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ABSTRACT

Southern New Brunswick consists of a collage of fault-bounded belts of Late Neoproterozoic igneous and metamorphic rocks, early Paleozoic sedimentary, metamorphic and igneous units, and overlying Carboniferous and locally Triassic sedimentary rocks. The area also contains the boundary between Avalonia and Ganderia as interpreted in the northern Appalachian orogen. New detrital zircon ages reported here provide improved understanding of depositional ages and provenance of diverse Neoproterozoic to Carboniferous rocks in this complex area. Detrital zircon data from samples with Neoproterozoic maximum depositional ages indicate a dominantly Gondwanan provenance with strong influence from the Amazonian craton. However, quartzite from The Thoroughfare Formation on Grand Manan Island contains dominanly 2 Ga zircon grains, consistent with derivation from the West African craton. The age spectrum is similar to that of the Hutchins Island Quartzite in the Isleboro block in Penobscot Bay, Maine, strengthening the possibility of correlation between the two areas. Cambrian samples also show prominent peri-Gondwanan provenance with strong influence from Ediacaran to early Cambrian arc magmatism. The maximum depositional ages of these samples are consistent with previous interpretations of Cambrian ages based on fossil correlations and field data. A Carboniferous sample from Avalonia shows a significant contribution from Devonian magmatism as the youngest detrital component, although its depositional age based on field relationships is Carboniferous. The results exemplify the need to integrate multiple datasets in making interpretations from detrital zircon data.

RÉSUMÉ

Le sud du Nouveau-Brunswick est constitué d'un collage de ceintures délimitées par des failles de roches ignées et métamorphiques du Néoprotérozoïque tardif, d'unités sédimentaires, métamorphiques et ignées du Paléozoïque précoce, ainsi que de roches sédimentaires sus-jacentes du Carbonifère et, par endroits, du Trias. Le secteur comprend également la frontière établie entre Avalonia et Ganderia selon son interprétation à l'intérieur de la partie septentrionale de l'orogène des Appalaches. De nouvelles datations de zircon détritique rapportées ici permettent une meilleure compréhension des âges sédimentaires et de la provenance des diverses roches néoprotérozoïques à carbonifères dans ce secteur complexe. Les données relatives au zircon détritique obtenues des échantillons faisant état d'âges sédimentaires remontant au maximum au Néoprotérozoïque signalent une provenance en prédominance gondwanienne avec une forte influence du craton amazonien. Le quartzite de la Formation The Thoroughfare sur l'île Grand Manan renferme toutefois prédominament des grains de zircon de 2 Ga, ce qui correspond à une dérivation du craton de l'Afrique occidentale. Le spectre de l'âge est similaire à celui du quartzite de l'île Hutchins à l'intérieur du bloc Isleboro dans la baie Penobscot, au Maine, ce qui renforce la possibilité d'une corrélation entre les deux secteurs. Les échantillons du Cambrien font eux aussi état d'une provenance périgondwanienne prononcée, marquée d'une forte influence d'un magmatisme d'arc de l'Édiacarien au Cambrien précoce. Les âges sédimentaires maximaux de ces échantillons correspondent aux interprétations antérieures des datations du Cambrien basées sur des corrélations de fossiles et des données d'échantillonnage sur le terrain. Un échantillon du Carbonifère provenant d'Avalonia révèle une contribution prononcée du magmatisme

dévonien à titre d'élément détritique le plus récent, mais son âge sédimentaire le situe au Carbonifère d'après les relations établies sur le terrain. Les résultats illustrent la nécessité d'une intégration de plusieurs ensembles de données pour effectuer des interprétations à partir de données provenant de zircon détritique.

[Traduit par la redaction]

INTRODUCTION AND GEOLOGICAL SETTING

Southern New Brunswick consists of a complex assemblage of three fault-bounded belts of mainly Neoproterozoic rocks with minor Paleozoic rocks termed (from southeast to northwest) Caledonia, Brookville, and New River, as well as five belts of mainly lower Paleozoic rocks termed Kingston, Mascarene, Annidale, St. Croix, and Fredericton (Fig. 1a). The area spans the boundary between Avalonia and Ganderia as defined by Hibbard et al. (2006), who placed the northern edge of Avalonia at the Caledonia-Clover Hill Fault that forms the boundary between the Caledonia and Brookville belts (Fig. 1b). In this interpretation most of New Brunswick, including Grand Manan Island, is considered part of Ganderia, as is adjacent New England (e.g., Fyffe et al. 2011; van Staal et al. 2011), whereas Avalonia extends offshore into the Bay of Fundy from the Caledonia belt of southern New Brunswick, underlies the Gulf of Maine, and re-emerges onshore in the Boston area of southeastern New England (Thompson et al. 2010).

The definition of Ganderia and Avalonia in the northern Appalachian orogen is based on multiple lines of evidence including differences in stratigraphy, magmatic and metamorphic histories, isotopic characteristics, and (increasingly) detrital zircon signatures which can provide information regarding source areas for present components of Ganderia and Avalonia during their pre-Appalachian evolution. The distribution of ages of detrital zircon grains in sedimentary units is a means of comparing units of similar age located in different areas, as well as an indicator of provenance. In addition, the youngest detrital zircon grains give an indication of maximum depositional age, significant in units where other age constraints are minimal or lacking. All three of these applications have relevance in southern New Brunswick, and this technique has been applied previously to rock units in that area as well as in adjacent parts of New England and Nova Scotia (Barr et al. 2003a, 2012; Fyffe et al. 2009; Satkoski et al. 2010; Dokken et al. 2018; Ludman et al. 2018). The significance of differences in detrital zircon populations between Ganderia and Avalonia is an ongoing debate, and the database of detrital zircon U-Pb data for both pre- and post-Appalachian strata is growing. The results reported in this paper add to that database, which may ultimately help to resolve questions about the initial relationships among the fault-bounded geological belts of southern New Brunswick (Fig. 1a).

As in other Appalachian detrital zircon studies the interpretations in the present study have to deal with difficulties in interpreting Meso- to Neoproterozoic zircons that could have multiple sources, for example the commonly encountered 1.4 - 1.0 Ga zircon grains which can be derived from any number of long-lived magmatic systems in arcs and continental settings associated with the Grenville orogen in either the West African or Amazonian craton. This difficulty is magnified in syn- and post-collisional strata because of potential contributions from the Laurentian craton with its very large area of Grenville-age magmatic activity. In addition, in Paleozoic samples the Proterozoic signatures are obscured by extensive contributions from syn-accretional and collisional magmatic systems active through the Ordovician to Devonian history of the Appalachian orogen.

New LA-ICP-MS detrital zircon age spectra are reported here for six sedimentary and metasedimentary rock units in southern New Brunswick. This study includes samples NB12-314 and NB12-315 of Cambrian age in the New River belt (Figs. 2, 3), one sample GM10-01 of uncertain Precambrian age and two samples NB16-356 and NB16-358 of Neoproterozoic to early Cambrian age from Grand Manan Island (Fig. 4), and sample BL15-01 from the Carboniferous Balls Lake Formation near the city of Saint John (Fig. 5). The new data are compared to previously published data, and in combination, shed light on stratigraphic and terrane relations in the area.

METHODS

Detrital zircon U-Th-Pb laser-ablation, inductively coupled plasma mass spectrometry (LA-ICPMS) analyses were conducted at the Texas A & M University R. Ken Williams Radiogenic Isotope Geosciences Laboratory (samples GM10-01, NB12-314, and NB12-315) and the University of New Brunswick (samples BL15-01, NB16-356, and NB16-358).

At Texas A & M University, zircon grains were concentrated from rock samples using standard crushing and density separation (jaw and disc crusher, Wilfley table, heavy liquids) methods. Zircon grains were separated from other dense minerals by hand-picking in a petrie dish under a binocular microscope, but no further separation was performed on the bulk zircon aliquot recovered from heavy liquids. The bulk zircon aliquot was piled and quartered repeatedly in the petrie dish to obtain a sub-sample of about 1000 grains. This zircon sub-sample was mounted on double-sided tape and encased in a 2.5 cm diameter epoxy disc, along with fragments of NIST 610, NIST 612, one primary reference material (zircon 91500; Wiedenbeck et al. 1995) and two secondary reference materials (zircons R33 and FC-1; Black et al. 2004 and Paces and Miller 1993, respectively). The disk was abraded with 2000 grit sandpaper to expose the interior of zircon grains and polished to 0.25 µm on a diamondsuspension lap wheel. LA-ICPMS analyses were conducted



Figure 1. (a) Simplified geological map of part of southwestern New Brunswick after Barr *et al.* (2014c). Boxes indicate the locations of the four areas shown in Figures 2–5 from which detrital zircon ages are presented. Arrow indicates the location of the detrital zircon sample from the Almond Road Group in the New River terrane reported by Johnson *et al.* (2018). Fault abbreviations: CCFZ, Cobequid-Chedabucto fault zone; CCHF, Caledonia-Clover Hill Fault. (b) Divisions of the northern Appalachian orogen after Hibbard *et al.* (2006) showing the location of the study area (black rectangle).

on a ThermoScientific iCAP RQ quadrupole mass spectrometer running in standard high-sensitivity (STDS) mode connected to an esi/NWR 193 nm 4 ns pulsed excimer laser system equipped with a two-volume sample cell (Tv2). Instrument settings and run parameters are given in Table A1 and analytical data in Table A2. Data are reduced using Iolite



Figure 2. Geological map of the Long Reach area in the New River belt showing the location of dated quartz arenite sample NB12-314. Map is modified from Figure 5 in Barr *et al.* (2014c).

v. 3.5 (Paton *et al.* 2011) under the U–Pb Geochron4 data reduction scheme (Paton *et al.* 2010). Analysis of the primary reference material, each treated separately as an unknown, indicates an internal analytical reproducibility of U–Pb ages to better than 0.7%. The average accuracy of secondary reference materials (Table A2) is better than 2.25% (FC-1) and better than 1.5% (R33).

For the dating done at the University of New Brunswick (UNB), rock samples were sent to Overburden Drilling Management in Ottawa, Ontario, for electro-pulse disaggregation



Figure 3. Geological map of the Beaver Harbour area showing the location of dated quartz arenite sample NB12-315. Map is modified from Barr *et al.* (2014a).

and zircon separation. Zircon grains were then hand-picked at Cape Breton University and taken to UNB where they were mounted in epoxy-covered thin sections polished to expose the centres of the zircon grains and imaged using cold cathodoluminescence to identify internal zoning and inclusions. These images were used to select ablation points (30 μ m diameter), avoiding any visible inclusions, cracks, or other imperfections. U and Pb isotopic compositions were measured using the Resonetics S-155-LR 193 nm Excimer laser ablation system connected to an Agilent 7700x quadrupole inductively coupled plasma – mass spectrometer, following the procedure outlined by McFarlane and Luo (2012) and Archibald *et al.* (2013). Data reduction was done in-house using Iolite software (Paton *et al.* 2011) to process the laser output into data files, and further reduced for U–Pb geochronology using VizualAge (Petrus and Kamber 2012). Data were sorted by % concordance (²⁰⁶Pb/²³⁸U versus ²⁰⁷Pb/²³⁵U), and by the % of radiogenic Pb in the grains as calculated using VizualAge (Table A3, A4).

In all cases we present probability distribution histograms based on ²⁰⁶Pb/²³⁸U dates for grains <1000 Ma and ²⁰⁷Pb/²⁰⁶Pb dates for >1000 Ma, and show all grains that are between 95

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and 101% concordant. To determine the youngest age represented in each sample we use only clusters of more than 3 grains with ages that overlap within error and are 98–101% concordant. Using only near-concordant grains that overlap within error is a conservative approach which serves to reduce the possibility of misrepresenting the maximum depositional age as too young by using single grains that may have experienced Pb loss (Dickinson and Gehrels 2010).

For each dated sample, the geological setting is described, followed by the results and interpretation. A subsequent Discussion deals with the oveall implications of the new data.

SAMPLE NB12-314 - CHEYNE SETTLEMENT ROAD

Geological setting

Quartz arenite sample NB12-314 was collected from an outcrop on Cheyne Settlement Road in the Long Reach area of the New River belt (Fig. 2). Cheyne Settlement Road crosses an enclave of Cambrian rocks, one of several such occurrences in the Long Reach area (Fig. 2). The Cambrian rocks overlie Late Neoproterozoic to early Cambrian volcanic rocks of the Belleisle Bay Group and have been correlated with the Saint John Group (Fig. 2). Matthew (1891) discovered the acrotretid brachiopod Linnarsonnia misera in grey sandstone at Belyeas Landing (now the "Public Landing" shown on Figure 2) about 600 m east of the sampled quartz arenite and Yoon (1970) later discovered trilobites at the same location which he suggested are consistent with a late early Cambrian age, consistent with the work of Boyce and Johnson (2004) based on newly collected material. Small black phosphatic shells tentatively identified as L. misera (R. Miller, personal communication, 2001) were discovered also in a sequence of dark grey shale, siltstone and very fine-grained, micaceous sandstone on Cheyne Settlement Road about 1.2 km west of Public Landing. Johnson (2001) assigned all of the rocks within the enclave, including the quartz arenite unit sampled for dating in the present study, to the Hanford Brook Formation of the Saint John Group (Fig. 2).

The dated sample is grey medium-grained quartz arenite. It is dominated by subangular to subrounded quartz grains and less than 10% silt/clay matrix. Feldspar, spherulitic volcanic, and quartzite clasts occur rarely.

Results

Zircon grains separated from sample NB12-314 display a wide range of sizes, morphologies, and colors. Most grains have abraded corners and edges and are rounded. The largest (~150 um diameter) and most highly rounded grains are

also commonly the most deeply colored in shades of pink and purple or tan. Other large (100–150 μ m long), more elongate zircon grains show light tan color. Relatively rare, small (50–100 μ m long), colorless crystals are acicular with sharp corners and tips.

A large percentage of the grains are discordant, and ablation profiles are consistent with Pb-loss being the dominant cause of discordance, as opposed to zircon grains with multiple age components. The main population of grains has ages between 480 and 540 Ma, with only four older grains between 1 and 3.2 Ga (Figs. 6a, b). Three grains have ²⁰⁶Pb/²³⁸U ages of ca. 450 Ma but they do not overlap within error and all are less than 98% concordant, our cut-off for calculating concordia ages as mentioned earlier, likely because of Pb loss. In contrast, a few grains have ages between 480 and 500 Ma that overlap within error, and three of these grains produce a calculated concordia age of 487.5 ± 13 Ma with very high MSWD of 15 and probability near zero. Using only two grains produces a calculated concordia age of 485.8 ± 19 Ma with a slightly better MSWD of 10.7 and probability of 0.001. The weighted mean of 7 grains between 475 and 495 Ma is 486.8 \pm 6.1 at 95% confidence with MSWD = 2.6, and probability = 0.015 (Fig. 6a, inset). Overall, we consider that the best estimate of the maximum depositional age for the sediment is ca. 487 Ma (late Cambrian to Early Ordovician).

This age, although not well constrained, is considerably younger than the age of 508.05 ± 2.75 Ma reported for an ash bed in the Hanford Brook Formation in the Somerset Street section in the city of Saint John (Landing *et al.* 1998; Schmitz 2012). Based on fossils, the age of the Hanford Brook Formation spans the traditional early to middle Cambrian boundary, or in newer time scales, the boundary between Series 2 and 3 (Palacios *et al.* 2016) at about 509 Ma (Cohen *et al.* 2013 updated 2018).

SAMPLE NB12-315 - BUCKMANS CREEK

Geological setting

The Buckmans Creek Formation (e.g., Currie 1988) in the Beaver Harbour area of the New River belt (Fig. 3) is an assemblage of fault-bounded and internally faulted sedimentary and mafic volcanic rocks that are in places fossiliferous. They have been correlated with the Saint John Group of the Saint John area (Fig. 5), implying a link between the New River and Caledonia belts (e.g., Currie 1988; Tanoli and Pickerill 1988; Landing 1996; Johnson 2001; Landing *et al.* 2008). Landing *et al.* (2008) assigned these Cambrian rocks to the marginal platform of the late Proterozoic to early Paleozoic Avalon microcontinent. They identified the lower Cambrian Chapel Island and Random formations in the Buckmans Creek area, unconformably overlain by mafic

Figure 4. (previous page) Geological map of Grand Manan Island showing the location of dated samples NB16-356, NB16-358, and GM10-01. Map is modified from Fyffe (2014).



Figure 5. Geological map of the Saint John area showing the location of dated sample BL16-01, Map is modified from Park *et al.* (2014).

volcanic-dominated rocks which Landing *et al.* (2008) assigned to the "Wade's Lane Formation". This name appears to be an incorrect transcription of "Waites Lane" which is shown on road signs in the area and on topographic maps.

Landing et al. (2008) reported that the presence of late early Cambrian trilobites and small shelly taxa in the lowest part of their "Wade's Lane Formation" demonstrates a hiatus between rocks that they assigned to the Random Formation and those of their "Wade's Lane Formation". They interpreted the volcanic rocks in the Beaver Harbour section as the result of latest early to middle middle Cambrian pyroclastic volcanism, one of three known volcanic centers that extended 550 km along the northwest margin of the Avalon microcontinent. According to Landing et al. (2008), the volcanic rocks are overlain by grey-green mudstone and limestone of the Fossil Brook Member and black mudstone of the upper Manuels River Formation. However, given the uncertainty of long-distance correlations in a complex orogen, we continue to use the earlier established name Buckmans Creek Formation collectively for all these rocks.

Near the mouth of Buckmans Creek, the formation is separated from the plutonic rocks of the Beaver Harbour porphyry by a reverse dip-slip fault (Bartsch 2005). The Beaver Harbour porphyry yielded a U–Pb zircon age of 551 ± 1.2 Ma (Barr et al. 2014a). On its northwestern margin, the formation is in faulted contact with the ca. 620 Ma Blacks Harbour granite (Barr et al. 2003b; Bartsch 2005).

Dated quartz arenite sample NB12-315 is from the unit assigned to the Random Formation by Landing *et al.* (2008). The sample is light grey and consists of recrystallized quartz grains that are sutured and polygonal in places. It contains rare felsic volcanic and quartzite clasts, and almost no matrix.

Results

A total of 203 zircon grains were analyzed from sample NB12-315. The main population has ages from 510 to 590 Ma (Figs. 6c, d). Other grains give an almost continuous range of ages from 1 Ga to 2 Ga and a few grains lie between 2 and 3.2 Ga. The youngest 4 grains that overlap within



Figure 6. Probability density plots and histograms for U–Pb data: (a) Sample NB12-314; (b) Expanded view of the data between 400 and 650 Ma for sample NB12-314; (c) Sample NB12-315; (d) Expanded view of the data between 400 and 650 Ma for sample NB12-315; (e) Sample GM10-01. Inserts in (a) and (c) show weighted mean ages for the youngest population of concordant zircon grains in each sample. Data are from Appendix Table A1. Dates with discordance >10% are excluded from these diagrams.

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error have a calculated concordia age of 518.4 ± 2.8 Ma with MSWD = 6.7 and probability = 0.010. The calculated concordia age with 5 overlapping grains including one that is more discordant is 518.3 ± 4.7 Ma with much higher MSWD of 12.0 and lower probability of 0.001. The weighted mean of the same 5 grains is 517.2 ± 2.7 at 95% confidence with MSWD = 0.41 and probability = 0.80 (Fig. 6c, inset). Hence the maximum depositional age for this sample is interpreted to be ca. 517 Ma (Cambrian series 2; Cohen *et al.* 2013, revised 2018).

SAMPLE GM10-01 -THE THOROUGHFARE FORMATION

Geological setting

The Thoroughfare Formation of Grand Manan Island is exposed on Ross, Nantucket, and White Head islands off the southeastern coast (Fig. 4). It is composed of very thick- to thin-bedded, locally cross-bedded, white to light grey quartzite interbedded with grey to black carbonaceous shale. Where exposed on the western shore of The Thoroughfare, the contacts between the formation and volcanic sequences of the Priest Cove Formation are highly sheared and interpreted as thrust faults based on the presence of low-angle cleavages in the vicinity of their mutual boundaries (Fyffe 2014). The inferred age of The Thoroughfare Formation is late Proterozoic as suggested by Alcock (1948) who correlated the quartzite with quartzite interstratified with platformal stromatolitic carbonates of the Late Proterozoic Green Head Group in the Saint John area on the New Brunswick mainland, although the latter unit does not include carbonaceous shale and The Thoroughfare Formation lacks carbonate rocks, so the only rock type in common is the quartzite itself. The Thoroughfare Formation could be correlative with the Hutchins Island Quartzite in Penobscot Bay, Maine (Fig. 1b) which also has an inferred late Proterozoic age (Reusch et al. 2018).

The dated quartzite sample consists of recrystallized quartz grains that are rectangular and elongate parallel to a weak foliation. Granular quartz around the larger grains suggests that brittle deformation may have overprinted earlier ductile structures. Rare muscovite and tourmaline are also present.

Results

Sample GM10-01 is distinctive in that it contains only Paleoproterozoic and older zircon grains that are much older than the inferred Late Proterozoic stratigraphic age. Its detrital signature is unlike any others yet seen in New Brunswick, including the nearby Flagg Cove Formation (Fig. 3; Fyffe *et al.* 2009), but like those from samples from Georges Bank and Penobscot Bay inferred to represent sediments deposited on the West African Craton (Kuiper *et al.* 2017; Reusch *et al.* 2018). The biggest population of zircon grains has ages between 1.9 and 2.2 Ga, with another significant peak at ca. 2.5, and an almost continuous range of ages from 2.5 to 3.2 Ga (Fig. 6e). The youngest two grains are around 1.65 Ga, but they do not overlap within error and cannot be used for a concordia age. Based on these youngest grains the maximum depositional age of the sample may be less than 1.65 Ga but this estimate is not robust. The maximum depositional age based on the detrital zircon populations is better constrained at 1.9 Ga based on the major population peaks.

SAMPLE NB16-356 - LONG POND BAY FORMATION

Geological setting

The Long Pond Bay Formation is exposed along Long Pond Bay and on nearby Wood Island on southern Grand Manan Island (Fig. 4). The Long Pond Bay shoreline section consists of subaqueous hyaloclastic basalt flows, mafic volcanic breccia, peperitic basalt, green cherty mudstone, and medium- to thick-bedded wacke. On Wood and adjacent islands, amygdaloidal basalt flows, felsic tuff, and arkosic sandstone appear to have been deposited in shallower water and are associated with coarse-grained gabbroic rocks (Fig. 4). A sample from a rhyolitic tuff or high-level intrusion from Wood Island yielded few zircon grains that were interpreted by Miller et al. (2007) to indicate a maximum depositional age of ca. 588 Ma. The relatively undeformed features of the unit and its lithological similarities to Silurian units of the Mascarene terrane on the mainland (McLeod et al. 1994) led to the assumption of a Silurian age (Miller et al. 2007). However, Fyffe (2014) subsequently interpreted the Long Pond Bay Formation to be part of the Ediacaran-Cambrian Castalia Group, together with the Priest Cove Formation dated at 539 ± 3 Ma by Miller *et al.* (2007). Fyffe (2014) correlated the Long Pond Bay Formation with the Simpsons Island Formation in the New River terrane on the mainland which also yielded an age of 539 ± 4 Ma (Barr et al. 2003b).

Dated sample NB16-356 is from a grey sandstone unit in the Long Pond Bay shoreline section (Fig. 4). It is immature and matrix-supported and consists of angular quartz and less abundant plagioclase grains in a fine matrix of clay (sericite) and silt. Detrital muscovite and biotite altered to chlorite are also present.

Results

In this sample only 64 out of 145 grains are between 95 and 101% concordant and a further 22 grains are between 90 and 95% concordant. The largest population of zircon grains in sample NB16-356 is in the range between 690 and 600 Ma, with minor populations at around ca. 790 Ma, 1.1–1.2 Ga, and a few grains between 1.5–2 Ga (Figs. 7a, b). The concordia age of the youngest three grains that overlap is 614.6 ± 6.1 Ma with MSWD = 5.7 and probability (of concordance) = 0.017. The weighted mean of the youngest



Figure 7. Probability density plots and histograms for U–Pb data: (a) Sample NB16-356; (b) Expanded view of the data between 540 and 840 Ma for sample NB16-356; (c) Sample NB16-358; (d) Expanded view of the data between 300 and 900 Ma for sample NB16-358; (e) Sample BL15-01; (f) Expanded view of the data between 350 and 800 Ma for sample BL15-01. Note that the expanded-scale diagrams in (b), (d), and (f) have different scales. Inserts in (a), (c), and (e) show weighted mean ages for the youngest population of concordant zircon grains in each sample. Data are from Appendix Table A1. Dates with discordance >10% are excluded from these diagrams.

6 grains that overlap within error is 614.7 ± 4.6 at 95% confidence with MSWD = 0.67 and probability = 0.64 (Fig. 7a, inset). The interpreted maximum depositional age for this sample is therefore < 614 Ma. This result does not tighten the limited constraints on the depositional age of the Long Pond Bay Formation, previously suggested to be <588 Ma (Miller *et al.* 2007). However, the similarity of the dates from the youngest detrital grains to the U–Pb (zircon) ages of 617.6 ± 3.2 Ma and 618.3 ± 2.8 Ma for two tuffaceous samples from separate locations in the nearby Ingalls Head Formation (Fig. 4) suggest that the Ingalls Head Formation was the source of the detrital grains. The result is consistent with the inclusion of the Long Pond Bay Formation in the upper part of the Neoproterozoic to Lower Cambrian Castalia Group (Fyffe 2014).

SAMPLE NB16-358 - ROSS ISLAND FORMATION

Geological setting

The Ross Island Formation underlies the greater part of Ross and White Head islands near the southeastern coast of Grand Manan (Fig. 4). It comprises interstratified plagioclase-phyric mafic and intermediate flows and breccias intruded by numerous diabase dykes. The flows are locally pillowed and interbedded with green laminated siltstone. They range from basalt to andesite based on chemical composition, and are calc-alkalic, formed in a volcanic arc setting (Hilyard 1992; Hewitt 1993; Hodgins 1994; Pe-Piper and Wolde 2000; Black 2005). The Ross Island Formation appears to be truncated by faults that separate it from quartzite of The Thoroughare Formation on the northern tip of Ross Island and western tip of White Head Island (Fig. 4). The formation had no previous age constraints but was assumed to be part of the Precambrian to early Cambrian Castalia Group (Fyffe 2014).

