269 6.2 1.3EE- | HRM08-002 | Beaver River Till | slate | 453063 | 4943309 | 45.8 | 8.28E-12 | 1.6 | 2.5 | 8.2 | 39.9 |
| Beaver River Till slate 454603 4946528 12.8 6.35E-12 1.1 1.2 5.4 Beaver River Till slate 44157 4956341 16.0 1.56E-11 1.5 2.0 6.7 Beaver River Till slate 440622 4955026 3.1 8.96E-12 1.0 1.5 5.0 6.7 Beaver River Till slate 440462 4955026 18.1 1.45E-11 0.6 1.0 3.4 Beaver River Till slate 485912 495867 6.0 5.91E-13 0.7 1.0 5.7 Beaver River Till monzogranite 420725 4944607 3.4 1.35E-11 1.6 1.8 6.7 Beaver River Till monzogranite 450191 4945869 6.9 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 450191 4942690 2.3 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 454867 494 | HRM08-005 | Beaver River Till | slate | 455095 | 4941683 | 27.1 | 6.29E-12 | 1.6 | 2.1 | 9.2 | 21.8 |
| Beaver River Till slate 441527 4956341 16.0 1.56E-11 1.5 2.0 6.7 Beaver River Till slate 441140 4956020 51.0 8.96E-12 0.9 1.1 5.0 Beaver River Till slate 440459 4955026 18.1 1.45E-11 0.6 1.0 3.4 Beaver River Till slate 43981 495867 65.1 1.15E-12 1.1 1.0 5.7 Beaver River Till monzogranite 420725 494607 3.4 1.3E-12 1.3 1.2 5.7 Beaver River Till monzogranite 420725 494607 3.4 1.3E-11 1.6 1.3 5.5 Beaver River Till monzogranite 449262 49269 2.3.2 1.3E-11 1.1 5.5 Beaver River Till monzogranite 449264 49269 2.3.2 1.63E-12 0.6 0.8 5.5 Beaver River Till monzogranite 44805 492649 6.2 <t< td=""><td>HRM08-008</td><td>Beaver River Till</td><td>slate</td><td>454603</td><td>4946528</td><td>12.8</td><td>6.35E-12</td><td>1.1</td><td>1.2</td><td>5.4</td><td>9.5</td></t<> | HRM08-008 | Beaver River Till | slate | 454603 | 4946528 | 12.8 | 6.35E-12 | 1.1 | 1.2 | 5.4 | 9.5 |
| Beaver River Till slate 441140 4956020 51.0 896E-12 0.9 1.1 5.0 Beaver River Till slate 440622 4955223 36.1 8.64E-12 1.0 1.5 5.0 Beaver River Till slate 440459 4955026 18.1 1.45E-11 0.6 1.0 3.4 Beaver River Till slate 485912 4958669 65.0 1.31E-12 1.1 1.0 5.7 Beaver River Till monzogranite 420725 4944607 34.8 1.33E-11 1.6 1.8 6.5 Beaver River Till monzogranite 47026 494269 23.2 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 449269 23.2 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 45084 492262 3.8 1.4EE-12 0.7 0.8 2.5 Beaver River Till monzogranite 45084 492626 6.2 < | HRM08-014 | Beaver River Till | slate | 441527 | 4956341 | 16.0 | 1.56E-11 | 1.5 | 2.0 | 6.7 | 17.7 |
| Beaver River Till slate 440622 4955233 36.1 8.64E-12 1.0 1.5 5.0 Beaver River Till slate 440459 4955026 18.1 1.45E-11 0.6 1.0 3.4 Beaver River Till slate 485912 495805 65.1 3.17E-12 1.1 1.0 5.7 Beaver River Till monzogranite 48634 495869 69.0 1.32E-12 1.3 1.1 1.1 5.7 Beaver River Till monzogranite 450725 4944607 3.2 1.3E-11 1.6 1.8 4.3 Beaver River Till monzogranite 49262 494269 3.2 1.3E-11 1.1 1.5 5.5 Beaver River Till monzogranite 447766 494269 3.2 1.0E-14 0.6 0.8 3.5 Beaver River Till monzogranite 45806 49.2 1.0 1.3E-12 0.7 0.8 2.5 Beaver River Till monzogranite 45806 4 | HRM09-005 | Beaver River Till | slate | 441140 | 4956020 | 51.0 | 8.96E-12 | 6.0 | 1.1 | 5.0 | 45.9 |