Dated sample NB16-358 is dark grey laminated siltstone that occurs in peperitic relationship with basalt near the ferry terminal on the western shore of White Head Island. The sample is fine-grained and contains abundant plagioclase. Its swirly matrix contains abundant sericite and has an ashlike appearance.

Results

NB16-358 is very poor in zircon and only had 25 grains analyzed, 20 of which are betwee 95 and 101% concordant. The largest populations of zircon grains are in the range between ca. 580 Ma and 630 Ma, with a small group at ca. 700 Ma, and a few grains between 1 and 2 Ga (Figs. 7c, d). A single grain at ca. 320 Ma is not considered to be a reliable indicator of maximum depositional age. The concordia age of the youngest three grains that overlap is 585.5 ± 8.4 Ma with MSWD = 2.6 and a probability (of concordance) = 0.11. The weighted mean of the same four grains is 580 ± 11 at 95% confidence with MSWD = 0.26, and probability = 0.86. Based on these data, the maximum depositional age for this sample is interpreted to be ca. 580 Ma, similar to that of the Long Pond Bay Formation as determined by Miller *et al.* (2007). This age is consistent with the suggestion by Fyffe (2014) that the volcanic rocks of the Ross Island Formation represent a proximal facies of the Priest Cove Formation.

SAMPLE BL15-01 - BALLS LAKE FORMATION

Geological setting

The Balls Lake Formation is a coarse clastic sedimentary unit in the Saint John area that is interpreted currently as the lower unit of the Upper Carboniferous Cumberland Group (Fig. 5). However, traditionally it was included in the Mispec Group as the middle formation, underlain by basaltic and sedimentary rocks of the West Beach Formation and overlain by plant-bearing lithic arenite of the Lancaster Formation. The sequence was considered conformable and the entire group regarded as Mississippian(?) to Pennsylvanian or Pennsylvanian based on plant remains in the Lancaster Formation (e.g., Hayes and Howell 1937; Alcock 1938). Plint and van der Poll (1982) reassigned the Balls Lake and Lancaster formations to the Cumberland Group and Park et al. (2014) showed that the West Beach Formation and the laterally correlative(?) Taylors Island Formation are part of the allochthonous Partridge Island block and not part of the stratigaphy of the Cumberland Group (Fig. 5). In the Calvert Lake area southeast of Saint John, rocks of the Partridge Island block are contained in a klippe, preserved in a synform in the Balls Lake Formation that plunges gently west-southwest. The conglomerate-sandstone-mudstone sequence of the surrounding Balls Lake Formation is overturned to the south in the footwall of the Calvert Lake klippe along its southern contact, consistent with thrust transport toward the south-southeast. The Balls Lake Formation has no direct biostratigraphic controls on its age.

The dated sample is typical reddish-grey sandstone from the Balls Lake Formation in the overturned section on Bayshore Drive. It contains subangular quartz and plagioclase in a sericitic matrix that contain abundant carbonate cement. The quartz grains are angular to subangular and varied in size and shape. Detrital muscovite and opaque phases are abundant.

Results

The largest populations of zircon grains in sample BL15-01 are in the range between ca. 430 and 390 Ma (Figs. 7e, f). Smaller groups of ages occur at ca. 550 Ma, 600 Ma and 1 Ga, with a few older grains between 1 Ga and 2 Ga. The youngest 5 grains that overlap within error have a calculated concordia age of 397.3 ± 1.9 Ma with MSWD= 5.0, and probability (of concordance) = 0.025. The weighted mean of the same 5 grains is 396.5 ± 1.9 Ma at 95% confidence with MSWD = 0.78 and probability = 0.54 (Fig. 7e, inset). Based on these data, the maximum depositional age for this sample is interpreted to be ca. 396 Ma, much older than the inferred Late Carboniferous depositional age for the formation based on field relationships. The lack of Late Devonian– Early Carboniferous ages indicates that the Partridge Island block, which contains volcanic and plutonic rocks of that age, was not providing debris to this unit of the Balls Lake Formation. The Middle Devonian – Silurian zircon grains in the sample could have been derived from any number of plutonic suites both locally and farther afield.

DISCUSSION

Depositional ages

The depositional ages of all six samples included in this study are equivocal based on other evidence, and hence the maximum depositional ages described above based on the youngest zircon populations are potentially important. However, as in all detrital zircon studies, the data are viewed in combination with field and other evidence because of the potential for Pb loss which can move zircon ages to younger points along concordia (e.g., Dickinson and Gehrels 2010), as well as the possibility of inclusion of second-cycle detritus or lack of zircon sources close in age to the deposition of sediment. However, even with these caveats in mind, the detrital zircon U–Pb data provide valuable information about sedimentary provenance and maximum depositional ages. The samples are discussed here in reverse age order.

The Silurian and younger populations present in sample BL15-01 from the Balls Lake Formation include prominent populations of Early and Middle Devonian zircon grains but no younger grains, although the depositional age of the Balls Lake Formation is Carboniferous based on stratigraphic and field relationships (e.g., Park et al. 2014). A similar pattern of Carboniferous units with Devonian zircon grains as their youngest populations was found in a study in the southern Appalachian orogen by Thomas et al. (2017) in which several Pennsylvanian units contain significant Devonian zircon populations but no younger grains. These well-documented examples are a reminder that "maximum deposition ages" provide only an upper limit on stratigraphic age. Pre-Devonian zircon grains are sparse in sample BL15-01 (Figs. 7e, f) and could be evidence for either Gondwanan or Laurentian source areas but could also represent recycled detrital material from multiple sources.

Cheyne Settlement Road sample NB12-314 contains a significant Cambrian zircon population with a maximum depositional age of ca. 487 Ma and, therefore, latest Cambrian or younger (Figs. 6a, b). This maximum age is younger than the broadly "middle Cambrian" age generally assigned to the Hanford Brook Formation based on fossils and a U–Pb zircon date of 508.05 ± 2.75 Ma from an ash bed in the city of Saint John (Landing *et al.* 1998; Schmitz 2012). Although more work needs to be done in order to investi-

gate this apparent age enigma, it is possible that the Cheyne Settlement Formation is correlative instead with the Snider Mountain Formation in the Almond Road Group which occurs in the New River belt to the northeast (Fig. 1a). The youngest zircon population in quartz arenite in the Snider Mountain Formation is ca. 530 Ma, and the age of the upper sequence that contains feldspathic quartz arenite near its base is constrained by a cross-cutting pluton that gave an age of 475.4 \pm 1.6 Ma (Johnson *et al.* 2018). It is possible that the Cheyne Settlement sample exemplifies the gradual younging of quart arenite deposition within the same unit outward from the platform during protracted rifting and opening of the ocean basin along the Gondwanan margin as illustrated by Johnson *et al.* (2018).

The sample from Buckmans Creek (Fig. 3) also has a significant Cambrian zircon population but the youngest population (maximum depoisitional age) is older at ca. 517 Ma (Cambrian series 2). Landing *et al.* (2008) interpreted the dated quartz arenite unit at Buckmans Creek to be part of the Random Formation. The age of that formation in the Saint John area (where it is historically known as the Glen Falls Formation) is constrained by volcanic ash beds with ages of ca. 528 Ma in the underlying Ratcliffe Brook Formation and ca. 508 Ma in the overlying Hanford Brook Formation. Hence the maximum depositional age of 517 Ma for sample NB12-315 is consistent with these age constraints.

In contrast to these early Paleozoic samples, the samples from the Long Pond Bay and Ross Island formations (Figs. 7a–d) do not have Cambrian or younger zircon grains and hence their maximum depositional ages based on zircon data alone appear to be Neoproterozoic. The data are broadly consistent with previous interpretations of these units as Neoproterozoic but do not narrow down the depositional age greatly, especially for the Long Pond Bay Formation, due to the small number of zircon grains that yielded concordant results. However, the results are consistent with the interpretations of Fyffe (2014) who included the Long Pond Bay Formation in the upper part of the Neoproterozoic to Lower Cambrian Castalia Group and suggested that the volcanic rocks of the Ross Island Formation are a proximal facies of the Priest Cove Formation of the Castalia Group (Fig. 4).

Provenance implications

To facilitate comparison of datasets of various sizes, data from the present study together with previously published detrital age data for samples from Avalonia and Ganderia in southern New Brunswick are displayed on probability plots normalized for the number of dates (Figs. 8, 9). Because older grains are typically much less abundant than Ediacaran grains and hence tend to be produce less prominent peaks on the probability plots (Fig. 8), the normalized plots in Figure 9 were made using only dates older than 900 Ma. Except for three samples (NB06-232, NB12-314, and NB16-358) in which the number of grains with dates >900 Ma is small (<10), the data give reasonable signatures for comparison of Mesoproterozoic and older zircon signatures among samples (Fig. 9).



Figure 8. Normalized probability distribution **f**or the six detrital zircon samples of this study in comparison to other samples from southern New Brunswick from Barr *et al.* (2012, 2014b), Johnson *et al.* (2018), Fyffe *et al.* (2009), and Satkoski *et al.* (2010). Data are normalized against the total number of concordant dates for each sample.



Figure 9. Normalized probability distribution using only ages >900 Ma for the six detrital zircon samples of this study in comparison to other samples from southern New Brunswick from Barr *et al.* (2012, 2014b), Johnson *et al.* (2018), Fyffe *et al.* (2009), and Satkoski *et al.* (2010). Data are normalized against the total number of concordant dates >900 Ma for each sample.

With the exception of sample GM10-01 from The Thoroughfare Formation, all of the samples are characterized by prominent Ediacaran peaks in zircon ages (Fig. 8). Such peaks are characteristic of sedimentary rocks from Gondwanaderived terranes and reflect the widespread pan-African igneous activity related to the assembly of the Gondwanan continent (e.g., Satkoski et al. 2010; Pollock et al. 2009, 2015; Dokken et al. 2018; Ludman et al. 2018). It is difficult to assess the significance of the variations in the position of the Ediacaran peak or of the spread in Ediacaran ages in terms of specific provenance areas in Gondwana because even samples from a single belt or stratigraphic unit can display significant differences, as has been documented in the Ganderian parts of New Brunswick, Nova Scotia, and Newfoundland (e.g., Fyffe et al. 2009; Satkoski et al. 2010; Barr et al. 2012; van Rooyen et al. 2019).

In addition to the Ediacaran peak somewhere between 539 Ma and 619 Ma, most samples show a scatter of older Neoproterozoic ages back to about 900 Ma, although such older Neoproterozoic ages are notably absent in the Cheyne Settlement Road sample (Fig. 8). In general, Grenville-age (1.0-1.2 Ga) peaks are not present in the samples of this study or those compiled from previous studies (Fig. 9), indicating that Laurentian sources were not significant contributors to these sediments. Also lacking in most samples are prominent "Eburnean" (2.0 -2.2 Ga) peaks, generally considered indicative of African sources. Exceptions include the sample from The Thoroughfare Formation on Grand Manan Island, in which that peak is dominant, and the sample from the nearby Flagg Cove Formation (data from Fyffe et al. 2009) which likely derived sediment from The Thoroughfare Formation or equivalent units. In general, Ganderian samples have more abundant Mesoproterozoic peaks than Avalonian samples, a pattern that is generally viewed as indicating Amazonian provenance (e.g., Barr et al. 2014b) but all of the Avalonian samples have some Mesoproterozoic peaks and some Ganderian samples, especially those from Grand Manan Island, have relatively few Mesoproterozoic peaks (Fig. 9).

The interpretation of Mesoproterozoic zircon provenance is challenging as illustrated in the Fredericton trough in New Brunswick and Maine northwest of the study area. Although the Fredericton trough is farther outboard of the Gondwanan margin within Ganderia than the current study areas (Fig. 1a), it provides a comparison dataset for areas to the southeast. Ludman et al. (2017, 2018) suggested that the Fredericton trough represents an independent basin that was not linked to the more southern New England basins, and interpreted the detrital zircon signatures as being derived from dominantly Gondwanan sources. In contrast, Dokken et al. (2018) documented more mixed zircon provenance signature with significant Laurentian contributions. The differences in detrital zircon signatures are likely the result of along-strike variations in the source terranes, and support interpretations that Ganderia may have been a collection of continental fragments that accreted to the Laurentian margin at different times rather than forming one coherent crustal block (Waldron *et al.* 2014, 2018, 2019; Pothier *et al.* 2015).

In Avalonia, Barr et al. (2012) noted a change in the provenance of detrital zircon grains through time, Neoproterozoic units being characterized by lack of zircon grains with ages between 2.2 and 1.9 Ga, with the exception of a small peak at 2.0 Ga in the Neoproterozoic Broad River Group in the Caledonia belt (Fig. 9). By the early Cambrian zircon grains of this age are more abundant. Fyffe et al. (2009) noted a similar trend in Neoproterozoic to Tremadocian sedimentary units in Ganderia, with 2.2 to 1.9 Ga ages becoming much more abundant overall in Cambrian-Ordovician samples. However, exceptions to the trend occur in Cambrian samples from both Ganderia and Avalonia. For example, a quartz arenite sample from the lower Cambrian Glen Falls Formation (Random Formation of Landing and Westrop 1998) in the Avalonian Caledonia belt (Fig. 8) contains few zircon grains ages between 2.2 to 1.9 Ga, and the dominant age population is ca. 537 Ma (Barr et al. 2012). The quartzite sample from the early Cambrian Matthews Lake Formation in the Ganderian New River belt (Fig. 8) also lacks zircon grains with ages between 2.2 and 1.9 Ga and is dominated by a single statistical age population at 539 Ma (Fyffe et al. 2009). The abundant volcanic rocks in the ca. 540 Ma Belleisle Bay Group in the New River belt are the most obvious source of the ca. 539 Ma zircon grains in the Matthews Lake quartzite, and along with the voluminous ca. 540 Ma plutonic rocks in the Brookville belt are the closest possible sources for the ca. 537 Ma zircons in the Glen Falls Formation, although ⁴⁰Ar/³⁹Ar cooling ages show that the Brookville plutons were not exposed at the time when the Glen Falls Formation was deposited (Dallmeyer and Nance 1992; White 1996).

The absence of Mesoproterozoic and Neoproterozoic zircon grains in the quartzite samples from The Thoroughfare Formation is intriguing. Grains of those ages form the dominant populations in every other sample in this study, and in every other sedimentary sample from the region (Fig. 8). It is one of only 3 northern Appalachian samples known to have this type of signature, one from drill core recovered from Georges Bank, underlying Mesozoic sedimentary rocks (Kuiper et al. 2017) and the other from the Hutchins Island Quartzite in the Islesboro fault block in Penobscot Bay in coastal Maine (Reusch et al. 2018). As noted by Kuiper et al. (2017) and Reusch et al. (2018) these detrital signatures, with a predominant population at ca. 2.0 Ga and a small peak between ca. 2.8 Ga and 2.4 Ga, are remarkably similar to that of the Paleoproterozoic Taghdout Quartzite in Morocco on the West African craton. Similar peaks are also present in the spectrum for the Flagg Cove Formation reported by Fyffe et al. (2009), although that sample also contains abundant Mesoproterozoic, Neoproterozoic, and Paleozoic grains. Given its proximity, The Thoroughfare Formation seems the most likely source of the Paleoproterozic grains in the Flagg Cove Formation. The detrital spectrum is very different from that of the Ashburn Formation of the Green Head Group in the Brookville belt, which like

other units of that belt (Martinon Formation and Brookville paragneiss) are dominated by Mesoproterozoic zircon grains (Fig. 8). This calls into question the previous correlation (e.g., Alcock 1948) of The Thoroughfare Formation with the Green Head Group and suggests that correlation with the Isleboro fault block in Penobscot Bay may be more likely.

CONCLUSIONS

New U-Pb data from detrital zircon grains in six clastic sedimentary and metasedimentary samples from Ganderian and Avalonian terranes in southern New Brunswick show both similarities and differences in Ediacaran and older age patterns. Like previously published data from southern New Brunswick, four of the samples (BL15-01, NB12-315, NB16-356, NB16-358) have prominent Late Ediacaran to earliest Cambrian zircon age populations, but the position of the modal peak varies from ca. 548 Ma to 618 Ma. The fifth sample (NB12-314) has an early Cambrian peak at ca. 522 Ma, and the sixth sample (GM10-01) has only Paleoproterozoic peaks (Fig. 8). Some samples show a smattering of ages back to ca. 800, but generally lack 800-1200 Ma zircon grains. The samples vary widely in their abundances of older Mesoproterozoic and Paleoproterozoic grains, and a few Archean zircon grains are present in some samples. No consistent differences are apparent between Avalonian and Ganderian samples. Because Gondwanan sources areas contain a wide range of ages which are broadly similar, combined with the many variables inherent in sediment erosion, transport, deposition, and recycling, the use of detrital zircon age signatures to interpret from which part of Gondwana the Gondwana-derived components of the Appalachian orogen were derived may not be possible.

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Editorial responsibility: David P. West, Jr.

APPENDIX

Table A1. Instrument settings and run parameters for analyses completed at Texas A & M University.

laser	esi/NWR 193 nm 4 ns excimer
background/washout times	14 s /8 s
laser repetition rate	15 Hz
spot size/shape	30 μm / circle
fluence	3.25 J cm ⁻²
carrier/makeup gas	0.6 l/min He, 0.8 l/min Ar
mass spectrometer	Thermo Scientific iCAP RQ
plasma RF power	1550 W
total duty cycle	195 ms
isotopes measured (dwell times in ms)	${}^{48}\text{Ti} (10), {}^{88}\text{Sr} (10), {}^{96}\text{Zr} (2.5), {}^{179}\text{Hf} (2.5), {}^{202}\text{Hg} (10), {}^{204}\text{Pb} (20), {}^{206}\text{Pb} (20), {}^{207}\text{Pb} (50), {}^{208}\text{Pb} (10), {}^{232}\text{Th} (10), {}^{232}\text{Th} (10), {}^{235}\text{U} (20), {}^{238}\text{U} (10), {}^{232}\text{Th} {}^{16}\text{O} (10), {}^{238}\text{U} {}^{16}\text{O} (10)$

	% con		88.2	89.7	73.8	9.99	94.6	97.7	9.96	86.4	96.9	92.4	95.1	99.3	38.8	83.4	97.8	87.7	50.6	88.4	97.1	98.0	99.7	98.2	99.0	91.3	85.5	99.2	89.0	92.6	35.7	95.4	73.4	90.4	41.6	37.2	100.5	77.0	64.2	96.0
	$\pm 2\sigma^2$		14	13	11	7.2	16	13	17	14	23	8.9	16	6.7	30	79	13	9.1	29	13	7.5	11	7.3	7.1	22	7.7	13	6.8	38	14	59	11	8	19	75	18	8.8	17	25	9.6
	⁰⁶ Pb/ ²³⁸ U		486	503	496.1	512.9	490	500	519	504	1877	499.9	1114	515.6	693	1752	531	531.7	672	516	535.9	555.1	563.1	587.2	473	564.4	535	499.4	510	524	747	519	523.5	507	757	564	523.4	498	1061	473.4
Ma)	20 ²		24	32	23	7.4	16	60	18	23	18	12	14	9.4	96	160	23	16	81	16	10	11	9.2	9.2	17	8	16	8.6	38	41	210	14	16	61	200	56	10	50	31	11
l ages (⁷ Pb/ [±]		551	561	672	513.2	518	512	537	583	1938	541	1171	519.1	1786	2100	543	606	1328	584	552.1	566.3	564.7	598	478	618.2	626	503.3	573	548	2090	544	713	561	1820	1517	520.9	743	1653	493.3
lculated	$2\sigma^2$		20	110	21	32	22	270	23	130	24	48	34	44	35	230	36	63	37	77	45	55	39	39	31	31	70	29	80	30	300	31	49	32	210	33	32	130	34	51
Ca	Pb/² ⁶ Pb ±		816	780	1336	509	648	570	620	910	2006	709	1283	524	3560	2460	589	886	2590	850	611	612	555	638	517	814	968	514	844	620	3870	640	1357	770	3410	3329	496	1570	2518	589
	$2\sigma^{2}_{0}$		22	35	43	9.2	21	37	18	19	33	14	31	10	120	300	35	19	110	26	17	17	15	13	28	76	31	10	50	36	48	16	20	100	250	77	15	31	31	13
	Pb/² ⁺Th ±		591	607	750	32.3	576	527	577	567	1925	562	1316	\$22.5	1650	8300 4	531	592	1360	609	545	560	565	611	590	1354	665	616.2	661	581	752	542	645	580	1580	1266	563	653	908	503
	Rho ³ ²⁰⁸		0.5	0.5	0.5	6433242 5	7543874	8709235	6419069	0.5	0.492303	5844654	7093767	4255614 5	0.5	0.5	7702496	0.5	0.5	0.5	5133702	4454405	5072991	0.480444	8016144	5534752	0.5	6108836 5	0.5	1508639	0.5	6564746	0.5	7202841	0.5	0.5	4960102	0.5	0.5	7118413
	a ²		0023	0022	0018	0012 0.	0027 0.	0022 0.	0029 0.	0023	0048 (0015 0.	0029 0.	0011 0.	0052	.016	0023 0.	0015	0052	0022	0013 0.	0019 0.	0012 0.	0013 (0037 0.	0013 0.	0021	0011 0.	0063	0023 1.	0.01	0019 0.	0013	0032 1.	.013	.003	0015 0.	0028	0046	0016 0.
	+2		84 0.	11 0.	08 0.	83 0.	79 0.	06 0.	38 0.	13 0.	38 0.	06 0.	86 0.	28 0.	36 0.	13 0	86 0.	86 0.	02 0.	33 0.	69 0.	.0 66	29 0.	23 0.	61 0.	51 0.	65 0.	55 0.1	24 0.	46 0.	23	38 0.	46 0.	17 0.	25 0	14 0	46 0.	04 0.	79 0.0	62 0.
	²⁰⁶ Pb ²³⁸ U		0.07	0.08	.0	0.082	0.0	, 0.08	0.08	0.08	0.3	0.08	l 0.18	0.083	0.11	6.0.3	0.0	0.0	0.11	0.08	0.086	0.08	0.091	0.095	0.07	160.0	0.08	0.080	0.08	0.08	0.1	0.08	0.08	0.08	0.1	60.0	0.08	0.08	0.1	0.07
	$\pm 2\sigma^2$		0.042	0.059	0.043	0.012	0.026	0.097	0.031	0.04	0.12	0.019	0.044	0.015	0.49	1.6	0.039	0.029	0.41	0.029	0.018	0.019	0.016	0.016	0.026	0.014	0.029	0.014	0.066	0.1	1.2	0.023	0.032	0.11	1.1	0.25	0.017	0.1	0.15	0.018
	²⁰⁷ Pb/ ²³⁵ U		0.727	0.749	0.94	0.6583	0.666	0.658	0.698	0.777	5.758	0.704	2.171	0.669	5.05	7.3	0.71	0.818	3.03	0.78	0.724	0.747	0.745	0.803	0.603	0.8385	0.854	0.642	0.76	0.74	7.8	0.709	1.021	0.74	5.6	3.52	0.672	1.09	4.12	0.626
ratios	$\pm 2\sigma^2$		0.0023	0.0041	0.0031	0.00082	0.0016	0.0074	0.0021	0.0046	0.0023	0.0014	0.0012	0.0012	0.023	0.027	0.0023	0.0021	0.016	0.0026	0.0013	0.0015	0.0011	0.0011	0.0017	0.00098	0.0025	0.001	0.0026	0.0065	0.052	0.0015	0.0023	0.014	0.038	0.012	0.0013	0.0071	0.0034	0.0012
Isotopic	²⁰⁷ Pb/ ²⁰⁶ Pb		0.067	0.0668	0.0864	0.05764	0.0614	0.0595	0.0607	0.0699	0.1239	0.0634	0.0838	0.0582	0.317	0.167	0.06	0.0691	0.191	0.0681	0.0606	0.0605	0.059	0.0613	0.0579	0.06637	0.0719	.05791	0.0673	0.0633	0.435	0.0612	0.0874	0.067	0.305	0.277	0.0576	0.0982	0.1666	0.0594
	$\pm 2\sigma^2$		0.0011	0.0018	0.0022	.00047 (0.0011	0.0019	.00093	86000.	0.0018	.00071	0.0016	.00052	0.0065	0.45	0.0018	86000.	0.0057	0.0013	.00085	.00084	.00078	.00066	0.0014	0.004 (0.0016	.00053 (0.0026	0.0018	0.0025	0.0008	0.001	0.0053	0.013	0.0037	.00078	0.0016	0.0016	.00067
	²⁰⁸ Pb/ ²³² Th	T)	0.0297	0.0305	0.0378	0.02669 0	0.0289	0.0264	0.02895 0	0.02843 0	0.0999	0.02822 0	0.0673	0.02619 0	0.0852	0.65	0.0266	0.02972 0	0.0702	0.0306	0.02736 0	0.02812 0	0.02833 0	0.03067 0	0.0296	0.0694	0.0335	0.02587 0	0.0333	0.0292	0.0379	0.02716	0.03245	0.0293	0.082	0.0637	0.02824 0	0.0328	0.0459	0.0252 0
	±2\sigma^2	Zone 19	0.13	0.21	0.24	0.12	0.42	0.27	0.24	0.16	0.13	0.23	0.28	0.093	0.078	2.9	0.42	0.2	0.11	0.13	0.21	0.2	0.18	0.1	0.21	4.6	0.12	0.11	0.23	0.15	0.25	0.28	0.11	0.72	0.14	0.057	0.15	0.11	0.11	0.094
	[%] Pb/	l; Grid	5.2	4.85	4.19	5.04	7.6	3.05	4.71	3.49	5.57	5.86	10.75	4.025	1.151	10	6.79	4.26	1.88	2.93	5.67	4.96	5.95	4.683	4.76	50.9	3.39	4.61	5.9	3.01	0.97	4.99	3.78	5.12	1.25	1.314	5.1	2.27	5.007	3.526
	²⁰⁶ Pb/ ² ²⁰⁴ Pb ² ²	E, 5032336N	18000	15000	9980	22000	14000	60000	40000	20000	63000	22000	26000	21900	345	2390	30000	13000	770	6200	0006	17000	24600	10900	21000	41000	3300	9500	20000	15000	630	30000	5300	12000	830	857	9300	4530	33000	48000
.s ¹	J/Th	719036	1.92	1.67	1.85	1.53	2.87	1.03	1.61	1.23	1.59	1.97	3.78	1.21	0.83	9.20	2.13	1.43	1.11	1.04	1.64	1.51	1.76	1.43	1.84	12.39	1.28	1.40	2.53	1.03	0.52	1.59	1.39	1.80	0.86	0.96	1.64	0.94	1.27	1.16
ntration	Th L	- MTU)	434	354	534	241.1	247	194.9	261	145.1	257.9	256	284	205.6	272	128	188	175	276	239.1	85.5	173	143.9	171.9	232	49.7 3	152.8	154.1	53	583	560	217	166	98	490	840	91.2	985	142	700
ed conce	U (II	nt Road	835	592	988	369.3	710	200.1	420	178.3	409.3	505	1073	249.7	227	1178	400	250	307	249.3	139.8	261	252.7	246	427	1610	195.7	216	134	602	290	346	231	176	420	810	149.4	923	181	810
Measur	Pb ppm) (p	Settleme	115.7	99.1	176	59.7	65.8	45.7	69	37.7	242.6	65.8	174.4	49.9	193	560	46.5	47.4	181	65.4	21.5	44.3	37.4	48.4	65	30.9	46.8	36.7	16.7	155	188	53.8	51.4	29	264	472	24	294	62	163
	Analysis Identifier (1	NB12-314 Cheyne	NB314a_001	NB314a_002	NB314a_003	$NB314a_004$	NB314a_005	NB314a_006	$NB314a_007$	NB314a_008	NB314a_009	NB314a_011	NB314a_012	NB314a_013	NB314a_014	NB314a_015	NB314a_016	NB314a_018	$NB314a_019$	NB314a_021	NB314a_022	NB314a_024	NB314a_025	NB314a_026	NB314a_032	NB314a_033	NB314a_043	NB314a_045	NB314a_046	NB314a_047	NB314a_048	NB314a_049	NB314a_050	NB314a_051	NB314a_052	NB314a_053	NB314a_054	NB314a_055	NB314a_056	NB314a_057

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TableA2. U-Pb geochronologic data for samples GM10-01, NB12-314, and NB12-31 run at Texas A & M University (analyst Brent Miller).

		% con	53.5	96.4	71.0	57.2	88.3	96.8	92.6	98.0	98.9	86.4	32.0	94.9	35.4	91.8	99.5	65.4	87.4	94.1	59.1	50.7	87.5	89.1	71.4	67.8	98.9	98.4	75.9	41.8	32.4	98.4	90.4	91.7	84.4	72.3	9.99	100.6	56.0	92.0	
		$\pm 2\sigma^2$	7.5	7.4	9.6	14	15	11	7.3	8.4	14	19	78	13	20	9.6	8.9	7.7	10	11	9.6	11	11	15	8.2	14	6.7	9.8	20	12	39	37	29	37	9.8	17	7.3	6.8	9.3	12	
		²⁰⁶ Pb/ ²³⁸ U	570	529.8	547.8	579	455	533.6	453.6	512.5	532	490	677	537	640	507.6	539	483.5	527.6	440	513.5	516.1	503	531	524.7	464	535.3	518.7	539	532	661	2786	530	476	536.6	489	535.1	525.6	494.8	474	
	(Ma)	$\pm 2\sigma^2$	18	10	18	31	39	13	9.2	8.8	19	25	82	17	120	9.4	10	14	22	11	18	27	14	26	19	73	9.1	14	32	72	160	19	30	30	15	67	8.8	7.9	36	15	
	ed ages	²⁰⁷ Pb/ ²³⁵ U	1066	549.5	772	1013	515	551	474.4	522.8	538	595	2437	566	1810	552.9	541.8	506	604	467.5	869	1018	575	596	735	684	541.4	527	710	1274	2040	2830	586	519	636	676	535.5	522.7	883	515	
	alculat	$\pm 2\sigma^2$	35	48	36	99	37	59	38	32	100	39	21	69	22	33	23	70	24	33	45	25	51	26	67	27	41	28	89	29	200	18	30	73	31	230	32	33	33	86	
	0	⁰⁷ Pb/ ² ⁰⁶ Pb	2302	623	1482	2124	750	616	565	568	570	1030	4399	682	3690	744	541	624	899	582	1932	2339	870	850	1445	1450	556	560	1301	2900	4010	2861	820	732	1005	1320	529	512	2040	731	
		2 ±2σ ²	23	13	22	37	28	21	9.3	13	24	30	190	19	54	11	13	15	20	18	55	58	15	31	20	49	11	16	32	47	38	64	40	18	20	84	13	8.5	28	28	
		³² Th :	928	546	727	800	481	555	477.1	559	535	587	1250	560	967	564.8	532	509	600	571	996	856	596	563	608	607	545	543	636	820	988	2851	585	486	616	791	554	538.9	833	575	0071
		Rho ³	0.5	0.523673	0.5	0.5	0.5	0.2336851	0.8968335	0.7204625	.3018705	0.5	0.5).6037424	0.5	.7376729	.3704538	0.484024	0.5	.7851674	0.5	0.5	0.5	0.5	0.5	0.5	.4929411	.2322481	0.5	0.5	0.5	.8330032	.6959478	.9044489	0.5	0.5	0.615696	.6155832	0.5	0630735	5
		±2\sigma ²	0.0013	0.0012	0.0016	0.0024	0.0026	0.0018	0.0012	0.0014	0.0023 (0.0032	0.014	0.0022	0.0034	0.0017 (0.0015 (0.0013	0.0017	0.0019 (0.0016	0.0018	0.0019	0.0025	0.0014	0.0024	0.0011 (0.0016 (0.0034	0.002	0.0067	0.0089 (0.0048 (0.0062 (0.0017	0.0028	0.0012	0.0011 (0.0016	0.0021 (
		⁰⁶ Pb/ ²³⁸ U [:]	.09246	.08567	0.0887	0.094	0.0732	0.0863	.07291	0.0828	0.0861	0.0789	0.129	0.087	0.1044	0.0819	0.0872	0.0779	0.0853	0.0706	0.0829	0.0834	0.0812	0.0858	0.0848	0.0746	.08659	0.0838	0.0872	0.086	0.1082	0.541	0.0857	0.0767	0.0868	0.0788	.08656	.08496	0.0798	0.0764	10000
		20 ²	0.052 0	0.018 0	0.039	0.089	0.068	0.021	0.015 0	0.014	0.032	0.044	1.5	0.03	0.61	0.016	0.017	0.022	0.042	0.017	0.049	0.074	0.025	0.047	0.039	0.15	0.015 0	0.02	0.066	0.28	1.1	0.31	0.051	0.049	0.029	0.13	0.015 0	0.013 0	0.086	0.025	0000
		⁷ Pb/ ± ³⁵ U [±]	1.867	0.719	1.141	1.728	0.667	0.721	0.596	0.675	0.7	797	9.5	0.749	5.41	0.724	0.706	0.646	0.816	0.585	1.343	1.73	0.763	0.8	1.067	0.98	0.705	0.677	1.015	2.59	7	15.27	0.783	0.669	0.872	0.96	9690	0.674	1.403	0.661	
	tios	²⁰ 2σ ² 2	0036	0.0013 (0.0032	0.0051	0.0077	.0019 (00075 (00086 (0.0027	0.0037	0.025	0.002	0.035	0.001	0014 (0.0018 (0.0033 (0.0011 (0.003	0.0043	0017 (0.0035	0.0032	0.012	0.0011 (0.0023 (0.0039	0.019	0.051	0.0023	0.0032 (0.0022 (0.0021	.0098) 66000	00088 (0.0062	0.0031	010 0
	otopic ra	Pb/ ± ⁵ Pb [±]	1462 0	0609 0	0931 0	1334 (0669 (0601 0	5905 0.	5924 0.	0594 0	0738 0	0.559	0626	0.366	6422	0587 0	0604 0	0697 0	0596 0	1188	1499 0	0684 0	0679 0	0912 0	0.095	0.059 (0594 0	0848 (0.216	0.456	2046 0	0667 0	0638 (0.073 0	0883 (5826 0.1	5775 0.1	0.128 0	0644 0	0000
	Is	σ^2 207	0012 0	0 6900	0 1100	0 6100	0014 0.	0.001	0047 0.0	0064 0.0	0012 0.	0015 0.	0.01	0 9600	0028	0054 0.0	0066 0.	0078 0.	0 6600	0094 0.	0028 0.	0.003 0.	0 6200	0016 0.	0.001	0025	0057	0079 0.	0016 0.	0024	0.002	0037 0.	0.002 0.	0092 0.	001	0043 0.	0064 0.0	0043 0.0	0014	0014 0.	
		b/ 1h ±2	.047 0.	741 0.0	366 0.	0.404	0.1	0 0279 0	389 0.0	806 0.0	0.268 0.	0.0	.064	811 0.0	.0 1650	834 0.0	669 0.0	551 0.0	016 0.0	864 0.0	.049 0.)433 (992 0.0	0.282	052 0	305 0.	2733 0.0	724 0.0	.032 0.	0.414 0.	1020	516 0.	0294 0	435 0.0	309 (0.0	0.0 0.0	202 0.0	9421 0.	0.0	0 000
		5 ² ²⁰⁸ P 5 ² ²³² T	58 0.	18 0.02	88 0.0	59 0.0	37 0.0	15 0.0	11 0.02	94 0.02	16 0.0	48 0.0	36 0.	13 0.02	0.0 0.0	27 0.02	11 0.02	13 0.02	19 0.03	12 0.02	11 0.	63 0.0	14 0.02	19 0.0	62 0.03	27 0.0	11 0.02	12 0.02	15 0.	54 0.0	13 0.0	37 0.1	34 0.0	23 0.02	11 0.0	1.4 0.0	15 0.02	85 0.02	14 0.0	34 0.0	00
		b/ b ±2c	87 0.0	38 0.	05 0.0	03 0.0	49 0.	37 0.	65 0.	45 0.0	88 0.	77 0.	24 0.0	99 0.	98 (26 0.	96 0.	21 0.	02 0.	63 0.	68 0.	85 0.0	39 0.	93 0.	89 0.0	06 0.	82 0.	3.5 0.	44 0.	89 0.0	87 0.	76 0.	31 0.	89 0.	76 0.	5.7	98 0.	0.0 0.0	85 0.	02 0.	- -
		^{208}Pl	0 2.1	0 5.	0 3.2	0 2.1	0 4.	0 3.	0 3.	0 4.7	0 2.	0 4.	0 0.6	0 2.	0.0	0 5.	0 2.	0 5.	0 4.	0 4.	0 3.	0 1.7	0 4.	0 2.	0 2.2	0 3.	0 4.3	0	0 2.	0 1.1	0 0.	0 11.	0 4.	0 2.	0 3.5	0	0 5.	0 3.	0 2.	0 5.	
		²⁰⁶ Pb/ ²⁰⁴ Pb	188	1020	520	233	1400	320	5900	1960	1300	2000	29	1500	64	1100	410	0006	1200	2100	258	156	5000	510	550	620	1050	50	520	95	31	4300	0006	5100	430	500	980	1640	179	7000	8
	ns ¹	U/Th	1.05	1.64	1.26	0.86	1.32	1.06	1.14	1.54	0.87	1.79	0.46	0.96	0.45	1.75	0.83	1.69	1.33	1.85	2.13	0.84	1.56	0.97	0.76	1.26	1.33	1.14	0.89	0.56	0.49	3.01	1.50	0.94	1.27	3.21	1.81	0.91	1.50	1.86	1 6.7
	ntration	Th l ppm)	300	108.1	352.2	288	356	115	1700	247.2	150	62	98	235	319	233	188	1145	184	655	126	1400	331	99	270.9	318	126	86	102	2220	710	47.8	104	220	153	85	102.4	376	681	207	64
	ed conce	U Ju (I	314	177.3	443.4	248	469	122	1945	381	131	111	45	225	144	408	155.7	1937	245	1210	268	1170	516	64	207.1	400	168	98	16	1241	350	144	156	207	194	273	185.1	343	1022	384	127
.pənı	Measur	Pb (ppm) (p	128.7	27.42	120.5	105.3	73.4	30.4	375	64.1	39	18.5	51	61.6	140	60.9	46.1	268.2	51	171.7	58	537	88	19.1	76.8	88	32.4	22	32	855	349	65	29	53	43.9	31	26.44	93.6	265	55	101
TableA2. Contir		Analysis Identifier (NB314a_058	NB314a_059	$NB314a_{060}$	NB314a_061	NB314a_062	NB314a_063	NB314a_064	NB314a_065	NB314a_066	NB314a_067	NB314a_068	NB314a_070	NB314a_071	NB314a_072	NB314a_073	NB314a_074	NB314a_075	NB314a_076	NB314a_077	NB314a_078	NB314a_079	$NB314a_080$	NB314a_081	NB314a_082	NB314a_083	NB314a_084	NB314a_085	NB314a_086	NB314a_087	NB314a_089	$NB314a_090$	NB314a_091	NB314a_092	NB314a_093	NB314a_094	NB314a_095	NB314a_096	NB314a_097	NTD 2145 008

	$\pm 2\sigma^2 \frac{\%}{con}$	7 95 92.4	1 14 96.9	3 14 86.7	1 9.4 98.9	€.9 97.6 €) 10 99.2	2 15 57.7	96.9) 88 38.2	5 71 37.2	i 80 30.8	5 63 35.7) 30 39.3	1 52 38.9) 38 38.7	3 18 70.8	5 7.8 99.6	5 9 98.4	1 9.2 79.7	1 19 37.5	5 39 75.4	2 54 49.3	2 17 80.4	5 42 60.7	5 37 69.0	1 11 99.2	7 51 61.0	1 17 91.3	3 77 88.6	5 50 82.5	2 17 89.1	2 17 96.5	a 26 77.9	3 11 82.2	2 8.9 97.3) 12 83.7) 56 38.2	1 05 003
	²⁰⁶ Pb/ ²³⁸ U	5167	524	505	519.4	529.9	484.9	482	517.9	1109	826	751	986	59(731	58(403	527.6	521.6	554	521	505	492	522	486	476	539.1	537	441	488	485	492	442	529	514.3	498.2	523	699	i
es (Ma)	$\pm 2\sigma^2$	13	1 17	5 30	5 12	9 8.4	9 12	5 77	5 10	3 95	0 120	0 110	5 75) 250	0 130	7 95	96 6	7 10	0 12	5 14	62 6) 200	7 65	9 36	320	330	5 10	0 110	3 18	1 75	3 78	2 22	8 14	9 75	5 16	2 10	2 12	0 150	0
ated ag	²⁰⁷ Pb/ ²³⁵ U	550	54	58	52	542.	48.	83	534.	290	222(244	276	150	188(149	56	529.	53(69	138	67(66	64	80(69	543.0	88	48	55	58	55	45	679	62	512.2	63.	175(
Calcul	,² ±2σ²	0 34	3 61	0 35	4 63	0 36	3 82	0 37	3 46	2 38	3 83	4 72	7 39	0 460	0 40	0 22	0 440	9 23	6 55	4 24	0 130	0 25	0 35	0 120	0 26	0 1100	1 27	0 290	0 28	69 0:	0 29	62 6	7 30	0 210	0 66	9 36	7 47	0 37	
	2 ⁰⁷ Pb, 06Pb	27	4 62	2 91	1 57	1 55	6 51	4 190	8 6(0 462	0 405	0 451	8 457	0 306	0 357	3 325	5 128	0 52	6 56	7 117	7 310	0 112	3 240	1 113	0 164	0 130	0 57	0 187	3 70	6 84	6 92	1 80	9 52	3 117	9 105	9 56	2 102	0 345	
	/ ² ±2σ	78	18 18	90 3.	46 2	.1 1	38 2	41 4	46 1	30 46	70 17	210	9	90 13	10 31	51 5	44 9	-I 6.	38 1	30 1	97 3	00 18	93 7.	89 3	50 39	10 33	36 21	40 10	93 1	29 6	73 3.	55 2	95 19	53 7.	23 1	55 1	80 2	20 17	
	²⁰⁸ Pb ³² Th	2	2.12	.5	⁷ 6 5 [,]	542	01 5(.5	⁷⁹ 5 ²	.5 28	.5 157	.5 100	.5 18	.5 96	5 22	.5	.5	68 537	24 53	.5	.5	.5 7(.5	.5	.5 100	.5 8.	35 58	.5 10	11 49	.5	.5	.5 65	30 <u>5</u> 6	.5	.5 62	55	.5	.5 102	
	Rho ³	0.088053	0.733801	0	0.368647	0.56676	0.073045	0	0.492747	0	0	0	0	0	0	0	0	0.46226	0.395202	0	0	0	0	0	0	0	0.394288	0	0.4011	0	0	0	0.881908	0	0	0.554515	0	0	
	$\pm 2\sigma^2$	0.0016	0.0024	0.0023	0.0016	0.0012	0.0017	0.0025	0.0013	0.016	0.01	0.014	0.011	0.0051	0.0092	0.0066	0.003	0.0013	0.0015	0.0015	0.0033	0.0066	0.0091	0.0029	0.0071	0.0062	0.0019	0.0086	0.0028	0.013	0.0082	0.0028	0.0028	0.0044	0.0019	0.0015	0.002	0.0096	
	²⁰⁶ Pb/ ²³⁸ U	0.0835	0.0847	0.0819	0.0839	0.08567	0.0781	0.0777	0.0837	0.188	0.133	0.124	0.166	0.0959	0.1205	0.0942	0.0645	0.08529	0.0843	0.0898	0.0842	0.0815	0.0794	0.0843	0.0783	0.0766	0.0872	0.0869	0.0708	0.079	0.0782	0.0793	0.071	0.0855	0.0831	0.0804	0.0856	0.1096	
	$\pm 2\sigma^2$	0.022	0.029	0.052	0.02	0.014	0.019	0.18	0.017	1.7	1.1	1.3	1.2	1.2	0.83	0.42	0.16	0.017	0.018	0.028	0.37	0.55	0.18	0.065	0.74	0.7	0.017	0.27	0.027	0.12	0.15	0.037	0.022	0.16	0.03	0.017	0.021	0.82	
	²⁰⁷ Pb/ ²³⁵ U	0 736	0.705	0.782	0.678	0.708	0.62	1.3	0.694	16.9	8.3	10.3	14.4	4	5.7	3.41	0.76	0.686	0.682	0.981	3.19	1.06	1.68	0.897	1.31	1.02	0.709	1.4	0.61	0.72	0.8	0.725	0.571	0.98	0.855	0.657	0.865	4.87	
ratios	$\pm 2\sigma^2$	0 0022	0.0017	0.0043	0.0017	0.00099	0.0021	0.019	0.0013	0.027	0.023	0.029	0.029	0.065	0.026	0.018	0.02	0.0013	0.0015	0.0019	0.019	0.036	0.012	0.0047	0.064	0.061	0.0015	0.018	0.0029	0.0022	0.0022	0.0026	0.0011	0.01	0.0025	0.0013	0.0018	0.033	
Isotopic 1	²⁰⁷ Pb/ ²⁰⁶ Pb	0.0646	0.0607	0.0697	0.0594	0.05989	0.0579	0.123	0.0602	0.651	0.445	0.605	0.627	0.278	0.333	0.266	0.087	0.0583	0.0592	0.0796	0.257	0.09	0.155	0.0776	0.12	0.096	0.0594	0.118	0.063	0.0671	0.0699	0.0666	0.058	0.082	0.0748	0.0592	0.0739	0.321	
	$\pm 2\sigma^2$	1 00067	0.0017	0.0016	0.0011	0.00054 (0.0013	0.0022	0.00094	0.027	0.0093	0.011	0.0053	0.0067	0.015	0.0028	0.0049	0.00053	0.00079	0.00087	0.0018	0.0094	0.0038	0.0016	0.02	0.017	0.001	0.0054	0.00067	0.0034	0.0019	0.0011	0.00095	0.0037	0.00099	0.00096	0.0011	0.009	
	²⁰⁸ Pb/ ²³² Th	102899 (0.0275	0.0296	0.0274	0.02718 (0.0254	0.0322	0.0274 (0.152	0.0813	0.051	0.0943	0.0501	0.112	0.0482	0.0324	0.02697 (0.02697 (0.03421 (0.0296	0.0356	0.0452	0.0347	0.054	0.041	0.02945	0.0526	0.02469	0.0316	0.0339	0.033	0.02987 (0.0334	0.03132 (0.02783 (0.0342	0.0521	
	t2σ ²	0 15 (0.44	0.27	0.22	0.07	0.53	0.38	0.32	0.022	0.056	0.063	0.028	0.36	0.089	0.056	0.89	0.074	0.15	0.087 I	0.079	0.48	0.12	0.21	1.3	1.4	0.11	0.39	0.14	0.5	0.19	0.33	0.18	0.28	0.15	0.18	7.007	0.14	
	[%] Pb/ [%] Pb ¹	431	5.66	3.47	5.1	2.953	10.84	2.75	4.85	0.59 (0.809 (0.591 (0.61 (1.48	1.193 (1.249 (3.66	2.917 (4.95	3.207 (1.22 (3.19	2.1	4.84	3.3	3.1	3.6	3.11	3.04	4.25	3.18	6.41	4.93	3.75	3.26	4.49	3.511 (1.24	
	²⁰⁶ Pb/ ²⁰	3700	15000	18000	19000	4900	80000	3100	4100	213	310	161	228	1550	457	605	10100	14600	400	600	780	19300	1090	5800	5500	41000	8600	1600	18000	30000	60000	100000	18000	10600	700	6400	2100	431	0000
s1	//Th	1 45	1.76	1.30	1.66	0.88	3.54	1.01	1.33	0.56	0.50	0.21	0.38	0.60	1.03	0.70	2.17	0.89	1.56	1.19	0.44	1.36	1.19	1.99	1.92	1.55	1.18	1.62	1.10	1.85	1.44	2.69	2.11	1.44	1.24	1.46	1.39	0.73	
ntration	Th U	230	106	40	169	208.5	29.7	83	244	57	201	570	178	336	234	1570	530	260.4	198.9	158.1	297	420	309	137	125	103	162.3	165	420	33	109	167	228	289	178.3	183	259.7	620	
sd conce:	U (F	333	187	52	280	84.4	105	84	325	32	100	121	67	202	242	1100	1150	30.8	10.9	88.5	132	570	368	272	240	160	191.9	267	460	61	157	450	480	417	20.6	6.99	362	450	
nuea. Measure	ld) (mqd) dq	64.6	30	10.9	44	52.4 1	7.3	27.3	59.1	80	137	250	156	167	179	640	179	64.9 2	49.2 🤅	50.2	77.8	132	136	52	43	26	43.8 j	16	100	10.3	36	51	65	88	52.1 2	46 2	83.1	215	
1 able A 2. Conti	Analysis Identifier	NB314a 099	NB314a_100	NB314a_101	$NB314a_102$	$NB314a_{103}$	$NB314a_104$	NB314a_105	NB314a_106	NB314a_107	NB314a_108	NB314a_109	NB314a_110	NB314a_111	NB314a_112	NB314a_113	NB314a_114	NB314a_115	NB314a_116	NB314a_117	NB314a_118	NB314a_119	$NB314a_{-}120$	NB314a_121	NB314a_122	NB314a_123	NB314a_124	NB314a_125	NB314a_126	NB314a_127	NB314a_128	NB314a_129	NB314a_130	NB314a_131	NB314a_132	$NB314a_{133}$	$NB314a_{134}$	NB314a_135	