| Beaver River Till slate 440459 4958026 18.1 1.45E-11 0.6 1.0 3.4 Beaver River Till slate 439981 4958057 65.1 3.17E-12 1.1 1.0 5.7 Beaver River Till slate 485312 495869 69.0 1.3E-12 1.3 1.0 1.1 Beaver River Till monzogranite 420725 4944607 34.8 1.3E-11 1.6 1.8 4.3 Beaver River Till monzogranite 449262 494269 23.2 1.3E-11 1.1 1.5 5.5 Beaver River Till monzogranite 447766 494269 3.2 1.0E-14 0.6 0.8 3.5 Beaver River Till monzogranite 454805 49367 4.0 1.3E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456894 4927659 65.2 1.63E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456894 4927659 | HRM09-006 | Beaver River Till | slate | 440622 | 4955233 | 36.1 | 8.64E-12 | 1.0 | 1.5 | 5.0 | 31.8 |
| Beaver River Till slate 439981 4958057 65.1 3.17E-12 1.1 1.0 5.7 Beaver River Till slate 485912 4957800 20.0 5.91E-13 0.7 1.0 1.1 Beaver River Till monzogranite 420725 4944607 34.8 1.33E-12 1.3 2.2 6.7 Beaver River Till monzogranite 450191 4941585 10.7 3.24E-13 1.6 1.8 4.3 Beaver River Till monzogranite 449262 494269 23.2 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 44776 494269 23.2 1.14E-12 0.6 0.8 3.5 Beaver River Till monzogranite 454805 49365 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 456984 4927643 1.34.8 1.46E-13 0.7 0.8 2.4 5.6 Beaver River Till monzogranite 45 | HRM09-007 | Beaver River Till | slate | 440459 | 4955026 | 18.1 | 1.45E-11 | 9.0 | 1.0 | 3.4 | 19.5 |
| Beaver River Till slate 485912 4957800 20.0 5.91E-13 0.7 1.0 1.1 Beaver River Till monzogranite 420725 4944607 34.8 1.33E-11 1.6 1.8 4.3 Beaver River Till monzogranite 420725 4944607 34.8 1.33E-11 1.6 1.8 4.3 Beaver River Till monzogranite 449262 4942690 23.2 1.33E-11 1.1 1.5 5.5 Beaver River Till monzogranite 447766 4942262 18.6 2.00E-14 0.6 0.8 2.5 Beaver River Till monzogranite 454805 4934872 41.0 1.31E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 0.5 1.1 Beaver River Till monzogranite 425803 | HRM09-013 | Beaver River Till | slate | 439981 | 4958057 | 65.1 | 3.17E-12 | 1.1 | 1.0 | 5.7 | 41.6 |
| Beaver River Till slate 486634 495869 69.0 1.32E-12 1.3 2.2 6.7 Beaver River Till monzogranite 420725 4944607 34.8 1.33E-11 1.6 1.8 4.3 Beaver River Till monzogranite 449262 494269 23.2 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 447766 494262 18.6 2.00E-14 0.6 0.8 3.5 Beaver River Till monzogranite 441274 4935057 38.6 1.14E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 456984 4926438 134.8 1.46E-13 0.4 0.5 1.1 Beaver River Till monzogranite 42267659 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 4226438 134.8 | HRM09-032 | Beaver River Till | slate | 485912 | 4957800 | 20.0 | 5.91E-13 | 0.7 | 1.0 | 1.1 | 8.4 |
| Beaver River Till monzogranite 420725 4944607 34.8 1.33E-11 1.6 1.8 4.3 Beaver River Till monzogranite 450191 4941585 10.7 3.24E-13 1.3 1.4 6.2 Beaver River Till monzogranite 447766 494262 18.6 2.00E-14 0.6 0.8 3.5 Beaver River Till monzogranite 44776 4935057 38.6 1.14E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 0.7 0.8 2.4 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.9 0.5 1.1 | HRM09-033 | Beaver River Till | slate | 486634 | 4958669 | 0.69 | 1.32E-12 | 1.3 | 2.2 | 6.7 | 35.4 |