inued. Measured concentration	d concentration	tration	IS 1						Isotopic r	atios								Calcula	ited ages ((Ma)			
$ \begin{array}{ccccc} Pb & U & Th & U/Th \\ (ppm) & (ppm) & (ppm) & U/Th & & & & & & & & & & & & & & & & & & &$	$ \begin{array}{cccc} U & Th & U/Th \\ & & & \\ & &$	$ (h U/Th) \begin{array}{c} {}^{206}\text{Pb}/ & {}^{208}\text{Pb}/ & {}^{208}\text{Pb}/ & {}^{208}\text{Pb}/ & {}^{208}\text{Pb}/ & {}^{208}\text{Pb}/ & {}^{208}\text{Pb}/ & {}^{202}\text{Pb}/ & {}^{232}\text{Ph}/ & {}^{23$		$^{208} Pb/ \pm 2\sigma^2 ^{208} Pb, \\ ^{206} Pb \pm 2\sigma^2 ^{232} Th$	$\pm 2\sigma^2 {}^{208} Pb$,	²⁰⁸ Pb,		$\pm 2\sigma^2$	²⁰⁷ Pb/ ²⁰⁶ Pb	$\pm 2\sigma^2$	⁰⁷ Pb/ [±] ²³⁵ U [±]	$2\sigma^2$	⁶ РЬ/ ³⁸ U	±2σ ² Rh	10 ³ 3	^s Pb/ ² ² Th ±20	5 ² ²⁰⁷ Pb ⁵² ⁰⁶ Pb	2 $\pm 2\sigma^{2}$	²⁰⁷ Pb/ ²³⁵ U :	² ±2σ ²	⁰⁶ Pb/ ²³⁸ U ¹	-20 ²	%
59 290 165 1.76 31000 3.79 0.69 0.0	290 165 1.76 31000 3.79 0.69 0.0	165 1.76 31000 3.79 0.69 0.0	31000 3.79 0.69 0.0	0.0 0.69 0.0	0.69 0.0	0.0	372	0.0093	0.083	0.036	0.88	0.36 (0.0782	0.004	0.5	740 1	30 102	0 540	620	160	485	24	78.2
45.7 286 176 1.63 20000 5.11 0.26 0.02	286 176 1.63 20000 5.11 0.26 0.02	176 1.63 20000 5.11 0.26 0.02	20000 5.11 0.26 0.02	0.26 0.02	0.26 0.02	0.02	5	0.0013	0.0589	0.0018	0.68	0.021	0.084	0.0014 0.289	90654 2 -	582	26 51	0 39	526	12	519.9	8.4	98.8
74.2 0.0 /1.0 0.74/ 0.029 0.02	386 413 0.93 5900 2.93 0.129 3.03 0.12	24/ 1.40 8000 4.5 0.17 0.029 413 093 5900 293 038 012	5900 2.93 0.38 0.12	920.0 /1.0 cc.4 1 2.03 0.38 0.12	0.38 0.12	0.12 0.12	- 6 2 6	28000.0 700.0	0.0688	0.002/	0./88	0.036 L).U828 0 443	0.032 0.032	0.5 0	285 2460 1	16 oc 315 oc	9 / 0 9 / 0	285 2814	02 L4	616 2360	c1 150 c	33.9
51.9 373 210 1.78 30000 5.86 0.38 0.02	373 210 1.78 30000 5.86 0.38 0.00	210 1.78 30000 5.86 0.38 0.02	30000 5.86 0.38 0.02	5.86 0.38 0.02	0.38 0.02	0.0	81	0.0017	0.0612	0.0019	0.707	0.024 (0.0843	0.0022 0.490	07848	559	33 6	6 25	543	14	522	13	96.1
104 90 196 0.46 257 0.807 0.05 0.1	90 196 0.46 257 0.807 0.05 0.1	196 0.46 257 0.807 0.05 0.1	257 0.807 0.05 0.1	. 0.807 0.05 0.1	0.05 0.1	0.1	.13	0.036	0.432	0.03	7.9	1.5	0.131	0.02	0.5	2090 6	10 402	3 94	2130	150	790	110	37.1
94 167 267 0.63 620 1.41 0.13 0.0	167 267 0.63 620 1.41 0.13 0.0	267 0.63 620 1.41 0.13 0.0	620 1.41 0.13 0.0	0.13 0.0	0.13 0.0	0.0	431	0.0027	0.284	0.025	3.92	0.5 (0.0973	0.0042	0.5	851	52 324	0 41	1570	100	598	24	38.1
40 230 125 1.84 16000 4.32 0.29 0.03	230 125 1.84 16000 4.32 0.29 0.03	125 1.84 16000 4.32 0.29 0.03	16000 4.32 0.29 0.03	0.03 0.29 0.03	0.29 0.03	0.03	321	0.0028	0.0648	0.0044	0.66	0.064 (0.0743	0.0046 0.718	83748	638	55 70	0 23	513	38	462	28	90.1
310 990 786 1.26 980 2.26 0.12 0.04	990 786 1.26 980 2.26 0.12 0.04	786 1.26 980 2.26 0.12 0.04	980 2.26 0.12 0.04	0.12 0.04	0.12 0.04	0.04	32	0.0021	0.1591	0.0087	1.72	0.12 (0.0777	0.0016	0.5	855	40 242	6 94	1009	45	482.1	9.5	47.8
72.5 295.5 209 1.41 2630 3.36 0.14 0.0	95.5 209 1.41 2630 3.36 0.14 0.0	209 1.41 2630 3.36 0.14 0.0	2630 3.36 0.14 0.0	0.0 3.36 0.14 0.0	0.14 0.0	0.0	38	0.0011	9660.0	0.0038	1.213	0.048 (0.0886	0.0017	0.5	754	22 16(5 24	805	22	547.4	10	58.0
94.7 446 315.7 1.41 2300 3.67 0.12 0.03	446 315.7 1.41 2300 3.67 0.12 0.03	315.7 1.41 2300 3.67 0.12 0.03	2300 3.67 0.12 0.03	0.12 0.03	0.12 0.03	0.03	25	0.0012	0.0724	0.0027	0.827	0.028 (0.0834	0.0022	0.5	645	24 97	3 76	611	15	517	13	34.6
38.23 148.6 148.1 1.00 8500 3.136 0.087 0.029	48.6 148.1 1.00 8500 3.136 0.087 0.028	148.1 1.00 8500 3.136 0.087 0.028	8500 3.136 0.087 0.028	3.136 0.087 0.028	0.087 0.028	0.028	304 (0.00072	0.0589	0.0014	0.697	0.019	0.0853	0.0014 0.500	01025	559	14 54	9 25	536	12	527.8	8.2	98.5
50.4 361.8 191.6 1.89 21000 5.75 0.16 0.025	61.8 191.6 1.89 21000 5.75 0.16 0.028	191.6 1.89 21000 5.75 0.16 0.028	21000 5.75 0.16 0.028	0.16 0.028	0.16 0.028	0.028	351 (0.00066	0.0621	0.0011	0.727	0.02 (0.0848	0.0017 0.766	60355	568	13 67	2 37	554	12	524.5	10	94.7
111.7 641 457 1.40 15000 4.115 0.076 0.026	641 457 1.40 15000 4.115 0.076 0.026	457 1.40 15000 4.115 0.076 0.026	15000 4.115 0.076 0.026	4.115 0.076 0.026	0.076 0.026	0.026	47 (0.00045 (0.06155 0	86000.	0.651	0.016 (0.0767	0.0013 0.765	55638	528 8	.9 6	2 26	508.7	10	476.3	2.9) 3.6
94.8 684 346.2 1.98 33000 5.62 0.13 0.02	684 346.2 1.98 33000 5.62 0.13 0.02	346.2 1.98 33000 5.62 0.13 0.02 ¹	33000 5.62 0.13 0.02	5.62 0.13 0.02	0.13 0.02	0.02) 696	0.00067 (0.06176 0	00082	0.7	0.014 (0.0823	0.0015 0.762	25137	591	13 6(1 28	538.6	8.5	509.6	8.7	94.6
157.7 961 640 1.50 29000 4.397 0.11 0.0262	961 640 1.50 29000 4.397 0.11 0.0262	640 1.50 29000 4.397 0.11 0.0262	29000 4.397 0.11 0.0262	4.397 0.11 0.0262	0.11 0.0262	0.0262	5	0.00062	0.0602	0.0016	0.609	0.019 0.	07345	0.001 0.532	24457	524	12 6(1 50	482	11	456.9	6.3	94.8
101.6 797 297.1 2.68 6600 6.13 0.17 0.03	797 297.1 2.68 6600 6.13 0.17 0.03	297.1 2.68 6600 6.13 0.17 0.03	6600 6.13 0.17 0.03	0.03	0.17 0.03	0.03	63	0.0013	0.0764	0.0018	0.82	0.019 (0.0781	0.0013	0.5	721	25 109	4 27	607.5	11	484.8	7.7	79.8
166 430 400 1.08 60000 2.53 0.49 0.03	430 400 1.08 60000 2.53 0.49 0.03	400 1.08 60000 2.53 0.49 0.039	60000 2.53 0.49 0.039	0.039 0.49 0.039	0.49 0.039	0.039	94	0.0096	0.118	0.07	1.18	0.46 (0.0851	0.0092	0.5	780 1	30 135	0 700	750	170	526	55	70.1
120 738 437 1.69 8000 4.29 0.2 0.030	738 437 1.69 8000 4.29 0.2 0.030	437 1.69 8000 4.29 0.2 0.030	8000 4.29 0.2 0.030	4.29 0.2 0.030	0.2 0.030	0.030	_	0.0018	0.0746	0.005	0.763	0.068 (0.0737	0.0017	0.5	600	36 102	0 28	570	35	458.3	10	30.4
24.2 158.4 81.6 1.94 9300 5.49 0.25 0.032	58.4 81.6 1.94 9300 5.49 0.25 0.032	81.6 1.94 9300 5.49 0.25 0.032	9300 5.49 0.25 0.032	0.25 0.032	0.25 0.032	0.032	~	0.0021	0.0693	0.0036	0.837	0.047 (0.0879	0.0015	0.5	651	±1 8(0 110	613	25	543	8.9	38.6
27 92 62 1.48 2500 2.47 0.78 0.04	92 62 1.48 2500 2.47 0.78 0.04	62 1.48 2500 2.47 0.78 0.04	2500 2.47 0.78 0.04	2.47 0.78 0.04	0.78 0.04	0.04	œ	0.011	0.116	0.04	1.41	0.55 (0.0882	0.0083	0.5	940 2	20 177	0 29	870	240	545	49	62.6
21.1 316 88.3 3.58 9800 11.25 0.43 0.026	316 88.3 3.58 9800 11.25 0.43 0.026	88.3 3.58 9800 11.25 0.43 0.026	9800 11.25 0.43 0.026	0 11.25 0.43 0.026	0.43 0.026	0.026	503	0.00085	0.0574	0.0013	0.634	0.017 (0.0804	0.0017 0.57	75992	519	17 49	7 50	498.1	11	498.3	10 10	0.00
82.7 406 288 1.41 90000 3.83 0.13 0.0	406 288 1.41 90000 3.83 0.13 0.0	288 1.41 90000 3.83 0.13 0.0	90000 3.83 0.13 0.0	0.03.83 0.13 0.0	0.13 0.0	0.0	316	0.0011	0.0795	0.0034	0.926	0.045 (0.0853	0.0017	0.5	628	21 116	9 30	671	20	527.7	10	78.6
39.3 262 161.9 1.62 16700 5 0.16 0.02	262 161.9 1.62 16700 5 0.16 0.02	(61.9 1.62 16700 5 0.16 0.02	16700 5 0.16 0.02	0.16 0.02	0.16 0.02	0.02	(657 (0.00074	0.0583	0.0014	0.641	0.018 (0.0801	0.0015 0.534	49065	530	15 52	1 53	502	11	496.6	8.7	98.9
66.1 313 282 1.11 10700 3.564 0.079 0.02	313 282 1.11 10700 3.564 0.079 0.02	282 1.11 10700 3.564 0.079 0.02	10700 3.564 0.079 0.02	3.564 0.079 0.02	0.079 0.02	0.02	543 (0.00054	0.0588	0.0011	0.65	0.013 0.	08013	0.0012 0.457	79106	507.6	11 55	8 31	508.1	8.2	496.9	5	97.8
7.1 65 24 2.71 36000 7.55 0.56 0.0	65 24 2.71 36000 7.55 0.56 0.0	24 2.71 36000 7.55 0.56 0.0	36000 7.55 0.56 0.0	0.7.55 0.56 0.0	0.56 0.(0.0	0282	0.0021	0.0728	0.0095	0.74	0.093 (0.0743	0.0024	0.5	563	41 100	0 26	562	55	462	14	82.2
61.5 304 197.1 1.54 3300 3.74 0.2 0.	304 197.1 1.54 3300 3.74 0.2 0.	[97.1 1.54 3300 3.74 0.2 0.	3300 3.74 0.2 0.	0.2 0.1	0.2 0.	0.0	0343	0.0021	0.0758	0.0026	0.873	0.04 (0.0842	0.0035	0.5	682	108	3 68	637	22	521	21	81.8
127 600 590 1.02 90000 4.38 0.93 0.0	600 590 1.02 90000 4.38 0.93 0.0	590 1.02 90000 4.38 0.93 0.0	90000 4.38 0.93 0.0	0.93 0.93 0.0	0.93 0.0	0.0	0266	0.0022	0.065	0.017	0.646	0.07 (0.0737	0.0068 2.407	78989	531	13 9	0 32	504	40	458	41	90.9
69.4 245 244.1 1.00 70000 2.72 0.27 0.0	245 244.1 1.00 70000 2.72 0.27 0.0	244.1 1.00 70000 2.72 0.27 0.0	70000 2.72 0.27 0.0	0.0 2.72 0.27 0.0	0.27 0.0	0.0	312	0.003	0.0657	0.0021	0.778	0.05 (0.0866	0.0067 0.914	45187	620	56 75	6 65	584	28	535	40	91.6
272.6 562 409 1.37 13600 4.8 0.34 0.07	562 409 1.37 13600 4.8 0.34 0.07	409 1.37 13600 4.8 0.34 0.07	13600 4.8 0.34 0.03	0.34 0.07	0.34 0.07	0.07	761	0.0058	0.1146	0.0036	4.11	0.15 (0.2617	0.0057 0.515	55055	1480 1	18(6 33	1655	29	1498	29	90.5
176 558 731 0.76 23000 2.459 0.063 0.026	558 731 0.76 23000 2.459 0.063 0.026	731 0.76 23000 2.459 0.063 0.026	23000 2.459 0.063 0.026	0.026	0.063 0.0265	0.026	51 (0.00054 (0.06281	0.0009	0.711	0.018 (0.0819	0.0016 0.820	62124	528.8	11 70	2 32	544.9	10	507.4	9.3	93.1
164 172 520 0.33 242 0.912 0.1 0.05	172 520 0.33 242 0.912 0.1 0.05	520 0.33 242 0.912 0.1 0.05	242 0.912 0.1 0.05	0.912 0.1 0.05	0.1 0.05	0.05	32	0.009	0.439	0.033	7.15	0.95 ().1165	0.0088	0.5	1040 1	70 40(0 34	2100	130	708	50	33.7
157.9 450 248 1.81 771 2.322 0.088 0.07	450 248 1.81 771 2.322 0.088 0.0 ⁻	248 1.81 771 2.322 0.088 0.0	771 2.322 0.088 0.0	2.322 0.088 0.0	0.088 0.0	0.0	707	0.0027	0.1657	0.0073	2.02	0.13 (0.0887	0.0028	0.5	1379	50 249	7 64	1113	39	547	16	49.1
33.2 157 119 1.32 9200 4.11 0.49 0.03	157 119 1.32 9200 4.11 0.49 0.03	119 1.32 9200 4.11 0.49 0.03	9200 4.11 0.49 0.03	4.11 0.49 0.03	0.49 0.03	0.03	14	0.0027	0.086	0.02	1	0.25 (0.0834	0.0026	0.5	624	53 107	0 35	670	100	516	15	77.0
166 85 166 0.51 142 0.597 0.057 0	85 166 0.51 142 0.597 0.057 0	166 0.51 142 0.597 0.057 0	142 0.597 0.057 0	0.597 0.057 0	0.057 0	0	.124	0.044	0.65	0.044	19.6	5.9	0.219	0.056	0.5	2330 7	50 462	0 100	3020	240	1260	280	47.7
333 1140 702 1.62 963 2.498 0.083 ((140 702 1.62 963 2.498 0.083 0	702 1.62 963 2.498 0.083 (963 2.498 0.083 (2.498 0.083	0.083	Ŭ	0.055	0.0025	0.1453	0.005	1.643	0.088 (0.0823	0.002	0.5	1080	48 228	0 36	066	36	509	12	51.4
63.7 162.4 170.8 0.95 2940 2.197 0.073 0.0	62.4 170.8 0.95 2940 2.197 0.073 0.0	170.8 0.95 2940 2.197 0.073 0.0	2940 2.197 0.073 0.0	0.073 0.073 0.0	0.073 0.0	0.0	0406	0.0012	0.1269	0.0032	1.623	0.051	0.093	0.0015	0.5	805	23 205	0 46	978	20	573.1	8.8	58.6
149 883 231 3.82 36000 11.3 1.8 0.0	883 231 3.82 36000 11.3 1.8 0.0	231 3.82 36000 11.3 1.8 0.0	36000 11.3 1.8 0.0	11.3 1.8 0.0	1.8 0.0	0.0	698	0.0025	0.0897	0.0032	2.45	0.23	0.197	0.015 0.9	93298	1364	14.	1 69	1244	73	1157	2 9	93.0
64.5 376 253 1.49 11000 4.53 0.16 0.027	376 253 1.49 11000 4.53 0.16 0.027	253 1.49 11000 4.53 0.16 0.027	11000 4.53 0.16 0.027	0.027 0.16 0.027	0.16 0.027	0.027	77 (0.00082	0.0612	0.0022	0.713	0.026 (0.0849	0.002 0.34	48343	554	16 6	4 37	546	15	525	12	96.2

	% con	77.4	62.0	6.66	87.7	89.0	97.2	39.5	90.7	78.9	88.5	83.3	94.4	95.2	97.0	99.1	30.4	95.0	97.5	95.3	53.7	44.2	76.7	40.2	91.2	98.2	97.6	59.0	42.5	91.9	91.6	92.5	81.3				
	$\pm 2\sigma^2$	18	18	6.9	20	8.1	8.1	19	8.6	8.8	26	500	13	8.2	11	7.6	53	7.5	7.5	15	7.1	59	13	15	14	6.5	38	9.3	14	6	9.9	12	9.5		2.9	1.9	
	²⁰⁶ Pb/ ²³⁸ U	472	510	529.6	543	457.7	506.5	621	451	509	493	500	523	493.1	489	511.4	748	448.8	539.9	526	488.4	942	511	611	541	492.5	1475	586.7	484	515.3	472.6	457	523.7		1065.6	418.2	
(Ma)	$\pm 2\sigma^2$	140	34	8.4	53	11	12	69	11	25	34	600	20	10	15	8.8	150	9.8	11	17	19	48	36	60	18	8	54	34	33	15	12	19	18		2.9	2.6	
d ages	⁰⁷ Pb/ ²³⁵ U	610	822	529.9	619	514	521	1573	497.2	645	557	600	554	517.7	504	516.3	2460	472.4	554	552	606	2131	666	1521	593	498.3	1512	994	1139	561	516	494	644		1063.3	417.3	
alculate	$\pm 2\sigma^2$	400	38	41	39	55	40	110	41	27	140	42	24	39	25	47	26	50	27	57	43	28	150	29	80	30	110	31	64	32	69	28	33		6.1	14.0	
C	⁰⁷ Pb/ ² ⁰⁶ Pb	1040	1801	533	910	781	584	3270	722	1170	830	1000	670	614	572	532	4490	591	595	664	2129	3636	1230	3189	810	521	1580	2018	2767	739	758	675	1094		1052.2	406.0	
	$\pm 2\sigma^2$	66	40	10	39	19	13	51	16	53	20	650	18	12	14	11	79	11	11	17	23	860	47	38	26	11	95	20	54	19	17	34	23		6.5	3.1	
	³⁸ Pb/ ² ³² Th	622	819	538.1	587	556	515	888	516	604	523	650	541	520	508	529	1164	476	558.8	566	968	7720	609	1469	568	506.8	1461	860	813	558	576	543	643		062.7	422.6	
	Rho ³	0.5	0.5	0.4512286	0.5	0.5	0.4334907	0.5	0.5889966	0.5	0.5	0.5	0.2360362	0.6592134	0.449934	0.4084449	0.5	0.4379545	0.2465725	0.7095127	0.5	0.5	0.5	0.5	0.3104085	0.5398206	0.4610627	0.5	0.5	0.488871	0.2463087	0.5832058	0.5		0.5497078	0.558043	
	$\pm 2\sigma^2$	0.0018	0.003	0.0012	0.0034	0.0013	0.0014	0.0033	0.0014	0.0015	0.0043	0.08	0.0022	0.0014	0.0019	0.0013	0.0092	0.0012	0.0013	0.0026	0.0012	0.011	0.0022	0.0026	0.0023	0.0011	0.0074	0.0016	0.0024	0.0015	0.0016	0.002	0.0016		0.00246	0.00118	
	²⁰⁶ Pb/ ²³⁸ U	0.0747	0.0824	0.08563	0.0879	0.0736	0.0817	0.1012	0.0725	0.0822	0.0795	0.08	0.0846	0.0795	0.0788	0.08256	0.1232	0.0721	0.08737	0.0851	0.07872	0.158	0.0825	0.0996	0.0876	0.07939	0.2572	0.0953	0.078	0.0832	0.0761	0.0734	0.0846		0.17962	0.06715	
	$\pm 2\sigma^2$	0.17	0.076	0.014	0.11	0.018	0.021	0.3	0.017	0.046	0.06	0.81	0.034	0.016	0.022	0.014	1	0.015	0.023	0.028	0.041	0.54	0.07	0.31	0.032	0.012	0.23	0.096	0.1	0.025	0.019	0.031	0.034		0.0381	0.0189	
	⁰⁷ Pb/ ²³⁵ U	0.75	1.254	0.686	0.85	0.66	0.671	3.78	0.632	0.889	0.734	0.81	0.727	0.666	0.639	0.663	10.65	0.593	0.734	0.723	1.441	7.21	0.932	3.64	0.795	.6328	3.44	1.7	2.078	0.739	0.664	0.628	0.887		.8538).5362	
atios	$\pm 2\sigma^2$	0.026	0.0038	0.0011	0.009	0.0017	0.0017	0.017	0.0014	0.0043	0.0048	0.073	0.003	0.0011	0.0019	0.0012	0.049	0.0014	0.0019	0.0017	0.0033	0.018	0.0067	0.015	0.0027	0.00095	0.0058	0.0065	0.0077	0.0019	0.002	0.0025	0.0025		0.0013 1	0.0017 0	
Isotopic 1	²⁰⁷ Pb/ ²⁰⁶ Pb	0.084	0.1106	0.0584	0.0715	0.0654	0.0598	0.269	0.0636	0.079	0.0675	0.073	0.0627	0.0606	0.0595	0.0584	0.61	0.0598	0.0609	0.0619	0.1328	0.343	0.0827	0.257	0.0664	0.05804 (0.0977	0.1288	0.1937	0.0643	0.0644	0.0623	0.0764		0.07488	0.05786	
	$\pm 2\sigma^2$	0.0051	0.0021	0.00053	0.002	0.00094	0.00067	0.0026	0.00081	0.0027	0.001	0.033	0.00091	0.00062	0.00071	0.00056	0.0041	0.00055	0.00055	0.00086	0.0012	0.065	0.0024	0.002	0.0013	0.00054 (0.005	0.001	0.0028	0.00098	0.00088	0.0017	0.0012		0.00161	0.00072	
	²⁰⁸ Pb/ ²³² Th	0.0313	0.0413	0.02698	0.0295	0.02788	0.02583	0.045	0.02587	0.0303	0.02621	0.033	0.02711	0.02608	0.02544	0.02652	0.0593	0.02384	0.02804	0.02842	0.0491	0.484	0.0306	0.0754	0.0285	0.0254	0.075	0.04346	0.041	0.02801	0.0289	0.0272	0.0323		0.0542	0.02198	
	±2ơ²	0.52	0.1	0.15	0.29	0.12	0.095	0.047	0.12	0.42	0.17	4.4	0.14	0.12	0.19	0.12	0.054	0.1	0.084	0.19	0.058	0.15	0.54	0.081	0.17	0.11	0.32	0.091	0.068	0.14	0.21	0.39	0.094		0.294	0.177	
	³⁸ Pb/ ⁹⁰⁶ Pb	3.79	2.887	4.59	2.76	4.51	3.374	1.147	4.39	4.52	2.95	4.4	3.12	4.81	5.35	4.38	0.619	3.937	3.137	4.2	2.475	1.5	5.46	1.53	2.74	4.184	4.36	2.204	1.817	5.25	5	5.24	3.555		.3655	.7078	
	²⁰⁶ Pb/ ²¹ ²⁰⁴ Pb ²	36000	1370	12800	6700	80000	12000	392	19000	10300	14000	4100	5400	14000	21000	14400	240	37000	8400	36000	2730	303	2400	384	12000	23000	17000	1360	520	19000	36000	38000	5400		10150 9	:741.666667 4	
1s ¹	d/Th	1.44	1.46	1.35	0.98	1.62	1.05	0.50	1.58	1.68	0.93	1.51	0.99	1.51	1.74	1.34	0.38	1.30	0.95	1.43	1.44	4.41	1.99	1.33	0.89	1.26	1.31	0.92	1.01	1.73	1.88	1.90	1.35		2.67	1.22 8	
ntration	Th l	1230	463	131.6	208	516.4	368.5	292	664	182.1	430	186	96.2	353.2	278.8	160	460	1027	170.3	265.7	552.7	286	122.3	301	243	242	225.6	436	744	197	467	310	231		30.03	212.72	
d conce	U (It	1770	674	77.7	203	835	87.5	147	1048	06.4	400	280	95.3	534	484	15.1	175	1336	62.4	379	798	1260	243	400	216	305	295	402	748	340	878	590	311		0.26	l(s)5 8.48 2	
ued. Measure	ld) (mqq	357	171	32.8 1	56.8	133.9	87.1 3	116	156.7	50.4 3	115	62	23.9	84.8	65.8	39 2	247	223.9	44.3 1	69.7	252.8	1200	34.1	208	62.8	56.5	154	176	284	50	124.9	79	68.4	material5	15.04 8	e materia 43.15 25	
TableA2. Continu	Analysis Identifier (₁	NB314a_178	NB314a_179	NB314a_180	NB314a_181	NB314a_182	NB314a_183	NB314a_184	NB314a_185	NB314a_186	NB314a_187	NB314a_188	NB314a_189	NB314a_190	NB314a_191	NB314a_192	NB314a_193	NB314a_194	NB314a_195	NB314a_196	NB314a_197	NB314a_198	NB314a_199	NB314a_200	NB314a_201	NB314a_202	NB314a_203	NB314a_204	NB314a_205	NB314a_206	NB314a_207	NB314a_208	NB314a_209	Primary reference	91500 (n=32)	Secondary referenc R33 (n=10)	

ATLANTIC GEOLOGY \cdot VOLUME 55 \cdot 2019

		% con		96.5	95.0	93.0	93.8	98.6	100.7	94.5	101.8	7.99.7	98.7	8.66	95.4	102.0	101.1	102.3	41.2	99.7	100.2	100.5	98.5	95.8	98.8	7.99 \$	98.7	95.6	90.5	97.9	99.3	98.9	5 101.4	87.4	92.2	97.4	99.1	100.2	100.6	0 101.6	100.0
		b/ U ±2ớ		1.2 7.6	738 24	0.1 8.	704 17	6.1	109 35	550 1	550 3.	7.8 5.4	6.8 7.2	750 21	2.6 8.5	817 24	1.8 6.6	5.8 8.6	756 21	5.5	2.4 8.1	2.6 7.2	582 1	569 13	325 15	3.7 8.6	4.2 9.2	742 21	172 40	0.7 5.9	750 19	209 19	0.6 8.6	205 3(6.9	340 3(9.9 7.5	9.1 8.2	3.7 9.9	559 8.9	722 3(
	a)	5 ² ²⁰⁶ Ρ 5 ²³⁸ η		.8 57	l6 17	12 57	17	12 55	[2 3]	8	12 26	.1 53	0 54	17	13 56	.6 28	3 54	.3 58	12	4 53	3 58	11 55	5	12	11 13	.5 56	4 57	15 17	37 14	.1 55	17	.7 17	12 56	30 12	8 54	16 18	.6 56	11 51	.6 57		13 27
	ages (M	b/ J ±2c		1.9 8	329	513]	316]	564]	186	582]	502]	9.6 9	554]	753]	200	2.3 8	536]	2.5 7	334	537]	581]	500	165	594	341]	1.3 8	582]	323]	527 3	2.8 9	762]	8.6 9	553]	379 3	593]	890	4.8 8	518]	0.1 8	550]	722]
	ulated	3^{207} P		46 59	33 16	59 (20 15	36	20 3(00	25 2(49 53	52	20 1.	66	14 276	55	30 57	33 18	20	57	52	81	20	1 61	49 57	74	24 13	56 10	49 56	25 1.	27 172	22	13 13	72	28 18	16 57	57	48 57	52	24 2.
	Calc	Pb ^{±2}		730	976	825	266	631	112	700 1	588	582	594	745	678	210	475	508	449	519	559	538	586	650 1	338	532	563	106	810	576	754	749	502	.662	756	944	585	500	549	512	725
		$2\sigma^2 \frac{207}{06}$		21	65	28	65	24	110	26	96	21	21	61	25	100	28	22	180	27	28	23	34	60	53	28	24	72	79	25	76]	16	21	56	23	29	10	17	15	11	32
		Pb/² ±⊆ Th		513	1641	574	1703	517	2919	514	2464	505	515	1580	580	2891	560	567	2290	546	595	559	628	622	1432	603	627	1862	1631	561	1863	1689	584	1785	601	1876	572	521	576	556	2705
		Rho ³ ²⁰⁸		2239513	4202736	0211745	5678714	0274095	6014034	0669106	4090556	1991273	2993411	7021688	0041829	.621833	.455363	.656057	.463423	2701615	0950376	3440297	1534212	8031105	7454191	.303766	0.110725	6316865	5644697	0466522	5657753	3550648	3347255	8431913	.451881	5264296	2594005	1551042	3308796	3782956	.414286
		$2\sigma^2$.0013 0.3	.0049 0.	.0014 0.0	.0034 0.0	.0012 0.0	.0089 0.	.0019 0.	.0072 0.4	0 16000	.0012 0.	.0043 0.	.0014 0.	.0057 0	0011 0	.0015 0	.0036 0	.0014 0.3	.0014 0.0	.0012 0.3	.0019 0.	.0021 0.	.0029 0.	.0013 0	.0016 0	.0043 0.	.0083 0.	0.001 0.0	.0038 0.	.0039 0.	.0015 0.	.0056 0.3	.0014 0	.0061 0.0	.0013 0.	.0014 0.	0017 0.	0015 0.	0071 0
		Pb/ [±] ±		0927 0	3095 0	0925 0	3027 0	0 1060	6202 0	0892 0	5087 0	8702 0.0	0885 0	0.312 0	0912 0	5483 0	0877 0	0951 0	1245 0	0866 0	0946 0	0895 0	0945 0	0923 0	2282 0	0924 0	0932 0	3104 0	2571 0	0892	3119 0	3037 0	0 6060	2056 0	0885 0	3305 0	9245 0	0839 0	0931 0	0 9060	5256 0
		20 ² 23		0.016 0.	.096 0.	0.02 0.	.076 0.	.021 0.	0.25 0.	.033 0.	0.16 0.	0.015 0.0	.017 0.	0.07	.022 0.	0.13 0.	0.022 0.	.013 0.	0.29 0.	.023 0.	.023 0.	.018 0.	0.027 0.	0.11 0.	0.04 0.	.015 0.	.024 0.	.087 0.	0.17 0.	.015 0.	.071 0.	.053 0.	.022 0.	0.12 0.	.038 0.	0.1 0.	0.014 0.0	0.018 0.	0.015 0.	.018 0.	0.19 0.
		b/ ±U		793 0	064 0	828	987 0	745 0	16.	774 0	.98	703 0	727 0	627	785 0	4.2	698 0	758 0	6.13	701 0	775 0	721 0	793 0	.85	751	754 0	776 0	031 0	.02	742 0	677 0	491 0	723 0	16.	0.8 0	446	.76 0	668 0	754 0	721 0	61
	0S	σ ² ²⁰⁷ F		014 0.	023 5.	0 610	014 4.	0.19 0.	029 19	.003 0.	026 11	013 0.	014 0.	012 4.	.002 0.	016 1	016 0.	0.79 0.	.015 5	0.19 0.	0.19 0.	014 0.	022 0.	073 0	085 2.	012 0.	.002 0.	016 5.0	.004 4	014 0.	014 4.	015 4.	017 0.	024 2	028	019 5.	012 0	0.17 0.	013 0.	0.14 0.	028 13
	opic ratio	/ ±2,		41 0.0	16 0.0	73 0.0	29 0.0	16 0.0	93 0.0	47 0	37 0.0	96 0.0	02 0.0	69 0.0	27 0	66 0.0	69 0.0	62 0.00	0 66	86 0.0	96 0.0	85 0.0	98 0.0	52 0.0	11 0.00	83 0.0	94 0	66 0.0	14 0	94 0.0	75 0.0	9.0 0.0	79 0.0	25 0.0	55 0.0	94 0.0	98 0.0	78 0.0	88 0.0	79 0.0	83 0.0
	Isot	²⁰⁷ Pł		1 0.06	35 0.12	14 0.06	35 0.12	12 0.06	55 0.23	13 0.06	54 0.17	0.05	0.06	33 0.10	13 0.06	58 0.18	[4 0.05	1 0.057	0.2	4 0.05	[4 0.05	2 0.05	17 0.05	31 0.06	28 0.086	[4 0.05	[2 0.05	11.0 68	11 0.11	13 0.05	H 0.10	37 0.106	1 0.05	3 0.10	12 0.06	[5 0.11	51 0.05	36 0.05	78 0.05	54 0.05	8 0.18
		$\pm 2\sigma^2$		7 0.001	6 0.003	8 0.001	9 0.00	2 0.00	5 0.006	6 0.001	7 0.005	3 0.00	1 0.001	3 0.003	1 0.001	8 0.005	1 0.001	4 0.001	2 0.009	4 0.001	0.001	3 0.001	6 0.001	3 0.003	4 0.002	1 0.001	3 0.001	5 0.003	1 0.004	4 0.001	6 0.004	2 0.0008	3 0.001	4 0.00	2 0.001	3 0.001	2 0.000	2 0.000	9 0.0007	9 0.0005	2 0.001
		²⁰⁸ Pb/ ²³² Th		0.025	0.084	0.028	0.087	0.0259	0.155	0.0257	0.129	0.025	0.0258	0.081	0.0291	0.153	0.028	0.0284	0.120	0.027	0.029	0.0280	0.031	0.031	0.073	0.0303	0.0315	0.096	0.084	0.0281	0.096	0.0871	0.029	0.092	0.030	10.097	0.0287	0.0261	0.028	0.0278	0.143
		±2σ ²	19T)	0.25	0.49	0.36	0.54	0.46	0.66	0.18	0.39	0.29	0.23	0.42	0.25	0.32	0.32	0.61	.0.1	0.33	0.53	0.25	0.43	0.45	0.72	0.57	0.18	0.8	1.2	0.28	0.72	0.15	0.29	0.36	0.21	0.14	0.19	0.18	0.56	0.11	0.087
		²⁰⁸ Pb/ ²⁰⁶ Pb	id Zone	2.92	6.67	4.66	7.7	5.99	9.1	2.27	5.45	3.997	3.165	5.92	3.27	4.489	4.07	8.56	1.074	4.23	6.73	3.29	5.27	4.53	10.29	7.52	2.469	11.7	7.6	3.72	9.38	4.875	5.68	6.37	4.83	4.485	4.67	4.07	6.9	3.013	2.738
		²⁰⁶ Pb/ ²⁰⁴ Pb	4291N; Gr	21000	59000	23300	205000	12300	38000	3000	34000	13800	16900	00069	7600	74000	3600	29000	124	5100	5300	9100	11100	0069	203000	0069	14200	143000	28000	12800	92000	12600	1790	6000	2200	13700	10300	3000	5100	9200	26000
	1S ¹	hTh	4E, 499	1.19	2.81	2.32	3.50	2.77	3.58	0.96	1.97	1.55	1.10	1.55	1.09	1.34	1.38	2.88	1.27	1.56	2.37	1.06	0.95	0.79	1.71	1.29	0.40	1.96	1.13	0.58	1.41	1.34	1.64	2.82	1.51	1.25	1.38	1.19	2.07	0.88	0.73
	ntratior	l (mqq	67889.	306	85.8	138	232.1	78.3	37.9	71	55.4	267	310	335	211	310	81.3	375	195.4	86.4	66.3	191.7	43.6	43.8	216.4	69	230	105.3	48.94	123	74.4	224.8	44.5	394	96.4	144.8	222.5	79.4	112.8	220	179
	ed conce	l) (lượ D	- MTU)	363	40.9	320	812	217	35.6	68.3	109	413	42.2	519	231	414	11.8	1081	47.9	34.9	157	02.7	41.6	34.8	371	89.1	92.2	206	55.2	71.8	04.9	301	73	1110	45.4	181	308	94.2	234	193	29.9
ued.	Measure	ld) (mdd dd	uns Creek	75.3	67.2 2	37	185	18.8	53.3 1	16.4	62.5	59.4	69.6	228	51.3	386	18.3 1	86.6	202 2	20 1	17.5	48.8 2	16.29	17.5	188.8	25.3	86.3	127.6	49.4	41.9	84.9 1	180.3	11.79	331.2	28.9 1	127.9	58.5	18.77	29.9	56.9	237 1
TableA2. Contin		Analysis Identifier (_j	NB12-315 Buckma	NB315a_01	NB315a_02	$NB315a_03$	$NB315a_04$	NB315a_05	NB315a_06	NB315a_07	NB315a_08	$NB315a_09$	NB315a_10	NB315a_11	NB315a_12	NB315a_13	NB315a_14	NB315a_15	NB315a_16	NB315a_17	NB315a_19	$NB315a_20$	NB315a_21	$NB315a_22$	NB315a_23	NB315a_24	NB315a_26	NB315a_27	NB315a_28	NB315a_29	NB315a_30	NB315b_01	$NB315b_03$	$NB315b_04$	$NB315b_05$	$NB315b_06$	$NB315b_07$	$NB315b_09$	$NB315b_10$	NB315b_11	NB315b_12

3 0.0053	.00 0.17 0.3721 0.0053	8 0.0014 5.03 0.16 0.3159 0.0064 87 0.0022 7.07 0.17 0.3721 0.012 44 0.00089 3.375 0.038 0.263 0.0053	0.0019 0.1287 0.0022 7.07 0.17 0.3721 0.012 0.00084 0.0904 0.00089 3.375 0.038 0.263 0.0053	3 0.1062 0.0019 0.1287 0.0022 7.07 0.17 0.3721 0.012 2 0.07594 0.00084 0.0904 0.0904 0.0053 3.375 0.038 0.263 0.0053	6.946 0.2 0.07594 0.00084 0.0904 0.00089 3.375 0.038 0.263 0.0053	170000 6.946 0.2 0.07594 0.00084 0.0904 0.00089 3.375 0.038 0.263 0.0053	900 190.1 4.73 190000 16.68 0.63 0.1062 0.0019 0.1287 0.0022 7.07 0.17 0.3721 0.012 02 471.8 1.91 170000 6.946 0.2 0.07594 0.00084 0.0904 0.00089 3.375 0.038 0.263 0.0053
0.265 0.05515 0.05515 0.055515 0.03515 0.03515 0.1305 0.1305 0.1305 0.1305 0.1305 0.1305 0.1305 0.1305 0.1305 0.1305 0.0906 0.09076 0.09076 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.09177 0.01187 0.01187 0.01187	 	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6.946 0.2 0.07594 0.0084 0.9004 0.0089 3.375 0.033 3.221 0.12 0.02799 0.00052 0.0575 0.0013 0.731 0.0355 5.311 0.16 0.153 0.00252 0.0575 0.0013 0.731 0.0255 5.311 0.16 0.153 0.00055 0.05846 0.0011 0.902 0.0254 0.0021 0.0254 0.0311 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03254 0.03256 0.03256 0.03256 0.03256 0.03256 0.03256 0.03256 0.03256 0.03256 0.03256 0.03256 0.032566 0.032566 0.0225666667 $0.0256667676666666666666666666666666666666$	$ \begin{array}{llllllllllllllllllllllllllllllllllll$	190.1 $4.7.3$ 170000 6.946 0.2 0.0025 0.0024 0.00024 0.0024 <th< td=""></th<>

		%	97.3	99.7	95.8	99.0	101.6	98.9	88.2	99.7	100.2	99.5	100.3	97.9	98.5	100.3	94.6	99.4	100.6	98.9	97.3	92.0	96.8	95.2	99.2	100.6	98.4	98.7	94.5	100.7	75.3	100.2	99.2	100.3	97.2	100.5	100.1	100.2	100.8	98.7	96.5
		$\pm 2\sigma^2$	11	Π	14	14	Π	11	13	15	60	22	15	16	38	52	25	15	22	42	15	15	14	40	35	46	15	16	35	15	15	14	14	45	25	33	46	16	31	6.3	7.6
		²⁰⁶ Pb/ ²³⁸ U	545.7	559.3	534.5	587	562.7	552.6	607.5	560.2	2610	813.3	548.2	558.9	1537	2141	606	528.1	795.5	1460	551	517.3	540.9	1613	1357	1859	531.8	566.4	1058	576.5	561.4	537.1	521.3	1793	928	1186	1586	572.9	1201	576.2	541.6
	(Ma)	$\pm 2\sigma^2$	13	12	21	16	7.8	14	25	11	22	14	12	12	20	21	17	11	15	22	12	17	12	20	19	21	13	12	24	11	38	=	12	21	17	20	25	14	19	9.2	10
	ed ages	⁰⁷ Pb/ ²³⁵ U	561	561	558	593	554.1	559	689	561.8	2604	817.3	546.8	570.8	1560	2135	961	531.5	790.5	1476	566.4	562	559	1694.2	1368	1847	540.5	573.7	1120	572.5	746	535.9	525.4	1788	955	1180	1584	572	1191	583.7	561
	alculate	$\pm 2\sigma^2$	48	46	73	57	35	56	62	53	38	49	53	55	43	41	46	58	55	50	58	82	62	45	47	43	62	57	56	54	120	60	64	42	48	50	45	71	52	42	51
	С	⁰⁷ Pb/ ² ⁰⁶ Pb	398	418	444	415	391	347	788	780	2764	1023	744	799	1735	2249	1203	658	849	1414	516	604	523	1709	1310	1762	499	543	1209	632	1370	626	645	1873	1132	1277	1692	683	1291	602	646
		$\pm 2\sigma^2$	9.6	Π	17	19	8.8	9.9	26	31	140	48	30	33	90	120	84	30	46	95	32	33	32	97	77	100	31	33	85	33	68	30	31	97	52	73	16	34	71	24	23
		⁸ Pb/ ² ³² Th	531.4	557	554	616	555.7	541.3	649	550.6	2582	860	543.4	578	1645	2183	1513	529	796	1252	558	554	558	1713	1397	1834	540	575	1406	584.5	775	544.2	522	1796	953	1226	1638	564	1213	583	551
		ho ³ 20	27908	60523	807494	28514	372612	647321	58975	46025	63602	96214	24444	647148	10864	64373	67339	31076	39383	62948	528361	744803	81882	76244	62145	65354	57394	79723	34465	87492	94573	33582	60782	81815	181936	646837	05752	15027	616819	00784	05182
		R	9 0.7	9 0.7	3 0.78	3 0.72	9 0.68	9 0.50	2 0.9	6 0.54	4 0.62	8 0.6	6 0.62	6 0.50	6 0.6	1 0.59	4 0.6	5 0.53	8 0.5	3 0.6	5 0.55	5 0.23	4 0.42	8 0.57	6 0.6	4 0.62	5 0.57	7 0.59	5 0.68	6 0.58	6 0.30	4 0.48	3 0.43	3 0.62	4 0.6	52 0.6	1 0.73	7 0.42	8 0.55	1 0.47	2 0.20
		$\pm 2\sigma^2$	0.00	0.001	0.002	0.002	0.001	0.001	0.002	0.002	0.01	0.003	0.002	0.002	0.007	0.01	0.004	0.002	0.003	300.0	0.002	0.002	0.002	0.00	0.00	0.00	0.002	0.002	0.00	0.002	0.002	0.002	0.002	0.005	0.004	0.00	00.0	0.002	0.005	0.001	0.001
		²⁰⁶ Pb/ ²³⁸ U	0.0883	0.09064	0.0865	0.0953	0.09122	0.08952	0.0988	0.0908	0.4993	0.1345	0.0888	0.0906	0.2692	0.3942	0.1514	0.0854	0.1314	0.2542	0.0892	0.0836	0.08754	0.2844	0.2343	0.3343	0.086	0.0918	0.1785	0.0936	0.091	0.08689	0.08423	0.3207	0.1548	0.202	0.2792	0.0929	0.2049	0.0935	0.0874
		$\pm 2\sigma^2$	0.023	0.021	0.037	0.029	0.013	0.023	0.05	0.019	0.29	0.03	0.02	0.02	0.096	0.18	0.044	0.019	0.031	0.094	0.02	0.031	0.02	0.11	0.072	0.13	0.022	0.021	0.071	0.02	0.086	0.019	0.019	0.12	0.042	0.064	0.12	0.025	0.06	0.016	0.017
		²⁰⁷ Pb/ ²³⁵ U	0.741	0.74	0.737	0.796	0.727	0.738	0.981	0.74	12	1.238	0.715	0.755	3.641	7.183	1.579	0.689	1.18	3.282	0.748	0.744	0.735	4.311	2.85	5.173	0.705	0.761	2.019	0.757	1.111	0.696	0.679	4.817	1.565	2.203	3.78	0.759	2.238	0.778	0.739
	atios	±2σ ²	0.0012	0.0011	0.0019	0.0014	0.00085	0.0014	0.002	0.0017	0.0044	0.0017	0.0016	0.0017	0.0025	0.0034	0.002	0.0017	0.0018	0.0023	0.0015	0.0027	0.0017	0.0026	0.002	0.0025	0.0016	0.0015	0.0023	0.0015	0.0068	0.0017	0.0018	0.0027	0.0019	0.0021	0.0025	0.0021	0.0022	0.0011	0.0015
	Isotopic 1	⁰⁷ Pb/ ²⁰⁶ Pb	0.0551	0.0555	0.0562	0.0554	.05468 (0.0539	0.0658	.06527	0.1927	.07336	.06425	.06584	.10634	0.1421	.08018	0.0618	0.0677	0.0896	.05787	0.0612	0.0582	0.105	.08492	10791.	0.0575	.05857	0.0807	96090.	0.0922	0.0609	0.0613	.11472	.07755	0.0835	0.1039	0.063	0.0842	0.0602	0.0617
		±2σ ²	0.0005	.00055	.00088	86000.	.00045 0	0.0005	0.0013	0.0016 0	0.0076	0.0025 0	0.0015 0	0.0017 0	0.0048 0	0.0064	0.0045 0	0.0015	0.0024	0.005	0.0016 0	0.0017	0.0016	0.0052	0.0041 0	0.0054 0	0.0016	0.0017 0	0.0045	0.0017 0	0.0035	0.0015	0.0016	0.0052 0	0.0027 0	0.0038	0.0049	0.0017	0.0037	0.0012	0.0012
		¹⁸ Pb/ ³² Th	.02664	02796 0	.02781 0	03097 0	02788 0	.02714	0.0327	.02762	0.1363	.04346	.02725	.02901	0.0848	0.1141	0.0777	.02655	.04019	0.064	.02798	.02779	.02798	0.0885	0.0716	0.095	0.0271	.02888	0.0721	.02934	0.0392	.02729	.02615	0.0929	.04827	0.0625	0.0844	.02829	0.0619	02929	.02765
		2σ ² 20	0.11 0	0.16 0	0.2 0	0.2 0	0.11 0	0.14 0	0.26	0.15 0	0.13	1.2 0	.083 0	0 200.	0.23	0.1	0.44	0.15 0	0.1 0	0.67	0.17 0	0.2 0	0 660.	0.25	.086	0.23	0.12	.073 0	0.38	0 960.	0.23	.054 0	0.15 0	0.12	0.1 0	0.24	0.12	0.17 0	0.24	0.18 0	0.22 0
		Pb/ [±] dq	.508	4.66	4.99	3.9	.744	3.41	5.3	5.95	.464	18.9	.597 0	.949 0	9.57	.892	2.95	3.52	.352	7.78	5.19	4.66	.778 0	8.34	.261 0	8.88	3.27	.651 0	9.86	.638 0	4.28	.598 0	4.54	.455	.116	9.43	.275	5.38	8.85	ŝ	4.25
		208	000 3	000	000	000	000 3	000	000	000	000 6	000	000 2	000 3	000	000 4	000 1	000	000 4	000 1	000	000	000 3	000	000 4	000	800	000 2	000	000 4	400	100 2	000	000 5	900 4	000	000 5	100	006	000	000
		²⁰⁶ Pb/ ²⁰⁴ Pb	410	42(48(19(42(48(41(32(230(330(92(48(139(64(130	34(18(310	32(20(19(14(33(1050	12	15(30(700	ý	19	12(28(22	28(46	3	5	16	50
	18 ¹	J/Th	1.02	1.37	1.60	1.09	1.09	0.96	1.61	2.06	1.99	6.09	0.83	1.33	2.98	1.42	6.25	1.03	1.29	3.93	1.53	1.43	1.15	2.49	1.26	2.36	0.94	0.79	3.95	1.28	1.52	0.72	1.21	1.39	1.12	2.46	1.41	1.47	2.35	0.83	1.35
	ntration	Th (mqq	132.2	116.9	77	140	389	121.3	41.2	107.8	142.3	222	509	207.8	246	77.5	54.6	122.6	61.7	122	82.2	79.4	129.9	59.5	96.5	65	108	401	44.84	205.9	173.9	213.6	101.8	156.4	413	61.7	106.6	47.2	27.1	237	76.5
	ed conce	l) (mq U	134.8	160.1	123.2	152	424	115.9	66.5	222	283	1352	422	276	733	110.4	341.5	126.1	79.3	480	125.4	113.6	148.9	148	122	153.7	102	317	176.9	263	264.5	154.3	122.7	218	461	152	150.5	69.2	63.8	196	103.1
.ned.	Measur	d) (mqq d	32.9	30.5	20.07	39.1	100.4	30.7	12.6	27.9	181.8	89.8	129.5	56.8	193.2	84.4	39	31.3	23.93	72.6	22.8	21.7	35.2	51.2	6.99	58.1	27.9	109.5	31.4	51.8	55.7	49.9	22.4	123.5	169.4	31.2	76	11.34	14.19	63.1	19.85
2. Contin		lysis ifier (24	25	26	27	28	29	30	01	02	03	04	05	06	07	08	60	_10	11	12	_13	_14	.15	_16	17	.18	_19	20	21	22	23	24	25	26	27	28	29	30	01	02
TableA		Anal Ident	NB315c_	NB315c_	NB315c_	NB315c_	NB315c_	NB315c_	NB315c_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315d_	NB315e_	NB315e_