| Beaver River Till monzogranite 450191 4941585 10.7 3.24E-13 1.3 1.4 6.2 Beaver River Till monzogranite 449262 4942690 23.2 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 447766 494262 18.6 2.00E-14 0.6 0.8 3.5 Beaver River Till monzogranite 454805 4934872 41.0 1.31E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 424075 4926438 134.8 1.46E-13 0.4 0.5 1.1 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM08-011 | Beaver River Till | monzogranite | 420725 | 4944607 | 34.8 | 1.33E-11 | 1.6 | 1.8 | 4.3 | 36.9 |
| Beaver River Till monzogranite 449262 4942690 23.2 1.35E-11 1.1 1.5 5.5 Beaver River Till monzogranite 447766 4942262 18.6 2.00E-14 0.6 0.8 3.5 Beaver River Till monzogranite 441274 4935057 38.6 1.14E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.9 2.4 5.2 | HRM09-001 | Beaver River Till | monzogranite | 450191 | 4941585 | 10.7 | 3.24E-13 | 1.3 | 1.4 | 6.2 | 3.8 |
| Beaver River Till monzogranite 447766 4942262 18.6 2.00E-14 0.6 0.8 3.5 Beaver River Till monzogranite 441274 4935057 38.6 1.14E-12 0.7 0.8 2.5 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 456984 4926438 134.8 1.46E-13 0.4 0.5 1.1 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-002 | Beaver River Till | monzogranite | 449262 | 4942690 | 23.2 | 1.35E-11 | 1:1 | 1.5 | 5.5 | 24.4 |
| Beaver River Till monzogranite 441274 4935057 38.6 1.14E-12 0.7 0.8 2.5 Beaver River Till monzogranite 454805 4934872 41.0 1.31E-12 1.0 1.5 4.1 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-003 | Beaver River Till | monzogranite | 447766 | 4942262 | 18.6 | 2.00E-14 | 9.0 | 8.0 | 3.5 | 4.7 |
| Beaver River Till monzogranite 454805 4934872 41.0 1.31E-12 1.0 1.5 4.1 Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-004 | Beaver River Till | monzogranite | 441274 | 4935057 | 38.6 | 1.14E-12 | 0.7 | 8.0 | 2.5 | 19.0 |
| Beaver River Till monzogranite 456984 4927659 65.2 1.63E-12 1.7 2.4 5.6 Beaver River Till monzogranite 453634 4926438 134.8 1.46E-13 0.4 0.5 1.1 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-008 | Beaver River Till | monzogranite | 454805 | 4934872 | 41.0 | 1.31E-12 | 1.0 | 1.5 | 4.1 | 20.8 |
| Beaver River Till monzogranite 453634 4926438 134.8 1.46E-13 0.4 0.5 1.1 Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-009 | Beaver River Till | monzogranite | 456984 | 4927659 | 65.2 | 1.63E-12 | 1.7 | 2.4 | 5.6 | 35.1 |
| Beaver River Till monzogranite 424075 4948850 58.0 2.36E-12 1.9 2.4 5.2 Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-010 | Beaver River Till | monzogranite | 453634 | 4926438 | 134.8 | 1.46E-13 | 0.4 | 0.5 | 1.1 | 46.5 |
| Beaver River Till monzogranite 428058 4952803 18.1 8.39E-12 1.6 0.5 4.7 | HRM09-011 | Beaver River Till | monzogranite | 424075 | 4948850 | 58.0 | 2.36E-12 | 1.9 | 2.4 | 5.2 | 34.2 |
| | HRM09-012 | Beaver River Till | monzogranite | 428058 | 4952803 | 18.1 | 8.39E-12 | 1.6 | 0.5 | 4.7 | 15.3 |

Notes: *clasts consist of 80% local (mixture of granite, slate, and msst), 20% erratics (mixture of North Mountain Formation, Cobequid Highlands, and Fundy and Windsor groups).

Appendix. Radon soil gas results from HRM (continued).