TableA2. Con	tinued.																								
	Meast	ired coi	ncentrati	ons ¹						Isotopic	ratios								Ca	lculate	d ages (N	fa)			
Analysis Identifier	Pb (mqq)	U (ppm)	Th (ppm)	U/Tħ	²⁰⁶ Pb/ ²⁰⁴ Pb	²⁰⁸ Pb/ ²⁰⁶ Pb	±2σ ²	²⁰⁸ pb/ ²³² Th	±2σ ²	²⁰⁷ pb/ ²⁰⁶ pb	$\pm 2\sigma^2$	²⁰⁷ Pb/ ²³⁵ U	±2\sigma^2	²⁰⁶ Pb/ ²³⁸ U	±2σ ²	Rho ³	²⁰⁸ pb/ ² ³² Th ±	$2\sigma^2$	⁷ Pb/ ² ± ⁵⁶ Pb [±]	$2\sigma^2$	⁷ Pb/ ³⁵ U ^{±2}	0 ² 200	Pb/ *U ±2	ن م2	.o F
NB315e_03	15.25	116.4	60.7	1.92	10000	6.46	0.33	0.02686	0.0011	0.0584	0.0011	0.709	0.014	0.08818	0.00091	0.3475069	536	22	530	42	543.2	8.3	44.7	5.4 100).3
NB315e_04	52.5	267.8	251.1	1.07	20000	4.069	0.2	0.02216	0.00099	0.0635	0.0013	0.771	0.02	0.0885	0.0015	0.6153002	443	20	719	43	580	11	46.6	9.2 94	1.2
NB315e_05	274	243	195	1.22	20000	4.9	0.47	0.1514	0.0067	0.1868	0.0018	13.2	0.22	0.5147	0.008	0.8232209	2847	120	2712	16	2692	16	2675	34 99	9.4
NB315e_06	23.2	109.7	95.6	1.15	16000	4.041	0.2	0.02644	0.0011	0.0586	0.0012	0.705	0.016	0.08689	0.00099	0.4361122	527	21	547	49	540.8	9.6	537	56 6.5	9.3
NB315e_07	18.81	91.7	78.5	1.16	1000	4.01	0.2	0.02601	0.0011	0.0595	0.0013	0.693	0.016	0.0845	0.0011	0.3745602	519	23	570	49	533.5	9.5	23.1	6.3 98	3.1
NB315e_08	42.5	149.9	164.7	0.91	30000	3.003	0.14	0.02783	0.0011	0.0585	0.0011	0.725	0.011	0.09029	0.00098	0.016878	554.7	21	534	40	552.8	6.8	57.2	5.8 100).8
NB315e_09	28.7	164	115.1	1.42	21000	4.81	0.24	0.027	0.0011	0.0595	0.0011	0.709	0.014	0.08687	0.0009	0.3799605	538	22	579	38	544.9	8.6	537	5.4 98	3.6
NB315e_10	12.11	59.1	44.3	1.33	5000	4.61	0.24	0.02949	0.0013	0.0609	0.0012	0.835	0.019	0.0991	0.0012	0.5010813	587	26	633	46	615	10	609	7.3 99	0.6
NB315e_11	31.8	172	134.2	1.28	17000	4.33	0.22	0.02557	0.001	0.0582	0.0011	0.685	0.013	0.08574	0.00089	0.2809545	510.3	20	522	41	528.8	7.6	30.3	5.3 100).3
NB315e_12	32.1	174	134.2	1.30	40000	4.381	0.22	0.02566	0.001	0.0579	0.001	0.678	0.013	0.08526	0.00095	0.4528638	512.1	20	512	40	524.6	7.6	27.4	5.6 100).5
NB315e_13	83.5	411	336	1.22	23000	4.026	0.19	0.02677	0.001	0.05871	0.0007	0.708	0.01	0.08727	0.00088	0.558252	533.9	20	550	26	542.9 (6.1	39.3	5.2 99	9.3
NB315e_14	23.09	146.2	94.1	1.55	11000	5.08	0.26	0.02691	0.0012	0.0622	0.0018	0.697	0.019	0.0819	0.00096	0.0673279	537	23	659	58	536	11	07.4	5.7 94	1 .7
NB315e_15	30.2	139.7	130	1.07	00006	3.634	0.17	0.02505	0.00099	0.0585	0.001	0.669	0.012	0.08321	0.00091	0.380136	500	19	538	38	519.2	7.3	15.2	5.4 99	9.2
NB315e_16	58.7	457	225.5	0.202	00006	6.91	0.33	0.02834	0.0011	0.05965	0.00067	0.758	0.011	0.0923	0.001	0.6417968	564.8	22	586	24	572.3	6.5	69.1	6.1 99	9.4
NB315e_17	90.2	186.8	172.6	1.08	13000	3.795	0.19	0.05667	0.0021	0.0802	0.00098	2.12	0.032	0.1922	0.0026	0.640383	1114	41	1197	24	1154	11	1133	14 98	8.2
NB315e_18	108.8	218.8	126.1	1.74	105000	6.38	0.3	0.094	0.0036	0.1224	0.0012	5.462	0.072	0.3241	0.0034	0.6786632	1816	67	1989	18	1894	11	1809	16 95	5.5
NB315e_19	26.5	208	105.5	1.96	14000	6.64	0.32	0.0269	0.0011	0.05866	0.00079	0.728	0.011	0.09044	0.00098	0.5019068	536	21	546	30	555	6.5	58.1	5.8 100).6
NB315e_20	28.65	130.1	124.4	1.05	1600	3.651	0.18	0.02515	0.001	0.0601	0.001	0.685	0.014	0.08297	0.00086	0.58603	502	20	598	39	528.9	8.3	13.8	5.1 97	7.2
NB315e_21	7.9.7	217	315	0.68	18000	2.282	0.11	0.02718	0.001	0.05804	0.00083	0.7135	0.0096	0.0896	0.001	0.336594	542.1	20	527	32	546.4	5.7	53.3	6 101	L.3
NB315e_22	60.8	246	251.5	0.98	18000	3.363	0.17	0.02624	0.001	0.05845	0.00089	0.706	0.013	0.0879	0.0011	0.5724344	523.5	20	540	33	541.7	7.5	42.9	6.3 100).2
NB315e_23	32.4	215	134.1	1.60	17000	5.24	0.26	0.02614	0.0011	0.05888	0.00089	0.677	0.011	0.08339	0.00079	0.4069205	521	21	553	33	524.4	6.4	16.3	4.7 98	3.5
NB315e_24	120.4	939	454.4	2.07	12000	6.67	0.33	0.02894	0.0013	0.0602	0.0011	0.766	0.019	0.09194	0.0009	0.7767253	576	25	598	35	576	10	567	5.3 98	8.4
NB315e_25	45.2	61.8	5(1.24	20000	4.65	0.29	0.0981	0.004	0.1199	0.0016	5.787	0.087	0.3518	0.0041	0.5244095	1890	73	1950	23	1943	13	1942	19 95	6.6
NB315e_26	59.1	292.1	236.8	1.23	20000	4.214	0.21	0.027	0.001	0.0618	0.0012	0.759	0.015	0.0895	0.00091	0.2909111	538.4	20	654	40	572.2	8.7	52.5	5.4 96	9.6
NB315e_27	278.3	250.4	304.5	0.82	75000	3.035	0.14	0.0999	0.0036	0.12051	0.00085	5.846	0.049	0.352	0.0029	0.6399274	1924	67	1964	12 1	952.7	7.3	1944	14 95	9.6
NB315e_28	106.3	298	157.2	1.90	51000	6.88	0.33	0.07354	0.0027	0.09619	0.00077	3.534	0.043	0.2668	0.0025	0.7532943	1434	52	1549	15 1	533.7	9.5	1524	13 99	9.4
NB315e_29	77	354.7	118.4	3.00	32000	11.4	0.69	0.0707	0.0027	0.09206	0.00064	3.162	0.035	0.2498	0.0025	0.7869409	1384	53	1466	13 1	448.3	8.3	1437	13 99	9.2
NB315e_30	24.9	146	5.66	1.47	2900	4.98	0.25	0.02723	0.0011	0.0614	0.0012	0.755	0.016	0.08944	0.00096	0.4008179	543	21	639	43	570.3	9.5	52.1	5.6 96	9.8
NB315f_01	46.9	293	186	1.58	30000	5.5	0.32	0.0269	0.0011	0.0627	0.0017	0.775	0.026	0.0886	0.0013	0.6151961	536	21	684	51	581	14	47.3	7.4 94	1 .2
$NB315f_02$	117	306	244	1.25	30000	4.96	0.45	0.0529	0.002	0.0738	0.0012	1.723	0.029	0.1702	0.0025	0.4745635	1041	38	1030	33	1019	12	1013	14 95	9.4
NB315f_03	65	241	176	1.37	30000	4.87	0.23	0.04086	0.0014	0.06728	0.00097	1.257	0.02	0.1354	0.0014	0.4625932	809	27	839	30	825.8	8.7	:18.7	26 6.7	9.1
$NB315f_04$	105.2	137.6	116	1.19	34000	4.429	0.19	0.0988	0.0032	0.1225	0.0012	5.995	0.075	0.3547	0.0039	0.6595387	1904	59	1990	18	1974	11	1957	19 95	9.1
$NB315f_05$	15.63	62.05	58.85	1.05	500	3.56	0.21	0.0296	0.0015	0.0739	0.0027	0.907	0.033	0.0887	0.0014	0.2072425	590	29	1014	73	653	17	47.7	8.1 8	3.9
NB315f_06	98	359	202	1.78	93000	5.8	0.27	0.0521	0.0022	0.078	0.0012	1.798	0.037	0.1678	0.0027	0.673009	1027	42	1142	31	1043	13	666	15 9	5.8
NB315f_07	35.2	169	116.6	1.45	35000	4.58	0.26	0.0319	0.0014	0.068	0.0021	0.881	0.03	0.0934	0.0012	0.4238884	635	27	868	99	641	16	76.9	7.3 9(0.0
NB315f_08	38.8	244	157.8	1.55	70000	5.41	0.25	0.02693	0.00091	0.05957	0.00099	0.733	0.013	0.0892	0.001	0.4124917	537.1	18	578	37	557.6	7.5	50.7	6.2 98	8.8
NB315f_09	20.92	80.7	78.3	1.03	00006	3.22	0.18	0.0294	0.0014	0.0759	0.004	0.875	0.048	0.0831	0.0015	0.2816301	585	28	1060	100	633	25	14.6	8.8	1.3
$NB315f_10$	39.4	185	162	1.14	70000	4.07	0.21	0.0265	0.00092	0.05855	0.00092	0.691	0.012	0.0856	0.0011	0.4925028	529	18	541	34	532.8	5	29.3	6.5 9	9.3
NB315f_11	16.82	369	48.41	7.62	110000	27.9	1.5	0.0381	0.0016	0.06536	0.00098	1.137	0.02	0.1257	0.0016	0.5507305	756	30	780	32	770.3	9.3 7	63.1	9.3 9.	9.1

TableA2. Continu	ıed.																							
	Measur	ed conc	entratio	ns ¹						Isotopic 1	atios								Calcu	ılated aş	ges (Ma			
Analysis Identifier (p	Pb pm) (p	U (ud	Th (ppm)	U/Th	²⁰⁶ Pb/ ²⁰⁴ Pb	²⁰⁸ Pb/ ²⁰⁶ Pb	$\pm 2\sigma^2$	²⁰⁸ Pb/ ²³² Th	$\pm 2\sigma^2$	⁰⁷ Pb/ ²⁰⁶ Pb	±2σ ²	⁰⁷ Pb/ ²³⁵ U	²⁰ 2	⁶ Pb/ ²³⁸ U	±2σ ² R	ho ³ ²⁰	⁵ Pb/ ² ² Th ^{±2}	$\sigma^2 \frac{^{207}}{^{06}}$	b/ ² 2b ±2σ	2 ²⁰⁷ Pb	/ ±2σ ²	²⁰⁶ Pb	, ±2σ ²	% con
NB315f_12	64.4	62.9	95.1	0.66	50000	2.484	0.12	0.0738	0.0025	0.095	0.0016	3.318	0.058	0.2527	0.0036 0.45	614762	1438	48 1	521 3.	2 148	34 14	145	2 19	97.8
NB315f_13	107.4	228.1	132.6	1.72	600000	3.92	0.19	0.0866	0.0031	0.1022	0.002	2.808	0.074	0.2002	0.0048 0.70	14206	1679	57 1	660 3	6 135	56 20	117	6 25	86.7
$NB315f_14$	63.7	148.4	91.2	1.63	00006	5.901	0.26	0.0761	0.0025 0	.09565	0.0011	3.458	0.036	0.2616	0.0025 0.33	89965	1482	46 1	537 2	2 1516	.8 8.3	149	8 13	98.8
NB315f_15	7.97	365	8.6	42.44	100000	149.9	8	0.1014	0.0045 0	.11705	0.0011	5.418	0.067	0.3351	0.0039 0.69	50185	1949	83 1	911 1	8 188	36 11	186	2 19	98.7
$NB315f_{-}16$	45	288.3	200.6	1.44	29000	5.162	0.23	0.0243	0.00078 0	.05864 (0.00083	0.666	0.011	0.0823	0.001 0.54	83517	485.2	15	546 3	1 517	.8 6.6	51	0 5.9	98.5
$NB315f_17$	47.5	140.9	197	0.72	50000	2.536	0.12	0.02628	0.00093	0.0584	0.0012	0.71	0.014	0.0882	0.0011 0.24	83244	524	18	530 4	6 543	8.8	544	6 6.4	100.1
NB315f_18	74.2	319	285	1.12	44000	3.67	0.18	0.02822	0.0011	0.0618	0.0014	0.782	0.022	0.0921	0.0019 0.60	63828	562	23	657 4	8	36 12	56	8 11	96.9
$NB315f_19$	89.4	219	166.5	1.32	65000	4.731	0.22	0.058	0.002	0.0803	0.0014	2.317	0.046	0.2096	0.0032 0.53	32714	1140	38 1	199 3.	5 12	16 14	122	6 17	100.8
NB315f_20	14.59	81.6	50.8	1.61	12000	5.14	0.32	0.0318	0.0016	0.0637	0.002	0.782	0.027	0.0888	0.0018 0.44	09434	632	32	713 6	6 55	35 16	54	8 11	93.7
NB315f_21	41.9	241.6	164.4	1.47	43000	5.14	0.25	0.0279	66000.0	0.0595	0.0012	0.732	0.017	0.0885	0.0012 0.50	124741	556	20	586 4	5	57 10	546	3 7.3	98.1
NB315f_22	86.8	293	356	0.82	30000	2.71	0.15	0.02647	0.001	0.0693	0.002	0.793	0.024	0.084	0.002 0.4	50985	528	20	893 6	2	95 15	52	0 12	87.4
NB315f_23	37.3	200	160	1.25	18000	4.78	0.28	0.02588	0.00097	0.0581	0.0011	0.673	0.015	0.084	0.0011 0.53	07124	516	19	524 4	3 521	.7 8.8	519	8 6.3	9.66
NB315f_24	51.4	249.6	198.3	1.26	11000	4.07	0.21	0.02789	0.0011	0.0654	0.0028	0.763	0.033	0.0845	0.0011 0.18	33833	556	21	780 9	0	73 18	522	7 6.6	91.2
NB315f_25	27.6	151.6	111.4	1.36	80000	4.57	0.22	0.02712	0.00099	0.0616	0.0013	0.735	0.016	0.0863	0.001 0.32	26472	541	20	650 4	7 558	.4 9.5	533.	3 6	95.5
NB315f_26	229	285	280	1.02	100000	3.87	0.17	0.0896	0.0029	0.1091	0.0013	4.649	0.064	0.3078	0.0033 0.5	50418	1735	53 1	782 2	2 175	57 12	173	0 16	98.5
NB315f_27	170.2	931	382.2	2.44	130000	8.85	0.38	0.04829	0.0015 0	.07223 (0.00067	1.671	0.018	0.1677	0.0017 0.6	607867	953	29	992 1	8 996	.8 6.8	666	1 9.3	100.2
NB315f_28	36	145	145	1.00	0	3.552	0.17	0.02713	0.00094	0.0585	0.0012	0.735	0.016	0.0911	0.0011 0.37	'83494	541	18	539 4	6 5(50 9.3	562	1 6.7	100.4
NB315f_29	63.1	256.6	244.6	1.05	00006	3.687	0.18	0.02829	0.0011	0.0626	0.0021	0.773	0.027	0.0892	0.0011 0.28	64193	564	21	679 6	5 56	30 15	550	6 6.6	94.9
NB315f_30	116.5	862	479	1.80	300000	6.473	0.28	0.02654	0.00087 0	.05807 (0.00064 (.7284 (0.0092	0.091	0.0011 0.60	31709	529.4	17	531 2	5 555	.3 5.4	561.	5 6.4	101.1
NB315g_01 2	245.2	947	373	2.54	220000	9.59	0.36	0.0675	0.0014 0	.09543 (0.00088	3.591	0.051	0.2698	0.0036 0.77	75842	1321	26 1	534 1	7 154	47 II	153	9 18	99.5
NB315g_02	23.4	145	98.3	1.48	12000	4.99	0.2	0.02467	0.00056	0.06 (0.00095	0.702	0.011 0	.08469 (0.00093 0.3	35405	492	11	593 3.	4 540	.7 6.7	. 52	4 5.5	96.9
NB315g_03	60.4	363.4	77	4.72	16000	21.3	1.9	0.0826	0.0016 0	.11149 (0.00086	4.808	0.058	0.3107	0.0036 0.78	379638	1603	29 1	824 1	4 178	35 10	174	4 18	97.7
NB315g_04	27	147.6	115.3	1.28	0	4.49	0.18	0.02445	0.00051	0.0603	0.0012	0.706	0.016	0.0845	0.0011 0.48	64734	488	10	615 4	4 541	.3 9.2	523	1 6.3	96.5
NB315g_05	49.2	131	95.6	1.37	30000	5.05	0.26	0.0555	0.0011 0	.07895 (76000.0	2.109	0.03	0.1926	0.0024 0.58	\$29705	1091	20 1	165 2	4 1150	9.6 9.8	113	5 13	98.6
NB315g_06	14.9	57	55.8	1.02	4400	3.8	0.27	0.0277	0.0011	0.0613	0.0018	0.741	0.022	0.0874	0.0013 0.27	22793	552	22	619 6	5	51 13	539	8	96.2
NB315g_07	77.3	199.6	100.1	1.99	59000	7.413	0.26	0.0825	0.0012 0	.10742 (86000.0	4.546	0.055	0.3054	0.0032 0.68	820824	1602	23 1	753 1	7 1738	.3 10	171	8 16	98.8
NB315g_08	58.2	314.8	259.8	1.21	26000	4.277	0.16	0.02393	0.00039 0	.05904 (0.00088	0.676	0.01 0	.08293 (0.00087 0.34	138478	478	7.7	559 3	3.	24 6.3	513	6 5.2	98.0
NB315g_09	101	115.1	86.5	1.33	25000	5.05	0.19	0.1264	0.0026	0.1797	0.0023	11.14	0.24	0.4499	0.0069 0.81	04089	2405	46 2	648 2	1 253	33 20	239	4 30	94.5
NB315g_10	26.3	103	100	1.03	800	3.6	0.18	0.02861	0.0008	0.0636	0.0016	0.832	0.022	0.0952	0.0015 0.37	75149	570	16	721 5	2 6.	13 13	586	2 8.9	95.3
NB315g_11	185	297	140	2.12	120000	7.33	0.31	0.1505	0.0047	0.239	0.0026	16.15	0.4	0.491	0.011 0.89	83976	2832	82 3	111	8 288	33 24	257	4 47	89.3
NB315g_12	55.5	234	222	1.05	18000	3.89	0.21	0.02846	0.00061 0	.05908	0.00092	0.727	0.012	0.0896	0.0011 0.44	58169	567	12	560 3.	4 554	.2 6.9	553	1 6.6	99.8
NB315g_13	16.5	95.6	65.3	1.46	50000	5.1	0.24	0.02785	0.00067	0.0599	0.0013	0.728	0.016 0	.08834 (0.00096 0.27	73907	555	13	581 4	7 554	.1 9.1	545	7 5.7	98.5
NB315g_14	59.8	176.8	221.4	0.80	20000	2.695	0.1	0.03019	0.00055	0.0611	0.001	0.806	0.015	0.096	0.0013 0.51	95274	601	11	633 3	5 599	.6 8.4	590	8 7.4	98.5
NB315g_15	28.5	86.7	70.9	1.22	10900	2.75	0.13	0.0445	0.0017	0.1113	0.0039	1.422	0.055	0.0928	0.0013 0.42	85439	880	33 1	796 6	6 85	96 24	57	2 7.9	63.8
NB315g_16	54.1	515	221.8	2.32	00006	8.24	0.31	0.02723	0.00046 0	.05847 (0.00063	0.737	0.01	0.0916	0.001 0.63	18556	542.9	9.1	542 2	3 560	.2 5.9	56	5 6	100.9
NB315g_17	42.4	203	179	1.13	21000	3.9	0.16	0.0261	0.00066	0.0587	0.0012	0.705	0.016	0.0872	0.0012 0.45	87154	521	13	545 4	5 542	.5 9.9	538	9 7.1	99.3
NB315g_18	51.2	291.4	161.2	1.81	70000	5.208	0.19	0.03559	0.00086 0	.06254 (.00098	0.831	0.015	0.0966	0.0011 0.51	06962	707	17	693 3.	3 614	.8 8.5	594	4 6.5	96.7
NB315g_19	125.7	454	158.3	2.87	160000	11.04	0.48	0.0876	0.0012 0	.11188 (00086	4.909	0.065	0.3184	0.0036 0.81	51592	1697	23 1	830 1	3 18(11 11	178	2 18	98.9
NB315g_20	105	203.7	150.6	1.35	35000	4.831	0.17	0.0774	0.0012	0.0958 (0.00086	3.553	0.04	0.2692	0.0028 0.65	90326	1506	23 1	541 1	7 1538	2	153	6 14	99.96

ued. Measured concentrations ¹ Isotopic rati Pb U Th 20^{6} pb/ $^{20^{8}}$ pb/ $^{20^{8}}$ pb/ $^{20^{7}}$ pb/ $^{20^{7}}$ pb/ pm) (ppm) (ppm) U/Th $^{20^{6}}$ pb/ $^{20^{6}}$ pb/ $^{20^{5}}$ pb/ $^{20^{2}}$ pb/ $^{20^{7}}$ pb/ $^{20^{7}}$ pb/ 42.6 164.5 178.3 0.92 20000 3.164 0.14 0.02539 0.00052 0.0569 0.1 19.03 88.4 8.36 1.06 2500 3.91 0.17 0.02428 0.0061 0.0	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \frac{18^{1}}{106} = \frac{20^{6} \text{pb}}{20^{4} \text{pb}} \frac{20^{8} \text{pb}}{12\sigma^{2}} \frac{20^{8} \text{pb}}{12\sigma^{2}} \frac{10^{7} \text{pb}}{12\sigma^{$	$\frac{^{206}\text{Pb}/}{^{204}\text{Pb}} \xrightarrow{^{208}\text{Pb}/}{^{204}\text{Pb}} \frac{1 \text{ sotopic rati}}{^{205}\text{Pb}/} \frac{1 \text{ sotopic rati}}{^{207}\text{Pb}/} \frac{1 \text{ sotopic rati}}{^{207}\text{Pb}/} \frac{1 \text{ sotopic rati}}{^{206}\text{Pb}} \frac{1 \text{ sotopic rati}}{^$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{\pm 2\sigma^2}{2^{30}} \frac{^{208}\text{Pb}}{\text{Pb}} \frac{1\text{sotopic rati}}{\pm 2\sigma^2} \frac{2^{07}\text{Pb}}{^{206}\text{Pb}} \frac{\pm 2}{2^{10}} \frac{1}{2^{10}} \frac{1}{2^{1$	²⁰⁸ Pb/ Isotopic rati ²⁰⁸ Pb/ ²⁰⁷ Pb/ ±2 ²³² Th ±2\sigma ² ²⁰⁶ Pb ±2 0.02539 0.00052 0.0569 0. 0.02428 0.00079 0.061 0.	Isotopic rati 1^{207} Pb/ $\pm 2\sigma^2$ 2^{06} Pb/ 100052 0.00079 0.061 0.061	Isotopic rati ²⁰⁷ Pb/ ±2 ²⁰⁶ Pb ±0.0.00569 0.0	±2 ±2 0.0	00 016 0016	²⁰⁷ Pb/ ²³⁵ U 0.672 0.732	$\pm 2\sigma^2$ 0.02 0.023	²⁰⁶ Pb/ ²³⁸ U 0.085 0.0865	$\pm 2\sigma^2$ 0.0013 0.0013	Rho ³ 0.3613656 0.2572564	²⁰⁸ Pb/ ² ³² Th 507 485	$2\sigma^2$ 20 10 10	$\begin{array}{c} \text{Ca} \\ \text{Pb/}^2 \\ \text{fpb} \\ \text{fpb} \\ 471 \\ 639 \end{array}$	$\frac{1}{2\sigma^2}$ $\frac{2\sigma^2}{2\sigma^2}$ $\frac{2\sigma^2}{2\sigma^2}$ $\frac{1}{2\sigma^2}$	1 ages (1 ⁷ Pb/ ±: ³⁵ U ±: 521 556	$\frac{Ma}{2\sigma^2}$ $\frac{2\sigma^2}{2}$ 12	⁵⁶ Pb/ ± ²³⁸ U ± 525.8 534.5	$2\sigma^2 \frac{9}{cc}$
19.03 88.4 83.6 1.06 2500 3.91 0.17 0.02428 0.0 79.1 182.5 123.8 1.47 69000 4.99 0.2 0.0664 0 22.82 144.9 91.9 1.58 90000 5.24 0.2 0.02625 0.0	88.4 83.6 1.06 2500 3.91 0.17 0.02428 0.0 182.5 123.8 1.47 69000 4.99 0.2 0.0664 0 144.9 91.9 1.58 90000 5.24 0.2 0.02625 0.0	83.6 1.06 2500 3.91 0.17 0.02428 0.0 123.8 1.47 69000 4.99 0.2 0.0664 0 91.9 1.58 90000 5.24 0.2 0.02625 0.0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2500 3.91 0.17 0.02428 0.0 69000 4.99 0.2 0.0664 0 90000 5.24 0.2 0.02625 0.0	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	0.17 0.02428 0.0 0.2 0.0664 0 0.2 0.02625 0.0	0.02428 0.0 0.0664 0 0.02625 0.0	0.C	0079 .0013 - 0063	0.061 0.08411 0.0599	0.0019 0.00091 0.0013	0.732 2.648 0.733	0.023 0.034 0.017	0.0865 0.2267 0.0884	0.0013 0.0027 0.00099	0.2572564 0.6201043 0.370172	485 1298 524	16 24 12	639 1290 581	72 21 1 47	556 312.9 557.4	13 9.5 9.8	534.5 1317 546	7.4 9 14 10 5.8 9
48.9 236 164 1.44 27000 3.96 0.48 0.03078 25.9 114.3 106.9 1.07 13000 3.595 0.14 0.02573 37.4 18.4 153 1.20 70000 4.18 0.2 0.0547	236 164 1.44 27000 3.96 0.48 0.03078 1.14.3 106.9 1.07 13000 3.595 0.14 0.02573 1.84 153 1.20 70000 4.18 0.2 0.2517	164 1.44 27000 3.96 0.48 0.03078 106.9 1.07 13000 3.595 0.14 0.02573 153 1.20 70000 4.18 0.2 0.0547	1.44 27000 3.96 0.48 0.03078 1.07 13000 3.595 0.14 0.02573 1.00 70000 4.18 0.2 0.0517	27000 3.96 0.48 0.03078 13000 3.595 0.14 0.02573 70000 4.18 0.2 0.02617	3.96 0.48 0.03078 3.595 0.14 0.02573 4.18 0.2 0.02617	0.48 0.03078 0.14 0.02573 0.2 0.02617	0.03078 0.02573 0.02617		0.00066 0.00058 0.00058	0.0665 0.0583 0.0583	0.0014 0.0012	0.925 0.696 0.695	0.02 0.016	0.1003 0.086	0.0013 0.0011	0.343048 0.4564116 0.3506846	613 513 577	11 13	812 521 537	47 47	664 535.2 535 3	11 9.4 7.3	615.9 531.7 531 2	7.79 6.79 5.79
32 170.8 117.9 1.45 90000 4.55 0.18 0.02642 28.1 169.4 111.5 1.52 17000 5.2 0.35 0.0263	170.8 117.9 1.45 90000 4.55 0.18 0.02842 (69.4 111.5 1.52 17000 5.2 0.35 0.0263	117.9 1.45 90000 4.55 0.18 0.0263 111.5 1.52 17000 5.2 0.35 0.0263	1.45 90000 4.55 0.18 0.02842 1.52 17000 5.2 0.35 0.0263	90000 4.55 0.18 0.02842 17000 5.2 0.35 0.0263	4.55 0.18 0.02842 5.2 0.35 0.0263	0.18 0.02842 0.35 0.0263	0.02842 0.0263	-	0.00051	0.0634	0.0018	0.765	0.026	0.0932	0.0011	0.2698019	566 525	10 20	691 573	68 58 68	589 576	14	554.5 574	 6.4 9 12 9
f primary reference material 15.04 81.54 30.09 2.71 38364.94253 9.3729 0.522 0.054	reference material 31.54 30.09 2.71 38364.94253 9.3729 0.522 0.054	ce material 30.09 2.71 38364.94253 9.3729 0.522 0.054	rial 2.71 38364.94253 9.3729 0.522 0.054	8364.94253 9.3729 0.522 0.054	9.3729 0.522 0.054	0.522 0.054	0.054	12	0.0026	0.0749	0.00189	1.8559	0.0523	0.17951	0.00355	0.4940114	1065.1	9.4 1	054.7	1.8 1	063.1	3.4 1	063.8	3.7
f secondary reference material(s) 40.56 501.73 257.14 1.95 301474.7126 6.3923 0.269 0.057 6.75 202.58 26.36 7.69 35802.5 26.65 1.555 0.027 50.51 302.64 263.06 1.15 3433.89831 4.6885 0.255 0.020	ry reference material(s) 11.73 257.14 1.95 301474.7126 6.3923 0.269 0.057 12.58 26.36 7.69 35802.5 26.65 1.555 0.027 12.64 263.06 1.15 34333.89831 4.6885 0.255 0.020	ence material(s) :57.14 1.95 301474.7126 6.3923 0.269 0.057 26.36 7.69 35802.5 26.65 1.555 0.027 63.06 1.15 3433.89831 4.6885 0.255 0.020	terial(s) 1.95 301474.7126 6.3923 0.269 0.057 7.69 35802.5 26.65 1.555 0.027 1.15 3433.389831 4.6885 0.255 0.020) 01474.7126 6.3923 0.269 0.057 35802.5 26.65 1.555 0.027 4333.89831 4.6885 0.255 0.020	6.3923 0.269 0.057 26.65 1.555 0.027 4.6885 0.255 0.020	0.269 0.057 1.555 0.027 0.255 0.020	0.057 0.027 9.020	01 35 (59 (0.002 0.002 0.002 0.000149 0.00001	0.07679 0.05941 0.05616	0.00131 0.00129 0.00172	1.9806 0.7427 0.5176	0.0414 0.0169 0.0168	0.18743 0.09084 0.06693	0.00367 0.00157 0.00146	0.6451225 0.4405425 0.416241	1093.7 548.7 401.4	3.0 1 4.5 2.0	104.2 559.4 423.6	3.4 1 7.3	105.8 562.9 419.1	1.4 1 1.5 1.3	102.3 562.4 417.0	1.8 1.3 1.1
fare Formation (UTM - 680759E, 4948958N; Grid Zone 19T)	1911) 1912) 1912) 1912) 1912) 1912) 1912) 1912) 1912)	UTM - 680759E, 4948958N; Grid Zone 19T)	680759E, 4948958N; Grid Zone 19T)	ıE, 4948958N; Grid Zone 19T)	∛; Grid Zone 19T)	(2016 19T)	(.:																	
166.7 170.7 136.4 1.25 108000 4.358 0.27 0.132 137.8 349.6 134.3 2.60 300000 8.45 0.54 0.111	170.7 136.4 1.25 108000 4.358 0.27 0.132 149.6 134.3 2.60 300000 8.45 0.54 0.111	136.4 1.25 108000 4.358 0.27 0.132 134.3 2.60 300000 8.45 0.54 0.111	1.25 108000 4.358 0.27 0.132 2.60 300000 8.45 0.54 0.111	108000 4.358 0.27 0.132 300000 8.45 0.54 0.111	4.358 0.27 0.132 8.45 0.54 0.111	0.27 0.132 0.54 0.111	0.132		0.0049 0.0043	0.1629 0.1281	0.0025 0.0021	10.273 6.35	0.09 0.1	0.4572 0.3591	0.009 0.0084	0.6631424 0.7145333	2507 2140	88 78	2484 2069	20 29 29	459.1 2024	8.1	2427 1977	40 5 9
7.69 33.5 7.57 4.43 5000 13.74 1 0.11	33.5 7.57 4.43 5000 13.74 1 0.11	7.57 4.43 5000 13.74 1 0.11	4.43 5000 13.74 1 0.11	5000 13.74 1 0.11	13.74 1 0.11	1 0.11	0.11	17	0.0063	0.1217	0.0025	5.72	0.1	0.3417	0.0083	0.5577116	2136	110	1973	37	1931	15	1894	40 9
9.88 78.2 9.56 8.18 50000 28 2.2 0.1 105.1 165.8 100.4 1.65 14000 5.097 0.32 0.1	78.2 9.56 8.18 50000 28 2.2 0.1 (65.8 100.4 1.65 14000 5.097 0.32 0.1	9.56 8.18 50000 28 2.2 0.1 100.4 1.65 14000 5.097 0.32 0.1	8.18 50000 28 2.2 0.1 1.65 14000 5.097 0.32 0.1	50000 28 2.2 0.1 14000 5.097 0.32 0.1	28 2.2 0.1 5.097 0.32 0.1	2.2 0.1 0.32 0.1	0.1 0.1	165 156	0.0063 0.0047	0.1293 0.1254	0.0024 0.002	6.598 6.261	0.081 0.076	0.3718 0.3606	0.0085 0.008	0.585835 0.715121	2224 2210	110 85	2082 2033	33 29	2061 2013	= =	2037 1987	40 9 36 9
294.3 696 239.3 2.91 280000 8.75 0.56 0.1	696 239.3 2.91 280000 8.75 0.56 0.1	239.3 2.91 280000 8.75 0.56 0.1	2.91 280000 8.75 0.56 0.1	280000 8.75 0.56 0.1	8.75 0.56 0.1	0.56 0.1	0.1	358	0.0056	0.159	0.0025	9.01	0.14	0.4113	0.0096	0.7430956	2573	100	2442	26	2337	14	2219	44
52.9 78.8 53.7 1.47 21000 4.693 0.3 0.1 230 1670 756 2.21 64700 11.41 0.74 0.0	78.8 53.7 1.47 21000 4.693 0.3 0.1 1670 756 2.21 64700 11.41 0.74 0.0	53.7 1.47 21000 4.693 0.3 0.1 756 2.21 64700 11.41 0.74 0.0	1.47 21000 4.693 0.3 0.1 2.21 64700 11.41 0.74 0.0	21000 4.693 0.3 0.1 64700 11.41 0.74 0.0	4.693 0.3 0.1 11.41 0.74 0.0	0.3 0.1 0.1 0.74 0.0	0.0	1114 1348	0.0045 0.0021	0.1229 0.106	0.0022 0.0018	6.078 2.464	0.092 0.036	0.3606 0.1674	0.0081 0.0039	0.607704 0.6872764	2134 691	82 41	1993 1730	33 32	1985 1264	13	1984 998	38 5
1209 2890 2197 1.32 161000 3.79 0.27 0.	2890 2197 1.32 161000 3.79 0.27 0.	2197 1.32 161000 3.79 0.27 0.	1.32 161000 3.79 0.27 0.	161000 3.79 0.27 0.	3.79 0.27 0.	0.27 0.	0	0636	0.0034	0.1324	0.0034	3.51	0.12	0.1928	0.008	0.7863809	1246	64	2127	44	1527	28	1136	43 7
151.4 384.9 149.7 2.57 250000 8.2 0.52 0.1	384.9 149.7 2.57 250000 8.2 0.52 0.1	149.7 2.57 250000 8.2 0.52 0.1	2.57 250000 8.2 0.52 0.1	250000 8.2 0.52 0.1	8.2 0.52 0.1	0.52 0.1	0.1	153	0.0046	0.126	0.002	6.209	0.088	0.3588	0.0083	0.7381851	2204	83	2042	27	2008	13	1979	38 9
224.4 326 102.7 2.00 160000 6.39 0.42 0.13 348.2 649 362.1 1.79 150000 4.81 0.32 0.1	326 162./ 2.00 160000 6.39 0.42 0.15 649 362.1 1.79 150000 4.81 0.32 0.1	162./ 2.00 160000 6.39 0.42 0.1. 362.1 1.79 150000 4.81 0.32 0.1	21.00 160000 6.39 0.42 0.12 1.79 150000 4.81 0.32 0.1	160000 6.39 0.42 0.15 150000 4.81 0.32 0.1	6.39 0.42 0.15 4.81 0.32 0.1	0.32 0.1 0.32 0.1	دا.ں 0.1	6/ 12	0.0046 0.0046	0.1178	0.0022	13.22 4.875	0.099	0.3016	0.0081	0.7195702	2962 2145	84	2/64 1920	30 33	2692 1796	17	2621 1698	67 40 9 9
75.8 192.8 75.1 2.57 57000 8.11 0.52 0.1	(92.8 75.1 2.57 57000 8.11 0.52 0.1	75.1 2.57 57000 8.11 0.52 0.1	2.57 57000 8.11 0.52 0.1	57000 8.11 0.52 0.1	8.11 0.52 0.1	0.52 0.1	0.1	15	0.0047	0.1277	0.0021	6.372	0.097	0.3623	0.0085	0.7164184	2200	84	2063	28	2026	13	1992	40 9
326.5 316 241 1.31 220000 4.395 0.28 0.155	316 241 1.31 220000 4.395 0.28 0.155	241 1.31 220000 4.395 0.28 0.155	1.31 220000 4.395 0.28 0.155	220000 4.395 0.28 0.155	4.395 0.28 0.155	0.28 0.155	0.155	6	0.0059	0.1892	0.003	13.51	0.18	0.5186	0.012	0.7485016	2927	100	2734	26	2714	13	2691	52 9
209 939 151.8 6.19 330000 18.7 2.2 0.158	939 151.8 6.19 330000 18.7 2.2 0.158	151.8 6.19 330000 18.7 2.2 0.158	6.19 330000 18.7 2.2 0.158	330000 18.7 2.2 0.158	18.7 2.2 0.158	2.2 0.158	0.158	9	0.0092	0.1875	0.0064	11.66	0.37	0.454	0.018	0.5618699	2970	160	2716	54	2575	30	2411	80 9
340.5 525 373.6 1.41 270000 4.596 0.29 0.10	525 373.6 1.41 270000 4.596 0.29 0.10	373.6 1.41 270000 4.596 0.29 0.10	1.41 270000 4.596 0.29 0.10	270000 4.596 0.29 0.10	4.596 0.29 0.10	0.29 0.10	0.10	5	0.0041	0.1256	0.002	5.867	0.086	0.339	0.0079	0.738265	2017	74	2035	28	1954	13	1881	38 9
224.1 873 171.7 5.08 130000 14.9 0.94 0.15	873 171.7 5.08 130000 14.9 0.94 0.15	171.7 5.08 130000 14.9 0.94 0.15	5.08 130000 14.9 0.94 0.15	130000 14.9 0.94 0.15	14.9 0.94 0.15	0.94 0.15	0.15	21	0.0059	0.1764	0.0029	10.77	0.15	0.4448	0.011	0.7770625	2861	100	2617	27	2502	13	2370	51 9
73.9 256.4 89.8 2.86 107000 9.75 0.63 0.0	256.4 89.8 2.86 107000 9.75 0.63 0.0	89.8 2.86 107000 9.75 0.63 0.0	2.86 107000 9.75 0.63 0.0	107000 9.75 0.63 0.0	9.75 0.63 0.0	0.63 0.0	0.0	941	0.0038	0.1058	0.0019	4.484	0.055	0.3066	0.0064	0.5149119	1817	70	1725	33	1727	10	1724	32 9
438 612 331.8 1.84 600000 5.79 0.38 0.1	612 331.8 1.84 600000 5.79 0.38 0.1	331.8 1.84 600000 5.79 0.38 0.1	1.84 600000 5.79 0.38 0.1	600000 5.79 0.38 0.1	5.79 0.38 0.1	0.38 0.1	0.1	538	0.0061	0.191	0.0035	12.47	0.24	0.477	0.013	0.741033	2892	110	2748	30	2639	18	2512	58 9
360 1560 791 1.97 98000 11.46 0.78 0.	1560 791 1.97 98000 11.46 0.78 0.	791 1.97 98000 11.46 0.78 0.	1.97 98000 11.46 0.78 0.	98000 11.46 0.78 0.	11.46 0.78 0.	0.78 0.	0	0534	0.0031	0.1701	0.0031	6.72	0.12	0.2863	0.0063	0.5992674	1051	60	2557	31	2075	16	1623	31
288.8 180.4 237.2 0.76 120000 2.563 0.16 0.14	180.4 237.2 0.76 120000 2.563 0.16 0.1 ⁴	237.2 0.76 120000 2.563 0.16 0.14	0.76 120000 2.563 0.16 0.14	120000 2.563 0.16 0.14	2.563 0.16 0.14	0.16 0.14	0.14	127	0.0056	0.1689	0.0028	10.89	0.15	0.4677	0.01	0.631661	2696	100	2544	28	2512	13	2473	46 9

		% con	94.5	98.6	76.8	98.2	9.96	99.0	87.9	98.6	9.99	99.2	97.5	92.6	98.5	9.96	97.6	97.4	98.7	98.2	92.5	103.2	99.1	82.5	97.7	9.66	97.5	98.2	98.7	98.3	97.8	96.1	95.4	98.5	71.0	99.1	94.2	94.6	87.9	98.6	98.7
		$\pm 2\sigma^2$	33	46	46	46	46	54	39	34	43	47	49	49	51	47	36	49	45	43	39	75	47	37	39	46	38	48	41	39	41	39	51	35	26	47	43	48	34	46	44
		. ⁰⁶ Pb/ ²³⁸ U	1773	1983	1659	2766	1827	2674	1670	1589	2484	2644	2373	1810	2667	2696	1726	2626	2438	2410	1718	2734	2636	1520	1981	2473	1945	2419	2415	2022	1962	1852	2074	1922	1277	2722	2262	2362	1540	2805	2696
	(Ma)	$\pm 2\sigma^2$	7.5	17	19	9.6	15	13	20	13	9.1	12	18	18	14	20	12	13	12	11	16	30	11	17	12	12	9.5	15	10	11	14	13	20	10	12	12	12	13	13	8.5	10
	d ages	⁰⁷ Pb/ ²³⁵ U	1876.1	2012	2159	2816.2	1892	2701	1899	1611	2485.9	2665	2433	1954	2708	2790	1769	2695	2470	2453	1857	2650	2660	1843	2028	2483	1995.7	2463	2447	2058	2006	1927	2174	1952	1799	2746	2401	2496	1752	2843.7	2732
	alculate	$\pm 2\sigma^2$	28	38	31	26	43	28	29	27	26	29	35	36	25	39	28	26	27	27	28	39	24	29	25	27	28	25	26	29	28	28	31	29	25	27	25	26	30	25	25
	C	³⁷ Pb/ ² ⁰⁶ Pb	1990	2043	2692	2844	1981	2723	2170	1642	2488	2689	2493	2111	2741	2857	1821	2747	2494	2484	2015	2578	2679	2235	2077	2491	2041	2501	2470	2092	2047	2008	2278	1982	2464	2762	2516	2601	2018	2864	2756
		$\pm 2\sigma^2$	78	84	74	100	350	100	46	67	93	110	120	220	100	230	71	110	92	92	83	150	66	76	76	93	76	89	89	78	80	78	100	76	53	110	89	94	74	100	100
		³⁸ Pb/ ² ³² Th	2130	2187	1612	2851	1780	2948	854	1755	2648	2831	2666	1090	2925	3540	1932	2765	2623	2601	1963	3070	2804	1852	2106	2625	2114	2580	2552	2170	2160	2137	2407	2044	1302	2823	2550	2673	1895	2964	2866
		10 ³	93947	76334	18797	22731	42916	67916	87113	76565	12136	90366	87581	50757	98247	38071	57454	61262	43735	80024	50302	26742	70248	73831	01477	64214	01385	93812	69238	73681	44021	64561	97089	60043	94981	10723	64453	48181	30338	25231	27318
		RI	8 0.78	6 0.60	2 0.8	1 0.62	5 0.57	3 0.75	9 0.79	7 0.79	8 0.71	1 0.52	1 0.51	1 0.74	2 0.76	1 0.33	3 0.78	1 0.69	1 0.69	7 0.67	9 0.81	8 0.75	1 0.7	2 0.79	1 0.77	1 0.67	8 0.73	1 0.75	3 0.6	2 0.65	5 0.75	8 0.78	1 0.78	4 0.64	9 0.75	1 0.6	5 0.7	1 0.82	6 0.7	1 0.71	1 0.58
		$\pm 2\sigma^2$	0.006	0.00	0.00	0.01	0.00	0.01	0.007	0.006	0.009	0.01	0.01	0.0	0.01	0.01	0.007	0.01	0.0	0.00	0.007	0.01	0.01	0.007	0.008	0.0	0.007	0.01	0.00	0.008	0.008	0.00	0.01	0.007	0.004	0.01	0.00	0.01	0.006	0.01	0.0
		²⁰⁶ Pb/ ²³⁸ U	0.3166	0.3604	0.2937	0.536	0.3281	0.5144	0.2959	0.2797	0.4702	0.5073	0.4454	0.3246	0.5129	0.5193	0.3072	0.5033	0.46	0.4536	0.3057	0.529	0.5056	0.266	0.3599	0.468	0.3518	0.4558	0.4545	0.3686	0.356	0.3331	0.3799	0.3475	0.2191	0.5249	0.4206	0.443	0.27	0.5453	0.5194
		±2\sigma²	0.047	0.12	0.16	0.15	0.097	0.2	0.13	0.061	0.11	0.16	0.19	0.13	0.2	0.31	0.069	0.19	0.13	0.12	0.094	0.4	0.15	0.11	0.088	0.13	0.07	0.17	0.11	0.08	0.099	0.085	0.15	0.068	0.067	0.17	0.13	0.15	0.071	0.14	0.15
		⁰⁷ Pb/ ²³⁵ U	5.349	6.27	7.4	15.02	5.456	13.28	5.51	3.894	10.56	12.82	10.02	5.87	13.43	14.65	4.721	13.25	10.38	10.18	5.243	12.66	12.75	5.13	6.38	10.56	6.135	10.34	10.15	6.597	6.214	5.685	7.5	5.846	4.878	13.97	9.66	10.7	4.619	15.47	13.76
	atios	±2σ ²	0.0019	0.0027	0.0034	0.0033	0.0029	0.0032	0.0022	0.0015	0.0025	0.0034	0.0036	0.0027	0.0029	0.005	0.0017	0.003	0.0026	0.0026	0.0019	0.004	0.0027	0.0023	0.0019	0.0026	0.002	0.0026	0.0025	0.0022	0.002	0.0019	0.0026	0.002	0.0024	0.0032	0.0025	0.0027	0.0021	0.0031	0.003
	sotopic r:	⁷ Pb/ ³⁶ Pb	.1225	.1264	.1845	.2024	0.1222	.1881	0.1356	0.101	.1634	0.1845	0.1637	.1313	.1901	0.2046	11149	.1909	0.164	0.163	.1242	0.1725	.1831	.1408	.1285	0.1637	0.1259	0.1644	.1616	0.1298	.1265	0.1238	.1445	0.122	0.161	0.1927	.1661	.1747	0.1244	0.205	.1917
	Ι	2σ ² 2	.0043 (.0047 (0.004 (.0058 (0.02 (0.006 (0.0024 (0036	0052 (0.006 (.0065 (0.012 (.0058 (0.014 (.0039 0.	0.0062 (.0052	.0052	.0045 () 6800.	.0056 (0.0042 (0.0042 (0052 (.0041 (0.005 (0.005 (.0043 (.0044 (.0043 (.0058 (.0042	.0028	.0062 (0.005 (.0053 (0.004 (.0059	.0058 (
		Pb/ Th ±	1111 0	1143 0	0.083	1515 0	0.095	1571	0432 0	0 2060	0.14 0	1504	1412 0	0.056	1558 0	0.192	1003 0	1467 0	1386 0	1374 0	1021 0	1644 0	1489 0	0 960.0	1098 0	1387 0	1103 0	1362	1346	1134 0	1128 0	1115 0	1266 0	1065 0	0666 0	0.15 0	1345	1414 0	0983	0.158 0	1524 0
		σ ² ²⁰⁸] σ ² 232	.72 0.	.29 0.	.47 (.36 0.	42 (.15 0.	0.7 0.	.78 0.	.13	.21 0.	.36 0.	1	.32 0.	0.5 (.66 0.	.15 0.	.23 0.	.26 0.	3 0.	.32 0.	.39 0.	.63	0.5 0.	.34 0.	.34 0.	.27 0.	.25 0.	0.2 0.	0.9 0.	.41 0.	.34 0.	.46 0.	.36 0.	.49	.37 0.	1 0.	0.5 0.	.32 (.31 0.
		Pb/ Pb ±2,	1.43 0	399 0	7.11 0	5.72 0	215	321 0	9.68	2.24 0	.135 0	267 0	5.17 0	0.71	.118 0	5.86	0.47 0	362 0	614 0	3.89 0	24	4.44 0	.133 0	9.35 0	7.9	5.36 0	284 0	346 0	3.15 0	209	4.21	6.08 0	5.08 0	7.15 0	739 0	7.43 0	956 0	6.23	7.4	.155 0	955 0
		208	0 1	000 4	000	000	000	000 2	500	000 1	000 2	000 3	000	000	000 5	000	000	000 2	000 3	000	000	000	9 000	000	000	000	000 5	000 4	000	000 3	000	000	000	000	500 5	000	000 5	000	000	000 5	000 4
		²⁰⁶ Pb/ ²⁰⁴ Pb		26(32(200(18(500(642	7000	30(42(15(42(9	84(1100	120(11(57(270(52(77(106(180(200(150(1700	260(909	1100	120(240(32(800	25(600	510(203(100(20(
	1S ¹	J/Th	3.94	1.38	2.08	1.54	29.16	0.70	1.40	3.95	0.62	0.95	1.59	0.78	1.54	2.01	3.40	0.66	1.06	1.12	6.80	1.29	1.75	3.44	2.36	1.54	1.58	1.29	0.81	0.96	4.43	1.97	1.65	2.16	1.72	2.04	1.87	5.09	2.58	1.48	1.45
	ntration	Th I pm)	442.2	118.1	247	154	1.9	325.8	365	104.6	268	90.6	24.86	520	192	188.5	176.6	299.4	128	134.8	79.6	27.2	92.1	137	153.1	139.9	196	326	313	214.6	99.8	255	181	69.69	666	34.8	429.7	174.6	241	152.5	74.2
	ed conce	U (Id (J	1743	163.2	513	237.4	55.4	229.4	510	413	166.4	86.4	39.5	404	295	378	601	1.661	135.4	151.3	541	35.2	161.4	471	361	215.1	310	419	254.4	207	442	503	299.1	150	1720	71	805	889	621	225.3	107.5
ıed.	Measure	Pb (mq	422	114	172	202.8 2	1.15	432.6 2	132.9	80.6	319	115.6	29.5	100.4	254.7	312	150.7	371	148.5	155.2	68.9	37.1	114.6	110.2	141.7	162.6	180.2	374	353	206	94.7	237.8	8.061	62.3	569	44	492.3	210	197	210.1	98.3
. Continu		rsis fier (p	a_024	a_025	a_026	a_027 2	a_028	a_029 4	a_030]	a_031	a_032	a_033]	a_034	a_035]	a_036 2	a_037	a_038]	a_039	a_040]	a_041 1	a_042	a_043	a_044]	a_045]	a_046]	a_047]	a_048]	a_049	a_050	a_051	a_052	a_053 2	a_054]	a_055	a_056	a_057	a_058 4	a_059	a_060	a_061 2	a_062
TableA2		Analy Identi	GM10-01	GM10-01	GM10-018	GM10-01	GM10-01	GM10-01	GM10-018	GM10-01	GM10-018	GM10-01																													