| Site ID | Till Sheet Name | Dominant Clast Type | utmE83 | utmN83 | Rn (kBq/m³) | Permeability (m^2) | K (pct) | eU (ppm) | eTh (ppm) | SRP Index |
|-----------|-------------------|------------------------|--------|---------|-------------|----------------------|---------|----------|-----------|-----------|
| HRM08-006 | Beaver River Till | c.g leucomonzogranite | 444427 | 4942847 | 27.3 | 1.41E-11 | 2.2 | 2.3 | 7.2 | 29.5 |
| HRM08-020 | Beaver River Till | c.g leucomonzogranite | 429975 | 4952069 | 49.9 | 1.07E-12 | 1.2 | 1.5 | 3.4 | 24.3 |
| HRM09-025 | Beaver River Till | c.g leucomonzogranite | 438330 | 4946447 | 17.4 | 4.22E-12 | 1.4 | 1.7 | 5.4 | 11.6 |
| HRM09-034 | Beaver River Till | c.g leucomonzogranite | 428016 | 4939025 | 22.0 | 3.93E-12 | 1.3 | 1.7 | 4.1 | 14.5 |
| HRM09-035 | Beaver River Till | c.g leucomonzogranite | 434454 | 4947329 | 71.6 | 2.37E-11 | 2.0 | 2.0 | 5.1 | 105.8 |
| HRM09-036 | Beaver River Till | c.g leucomonzogranite | 434504 | 4945656 | 23.1 | 1.81E-11 | 2.3 | 3.7 | 4.9 | 28.2 |
| HRM09-037 | Beaver River Till | c.g leucomonzogranite | 433291 | 4947074 | 150.8 | 1.10E-11 | 2.0 | 4.5 | 3.2 | 149.9 |
| HRM09-038 | Beaver River Till | c.g leucomonzogranite | 437742 | 4929404 | 75.4 | 4.82E-13 | 1.2 | 1.7 | 3.6 | 31.6 |
| HRM09-039 | Beaver River Till | c.g leucomonzogranite | 428674 | 4944453 | 15.7 | 7.49E-12 | 1.3 | 1.9 | 3.7 | 12.6 |
| HRM09-040 | Beaver River Till | c.g leucomonzogranite | 443385 | 4942820 | 49.1 | 2.54E-12 | 1.5 | 2.3 | 4.1 | 29.4 |
| HRM08-010 | Beaver River Till | f.g. leucomonzogranite | 432958 | 4948884 | 104.4 | 6.43E-12 | 1.6 | 2.5 | 5.2 | 83.9 |
| HRM09-022 | Beaver River Till | f.g. leucomonzogranite | 432399 | 4950052 | 154.6 | 4.15E-12 | 2.3 | 3.7 | 4.2 | 107.9 |
| HRM09-023 | Beaver River Till | f.g. leucomonzogranite | 432141 | 4948500 | 28.9 | 9.34E-12 | 1.4 | 1.9 | 3.1 | 26.0 |
| HRM09-024 | Beaver River Till | f.g. leucomonzogranite | 433170 | 4948973 | 24.5 | 8.13E-12 | 1.4 | 2.0 | 3.4 | 20.8 |
| HRM09-026 | Beaver River Till | f.g. leucomonzogranite | 433637 | 4949059 | 18.6 | 8.44E-13 | 2.6 | 4.7 | 4.6 | 8.3 |
| HRM09-027 | Beaver River Till | f.g. leucomonzogranite | 432299 | 4948661 | 21.9 | 3.68E-12 | 1.2 | 1.7 | 2.9 | 14.2 |
| HRM09-028 | Beaver River Till | f.g. leucomonzogranite | 432613 | 4948920 | 41.0 | 1.72E-12 | 1.1 | 1.5 | 2.8 | 22.2 |
| HRM09-029 | Beaver River Till | f.g. leucomonzogranite | 440634 | 4945605 | 52.8 | 2.63E-12 | 1.3 | 2.0 | 3.6 | 32.0 |
| HRM09-030 | Beaver River Till | f.g. leucomonzogranite | 440340 | 4945402 | 19.8 | 1.78E-12 | 0.7 | 1.0 | 3.1 | 10.5 |
| HRM09-031 | Beaver River Till | f.g. leucomonzogranite | 434042 | 4948600 | 43.3 | 5.52E-12 | 6.0 | 1.9 | 2.6 | 32.5 |
| | | | | | | | | | | |

Notes: c.g. = coarse-grained; f.g. = fine-grained.