TableA2. Conti	nued.																							
	Measu	ured con	centratic	ons ¹						Isotopic 1	atios								Calcu	lated age	es (Ma)			
Analysis Identifier	Pb (mqq)	U (mqq	Th (ppm)	U/Th	²⁰⁶ Pb/ ²⁰⁴ Pb	²⁰⁸ Pb/ ²⁰⁶ Pb	$\pm 2\sigma^2$	²⁰⁸ Pb/ ²³² Th	±2\sigma²	²⁰⁷ Pb/ ²⁰⁶ Pb	$\pm 2\sigma^2$	⁰⁷ Pb/ ¹	20 ²	⁰⁶ Pb/ ²³⁸ U	±2\sigma ² Rŀ	10 ³ 3	³ Pb/ ² ±2 ² Th ±2	$\sigma^2 \frac{^{207}P}{^{06}H}$	b/² ¹b ±2ơ	2 ²⁰⁷ Pb/ 2 ³⁵ U	$\pm 2\sigma^2$	²⁰⁶ Pb/ ²³⁸ U	$\pm 2\sigma^2$	%
GM10-01a_063	63.9	73.2	49.4	1.48	46000	4.612	0.29	0.1478	0.0058	0.1729	0.0028	11	0.15	0.4612	0.01 0.6	65989	2786 1	00 2	583 27	7 252	l 12	2444	44	96.9
GM10-01a_064	156.7	199.1	111.6	1.78	110000	5.92	0.37	0.1597	0.0059	0.2145	0.0034	15.85	0.19	0.5363	0.011 0.63	68074	2999 1	10 2	937 25	5 286	5 11	2767	47	96.5
GM10-01a_065	225	71	169	0.42	58000	1.506	0.095	0.1504	0.0064	0.255	0.0069	18.29	0.51	0.523	0.016 0.57	51464	2832 1	10 3	212 42	300	3 27	2709	70	90.2
GM10-01a_066	289.9	373	243.1	1.53	290000	5.032	0.32	0.135	0.005	0.1615	0.0024	9.95	0.12	0.4484	0.0099 0.77	37748	2559	88 2	469 25	5 2433	11	2387	44	98.1
GM10-01a_067	150.3	165.5	127.9	1.29	45000	4.299	0.27	0.1329	0.005	0.1601	0.0025	10.03	0.14	0.4534	0.0098 0.69	30432	2522	88 2	454 27	7 2430	5 13	2409	44	98.9
GM10-01a_068	459	491	464	1.06	170000	3.058	0.21	0.1138	0.005	0.1268	0.0023	5.93	0.15	0.3391	0.011 0.3	83061	2177	90 2	051 32	196	22	1881	52	95.9
GM10-01a_069	4.65	142.4	4.61	30.89	55000	94.7	7.6	0.1142	0.0073	0.1189	0.0019	5.518	0.062	0.3352	0.0069 0.630	69154	2180 1	30 1	936 29	1902.	3 9.7	1863	33	97.9
GM10-01a_070	157.6	283.2	157	1.80	60000	5.801	0.36	0.1125	0.0043	0.1276	0.0019	6.412	0.069	0.3634	0.0075 0.720	04787	2154	78 21	062 27	2034.	6	1998	35	98.2
GM10-01a_071	188	221.3	192.6	1.15	100000	3.653	0.23	0.1104	0.0045	0.1275	0.0021	6.29	0.086	0.3575	0.0088 0.77	48748	2116	81 2	061 29	2016	5 12	1969	42	97.7
GM10-01a_072	179.3	153	145.5	1.05	53000	3.44	0.22	0.1354	0.005	0.1632	0.0025	10.28	0.12	0.4569	0.0096 0.69	93843	2567	90 2	487 26	5 2459	11 (2425	43	98.6
GM10-01a_073	210.4	207.1	176.7	1.17	138000	3.561	0.23	0.1297	0.005	0.1686	0.0028	9.28	0.17	0.4002	0.011 0.80	95755	2463	89 2	541 28	3 236	± 16	2168	50	91.2
GM10-01a_074	137.3	234.5	137.7	1.70	140000	5.44	0.35	0.1093	0.0041	0.1241	0.0019	6.252	0.076	0.3658	0.0077 0.69	65287	2096	75 21	013 27	7 201	11	2009	36	9.66
GM10-01a_075	109.8	115.7	108.5	1.07	50000	3.409	0.23	0.1101	0.0042	0.1264	0.0021	6.249	0.073	0.3582	0.0073 0.57	91819	2110	76 21	045 29	2010) 10	1973	35	98.2
GM10-01a_076	88.2	204	86.1	2.37	190000	7.31	0.46	0.1112	0.0043	0.1279	0.002	6.421	0.064	0.3625	0.0076 0.70	43548	2131	77 2	066 28	3 2034.2	2 8.7	1993	36	98.0
GM10-01a_077	77.5	523	95.61	5.47	180000	16.02	1	0.0878	0.0035 (0.10177	0.0015	3.781	0.046	0.2699	0.0058 0.750	07736	1700	64 1	654 27	7 158	7 10	1540	30	97.0
GM10-01a_078	105.3	312	113	2.76	57900	7.04	0.49	0.1007	0.005	0.1895	0.0031	6.85	0.13	0.2594	0.0063 0.74	40269	1939	91 2	737 27	209	l 17	1487	32	71.1
GM10-01a_079	53.7	62.6	50.1	1.25	13000	3.919	0.25	0.1155	0.0045	0.129	0.0022	6.766	0.093	0.3802	0.0084 0.63	58823	2208	82 21	080 3(207) 12	2076	39	6.66
GM10-01a_080	237.8	299.1	178.2	1.68	260000	5.808	0.37	0.1412	0.0052	0.1861	0.0029	12.94	0.15	0.5018	0.011 0.73	21227	2670	93 2	706 26	5 267	11	2621	45	98.0
GM10-01a_081	255	346	255	1.36	210000	4.129	0.27	0.107	0.004	0.1237	0.0019	5.869	0.091	0.3438	0.0082 0.77	52016	2055	73 20	007 27	7 1950	5 13	1904	40	97.3
GM10-01a_082	150.9	331	114.9	2.88	50000	9.04	0.62	0.1393	0.0052	0.1639	0.0025	10.27	0.13	0.4551	0.0098 0.71	77226	2636	91 2.	494 26	5 2458	3 12	2417	44	98.3
GM10-01a_083	153.7	159.5	135.5	1.18	105000	3.679	0.24	0.1199	0.0057	0.1646	0.0028	9.13	0.2	0.4029	0.011 0.783	24245	2298	99 2	503 31	234	7 21	2180	53	92.9
GM10-01a_084	86.2	141.1	92.6	1.52	147000	4.3	0.29	0.1004	0.005	0.1355	0.0031	5.69	0.14	0.3064	0.011 0.77	59547	1931	93 2	164 41	192	5 21	1721	52	89.4
GM10-01a_085	152.8	111.2	98	1.13	200000	3.64	0.25	0.1663	0.0066	0.2214	0.0036	17.17	0.24	0.5633	0.013 0.718	85624	3108 1	10 2	989 27	7 294	5 13	2879	53	97.8
GM10-01a_086	202	468	633	0.74	82000	3.98	0.27	0.0351	0.0026	0.144	0.0034	4.13	0.11	0.2055	0.0077 0.7	79513	698	50 2	272 41	165	9 21	1204	41	72.6
GM10-01a_087	43.2	48.5	29.39	1.65	44000	5.17	0.33	0.1538	0.0063	0.1949	0.0034	14.02	0.18	0.521	0.011 0.56	49514	2890 1	10 2	780 29	274	9 12	2702	45	98.3
GM10-01a_088	27.8	44	17.6	2.50	25000	8.8	0.69	0.1707	0.0078	0.2284	0.0039	18.79	0.23	0.5963	0.013 0.65	24965	3180 1	40 3	037 28	302	9 12	3013	52	99.5
GM10-01a_089	148	194.3	91.8	2.12	300000	6.8	0.43	0.1679	0.0063	0.2219	0.0033	17.87	0.18	0.5811	0.012 0.73	73293	3135 1	10 2	992 24	1 2981.4	1 9.7	2952	51	0.66
GM10-01a_090	128	136.3	129.9	1.05	50000	2.128	0.16	0.1061	0.0058	0.1425	0.0054	4.94	0.25	0.251	0.017 0.83	32857	2038 1	10 2	253 67	7 180	5 43	1442	86	79.8
GM10-01a_091	60.7	232	58.2	3.99	800000	11.94	0.77	0.1079	0.0043	0.1227	0.002	5.91	0.064	0.3489	0.0074 0.650	61861	2070	79	995 28	3 1961.6	5 9.5	1929	36	98.3
GM10-01a_092	66.2	158.9	290	0.55	46000	6.24	0.44	0.02309	0.0012	0.2239	0.0036	8.78	0.17	0.2829	0.0077 0.81	32775	461	24 3	007 26	5 231	3 17	1605	39	69.4
GM10-01a_093	551	325	350	0.93	220000	2.721	0.18	0.1615	0.006	0.2032	0.0032	14.84	0.21	0.5301	0.012 0.72	53165	3026 1	00	849 26	5 280	3 14	2740	50	97.8
GM10-01a_094	172.4	484	165	2.93	160000	7.45	0.53	0.1111	0.0052	0.1256	0.0024	5.56	0.16	0.3222	0.011 0.82	88158	2128	95 21	035 35	1908	8 24	1799	54	94.3
GM10-01a_095	239.1	367	227.5	1.61	200000	4.23	0.27	0.1085	0.0042	0.1177	0.0019	5.148	0.086	0.3167	0.0075 0.73	21634	2081	76 1	923 27	7 184	l 14	1772	37	96.3
GM10-01a_096	190.2	201.6	123	1.64	34600	2.746	0.18	0.1614	0.0065	0.1724	0.0041	7.25	0.12	0.3058	0.0087 0.549	97831	3023 1	10 2	573 4(214	l 15	1719	43	80.3
GM10-01a_097	94.7	240.9	85.4	2.82	70000	8.25	0.57	0.112	0.0044	0.1282	0.002	6.429	0.081	0.3622	0.0076 0.67	26277	2144	80 2	071 28	3 203!	11	1992	36	97.9
GM10-01a_098	127.8	97.7	94.1	1.04	40000	3.058	0.2	0.1405	0.0055	0.1631	0.0028	10.34	0.12	0.4601	0.0099 0.600	65941	2656	97 2.	484 29) 246	± 10	2439	44	0.66
GM10-01a_099	121	204.6	112	1.83	100000	5.305	0.34	0.1123	0.0043	0.1245	0.002	6.165	0.073	0.3579	0.0083 0.76	46745	2150	78 2	018 28	8661 8	3 10	1975	38	98.8
GM10-01a_100	206.1	418.8	192.1	2.18	150000	6.255	0.4	0.1112	0.0043	0.1274	0.0019	6.19	0.1	0.3506	0.0085 0.79	95945	2131	79 20	062 26	5 200	3 14	1936	40	96.7
GM10-01a_101	54.2	206.5	48.1	4.29	000006	12.44	0.8	0.1166	0.0048	0.1284	0.0021	6.595	0.077	0.3735	0.008 0.65	49978	2228	87 21	073 29) 205	7 10	2045	38	99.4

		% con	98.4	94.0	97.6	70.8	98.7	99.4	92.1	99.3	98.9	99.7	98.3	98.2	98.2	85.6	96.0	98.9	93.1	99.4	98.4	98.9	94.6	79.0	98.3	98.5	99.2	98.0	97.6	97.0	96.4	98.4	97.2	98.4	98.7	98.5	98.1	97.2	98.3	97.6	99.4
		±2σ ²	45	74	38	47	57	38	34	38	37	40	44	36	47	31	44	40	42	53	52	38	34	34	51	30	36	45	29	52	44	41	37	37	50	36	38	37	46	44	43
		.06Pb/ ²³⁸ U	2586	2947	2015	1157	1937	2014	1818	2012	1987	2005	2039	1976	2728	1379	1803	2124	2406	2968	2792	1955	1833	1712	3160	1630	2013	2549	1602	2752	2355	2414	1968	1960	2871	2016	1950	1996	2673	2390	2477
	(Ma)	$\frac{2}{\pm 2\sigma^2}$	13	27	11	32	24	10	11	9.5	10	13	21	9.3	6	11	16	12	9.6	13	12	16	10	12	10	10	9.1	11	10	12	13	8.8	11	11	10	11	14	12	9.2	13	11
	d ages	⁷⁷ Pb/ ²³⁵ U	2628	3134	2065	1634	1962	2026	1975	025.2	2010	2011	2074	013.1	777.8	1611	1879	2147	585.2	2986	2836	1976	1942	2168	3215	1655	029.6	2602	1641	2838	2442	2454	2024	1992	2908	2047	1987	2054	2718.3	2447	2493
	alculate	20 $\pm 2\sigma^2$	28	32	30	31	35	30	32	30 2	29	30	46	29 2	25 2	31	31	30	24 2	26	25	42	29	27	24	34	29 2	26	28	25	25	25	27	28	24	27	34	31	24 2	25	24
	Ö	⁰⁷ Pb/ ² ⁰⁶ Pb [:]	2653	3250	2108	2321	1997	2039	2131	2034	2027	2014	2110	2046	2807	1938	1968	2164	2721	2995	2854	1990	2051	2622	3245	1677	2035	2633	1688	2891	2515	2481	2070	2011	2923	2076	2027	2107	2747	2490	2500
		$\pm 2\sigma^2$	110	170	86	54	95	85	42	80	78	84	100	82	100	71	78	83	66	110	100	89	78	61	120	63	78	100	62	120	93	90	76	75	110	76	80	80	100	88	91
		8 Pb/ ² 32 Th	2740	3120	2150	890	2278	2209	836	2159	2133	2199	2230	2138	2906	1483	2127	2277	2842	3223	2984	2082	1946	1330	3346	1693	2144	2668	1732	2913	2593	2565	2129	2141	3031	2145	2130	2153	2840	2533	2564
		Rho ³	462084	8063663	6414089	002763	8045905	534558	613551	6080823	5773058	022834	039067	600301	.702492	564809	844372	5245996	212499	.731954	.741586	363348	657343	226611	920297	.548394	6041612	5516384	.661816	352489	'383447	'345321	.706767	7413643	7495719	656247	5238763	816015	8144673	577553	338032
		2	.0 IO.	18 0.8	0.6 0.6	88 0.5	0.5	0.6 0.6	0.5	0.6 0.6	0.6	86 0.7	93 0.4	0.6	0 110	59 0.7	89 0.7	85 0.6	94 0.7	013 0	012 0	0.3	9.0 69	0.7	0.6	006 0	0.6 0.6	.01 0.6	58 0	0.7	0.2	92 0.7	0 820	0.0 0.7	0.7	0.6 0.6	9.0 0.6	0.5	3.0 110	2.0 66	20 26
		±20	0	0.0	0.0	0.00	0.0	0.0	0.00	0.0	0.00	0.00	0.00	0.00	0.0	0.00	0.00	0.00	0.00	0.0	0.0	0.00	0.00	0.00	0.0	0.0	0.00	0	0.00	0.0	0.00	0.00	0.00	0.0	0.0	0.00	0.00	0.00	0.0	0.00	0.00
		²⁰⁶ Pb/ ²³⁸ U	0.4937	0.58	0.3672	0.197	0.351	0.3668	0.326	0.3664	0.3611	0.365	0.3724	0.3583	0.5272	0.2386	0.323	0.3904	0.4526	0.5851	0.5426	0.3544	0.3291	0.3042	0.633	0.2878	0.3666	0.4852	0.2822	0.533	0.4412	0.4545	0.3572	0.3548	0.5613	0.3672	0.3533	0.363	0.5141	0.4491	0.4687
		$\pm 2\sigma^2$	0.17	0.61	0.082	0.15	0.16	0.075	0.08	0.069	0.071	0.091	0.16	0.066	0.14	0.055	0.1	0.093	0.13	0.25	0.2	0.11	0.068	0.095	0.23	0.052	0.064	0.14	0.05	0.19	0.15	0.097	0.084	0.087	0.18	0.078	0.099	0.093	0.13	0.14	0.12
		²⁰⁷ Pb/ ²³⁵ U	12.33	20.84	6.643	4	5.93	6.365	5.994	6.357	6.248	6.264	6.75	6.269	14.44	3.892	5.38	7.295	11.75	17.93	15.33	6.02	5.78	7.469	22.72	4.111	6.378	11.98	4.038	15.38	10.1	10.221	6.336	6.081	16.55	6.52	6.086	6.574	13.56	10.16	10.66
	ratios	$\pm 2\sigma^2$	0.0031	0.0049	0.0022	0.0029	0.0025	0.0021	0.0024	0.0022	0.002	0.0021	0.0035	0.002	0.0031	0.002	0.0021	0.0023	0.0028	0.0034	0.0031	0.0029	0.002	0.0028	0.004	0.0018	0.0021	0.0028	0.0016	0.0033	0.0025	0.0024	0.002	0.0019	0.0032	0.002	0.0022	0.0023	0.0028	0.0024	0.0024
	Isotopic	²⁰⁷ Pb/ ²⁰⁶ Pb	0.1804	0.2601	0.131	0.1477	0.1231	0.1258	0.1329	0.1257	0.1251	0.1243	0.1316	0.1264	0.198	0.119	0.121	0.1351	0.1878	0.222	0.2038	0.1229	0.1266	0.1769	0.2601	0.103	0.1257	0.178	0.10352	0.2085	0.166	0.1627	0.1282	0.124	0.2125	0.1286	0.1248	0.131	0.1907	0.1635	0.1644
		$\pm 2\sigma^2$	0.0063	0.0097	0.0047	0.0028	0.0053	0.0047	0.0022	0.0044	0.0043	0.0046	0.0058	0.0045	0.0059	0.0038	0.0043	0.0046	0.0056	0.0064	0.0059	0.0049	0.0043	0.0032	0.007	0.0034	0.0043	0.0057	0.0034 (0.0066	0.0052	0.0051	0.0042	0.0042	0.0061	0.0042	0.0044	0.0044	0.0057	0.0049	0.0051
		⁰⁸ Pb/ ³² Th	0.1454	0.167	0.1123	0.0451	0.1194	0.1155	0.0422	0.1128	0.1113	0.115	0.1168	0.1116	0.1547	0.0762	0.111	0.1193	0.151	0.1729	0.1591	0.1085	0.1011	0.0681	0.1801	0.0874	0.1119	0.1412	0.0895	0.1552	0.137	0.1353	0.1111	0.1117	0.1618	0.112	0.1112	0.1125	0.1509	0.1335	0.1353
		$\frac{2}{12\sigma^2}$	0.63	0.51	0.33	0.39	0.58	0.43	0.67	0.24	0.26	0.36	0.4	0.66	0.36	0.53	0.63	0.31	0.44	0.16	0.31	0.24	0.57	69.0	0.43	0.25	0.4	0.52	0.21	0.26	0.21	0.21	0.63	0.44	69.0	0.43	0.22	0.32	0.26	0.4	0.65
		⁸ Pb/	9.45	7.32	4.54	5.37	7.53	6.74	10.3	3.827	4.094	5.41	5.75	10.21	5.04	8.14	9.91	4.868	7.012	2.465	4.85	3.588	8.94	10.42	6.66	3.925	6.21	8.11	3.353	4.131	3.415	3.378	7.56	7.02	10.94	6.74	3.316	4.918	3.965	6.336	16.6
		⁶ Pb/ ²⁰ ³⁴ Pb ²⁰	38000	110000	55000	54200	000006	100000	68000	800000	300000	700000	80000	000006	150000	301000	320000	000006	2000000	410000	130000	20000	240000	207000	100000	110000	000006	190000	150000	100000	210000	300000	350000	590000	350000	700000	320000	200000	140000	400000	400000
		h 20	3	T	0	9	5	3	4	8	8	0	0	5	T	0	3	9	ŝ	5	ę	0	4		9	8	8	5	5	4	5	6	3	9	6	1	3	ŝ	0	9	
	ttions ¹	U/T (74 3.0	.3 2.3	6 1.4	70 1.3	.4 2.8	.2 2.3	58 1.4	.4 1.2	.2 1.3	.4 1.8	12 1.9	.4 3.3	.4 1.6	15 2.7	.1 3.6	.7 1.5	90 2.4	24 0.7	.2 1.4	15 1.1	.8 2.7	58 2.2	.4 1.8	.3 1.1	87 1.8	.1 2.2	04 1.0	.8 1.1	32 1.0	33 0.9	.8 2.2	.6 2.1	.2 2.9	5 2.0	.8 1.0	.3 1.4	98 1.1	21 1.8	.1 2.8
	ncentra	Th (ppm	18.	104	56	5	107	74	74.	137	156	64	10.	59	116	9	220	72	4		189	40.	113	2	54	131		150	3(222	3	=	164	163	113	174	208	. 50	51		188
	ured co	U U	56.8	240.6	79.2	366	306	172.9	107.4	176.5	215	170	19.2	199	187	1659	799	113.5	1193	248	277	44	312	371	101.4	155	163.2	337.1	318	261.2	349	181.3	368	354	339	350	215.3	74.4	218	596	528
inued.	Meas	(mqq) dq	26.01	157.9	59.5	111.5	117.8	80.2	29.2	144.3	160.7	98.4	10.62	59.5	159.8	398.8	212.8	75.6	643	492	258.4	37.6	94.1	92.5	79.2	92.1	78.1	172.6	216.8	275.2	363	196.4	143.8	143.8	146.3	154	180.5	44.7	234	334	200.6
TableA2. Cont		Analysis Identifier	GM10-01a_102	GM10-01a_103	GM10-01a_104	GM10-01a_105	GM10-01a_106	GM10-01a_107	GM10-01a_108	GM10-01a_109	GM10-01a_110	GM10-01a_111	GM10-01a_112	GM10-01a_113	GM10-01a_114	GM10-01a_115	GM10-01a_116	GM10-01a_117	GM10-01a_118	GM10-01a_119	GM10-01a_120	GM10-01a_121	GM10-01a_122	GM10-01a_123	GM10-01a_124	GM10-01a_125	GM10-01a_126	GM10-01a_127	GM10-01a_128	GM10-01a_129	GM10-01a_130	GM10-01a_131	GM10-01a_132	GM10-01a_133	GM10-01a_134	GM10-01a_135	GM10-01a_136	GM10-01a_137	GM10-01a_138	GM10-01a_139	GM10-01a_140

d. Aessured concentrations ¹
b U Th $_{206}^{206}$ Pb/ $_{208}^{208}$ Pb/ $_{208}^{208}$ Pb/ $_{\pm 2\sigma^2}^{208}$ Pb/ $_{\pm 2\sigma^2}^{208}$ Pb/ $_{\pm 2\sigma^2}^{2}$
0.3 493 75 6.57 870000 19.93 1.3 0.1031 0.0042
(92 678 217 3.12 2300000 10.36 0.7 0.1103 0.0044
7.1 550 181.5 3.03 680000 21.87 1.5 0.0625 0.0042
335 807 269.9 2.99 1500000 9.62 0.6 0.1573 0.006
9.9 198.4 146 1.36 610000 4.574 0.29 0.1384 0.00
8.5 204.3 66.7 3.06 50000 10.15 0.65 0.1107 0.00
.85 83.5 4.22 19.79 270000 67.6 6 0.1144 0.00
725 794 879 0.90 1000000 2.894 0.18 0.1044 0.00
3.3 31.1 37.2 0.84 500000 2.888 0.2 0.1469 0.0
.32 398 285 1.40 600000 4.768 0.3 0.1018 0.00 ²
243 478 272 1.76 8000000 5.571 0.35 0.1121 0.002
326 463 236 1.96 2000000 6.92 0.46 0.1752 0.006
158 370 182.1 2.03 9000000 6.65 0.43 0.1091 0.004
4.1 142.2 102.6 1.39 240000 4.557 0.29 0.1156 0.00
4.9 456 162.2 2.81 3000000 8.81 0.56 0.1121 0.004
8.4 184.8 139.6 1.32 70000 4.58 0.32 0.108 0.004
358 785 821 0.96 8100000 3.117 0.2 0.1319 0.00
312 327 287 1.14 2100000 3.87 0.25 0.1363 0.00
3.1 325.1 168.2 1.93 10000000 6.684 0.42 0.1356 0.00
723 2140 633 3.38 10000000 10.25 0.65 0.1433 0.00
596 933 566 1.65 27000000 4.79 0.31 0.1548 0.00
9.5 299 67.5 4.43 30000000 14.18 0.92 0.1462 0
178 174 202 0.86 4100000 3.15 0.22 0.1139 0
560 928 563 1.65 30000000 5.55 0.36 0.1446 0
.98 37.9 19.45 1.95 800000 6.99 0.48 0.1637 0
9.2 259.5 129.8 2.00 8000000 6.86 0.46 0.1228 0
6.9 135.1 70 1.93 1200000 6.63 0.43 0.1175 0
159 243.1 186 1.31 3000000 4.572 0.29 0.1045 0.20
5.7 112.6 61.4 1.83 370000 6.57 0.43 0.1493 0.0
3.2 463.5 151.2 3.07 1300000 10.05 0.64 0.0902 0.0
64 51 1.02 500000 3.33 0.23 0.1536 0.00
2.3 249.3 224.2 1.11 7000000 3.845 0.24 0.1346 0.00
360 284 194.1 1.46 30000 5.329 0.34 0.1605 0.00
1.8 87.4 55.7 1.57 600000 5.26 0.34 0.1114 0.00
1.8 751 588 1.28 468000 5.4 0.35 0.0567 0.0
545 618 479 1.29 200000 4.54 0.36 0.1384 0
9.3 167.5 78.6 2.13 200000 7.18 0.46 0.1051 0.0
2.6 141.9 76.2 1.86 200000 6.19 0.4 0.1135 0.0
356 1140 1061 1.07 1800000 3.78 0.24 0.0976 0.0

| entrations ¹ | | | | | | | Isotopic r
 | atios | | | |
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 | Cal | culated | ages (M
 | Ia) | |
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Th ppm) U/Tl	Th 204	Pb/ ²⁰ ¹ Pb ²⁰
 | ²⁰⁷ Pb/
²³⁵ U | ±2σ ² | ²⁰⁶ pb/
²³⁸ U | ±2σ ²
 | Rho ³ | ²⁰⁸ Pb/ ²
³² Th [±] | 20^{20}
 | ⁷ Pb/ ² ±2
⁶ Pb | 2σ ² 23 | Pb/
⁵ U ^{±20}
 | $\sigma^2 \frac{^{206}F}{^{238}}$ | ъ), ±2с
U | 3 ² %
 | <u>,</u> с | |
| 216 1.5 | 51 81 | 000000 | 5.328 | 0.34 (| 0.1554 0 | 0.0058 | 0.2088
 | 0.0031 | 16.34 | 0.15 | 0.5653 | 0.011
 | 0.6787407 | 2919 | 100
 | 2894 | 24 28 | 96.2 9
 | 9.1 2 | 888 | 46 99
 | 9.7 | |
| 65.5 2.2
7667 1.7 | 25 | 700000 | 7.58 | 0.49 | 0.107 (| 0.0042 | 0.1273
 | 0.0022 | 6.469
6 2 16 | 0.071 | 0.3667 | 0.0075
 | 0.5348087 | 2055 | 70
 | 2056 | 30 20 | 40.5 5
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Table A3.

			Measu	ired co:	ncentr	ations						Isc	topic ra	tios				Calcu	llated ag	es (Ma)		I	
Sample	⁹⁰ Zr (cps)	U (ppm)	Th (ppm)	Th/U	²⁰⁴ Pb (cps)	±2σ	% error	$^{206}{\rm Pb/}$	%Pb ³	C4 7	$^{7}\mathrm{Pb/}_{35}$ $^{\pm 2\sigma}$	²⁰⁶ Pb/ ²³⁸ U	±2σ	β	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	² ±2σ	⁰⁷ Pb/ : ²³⁵ U :	²⁰ ±2σ 20	⁵ Pb/ ±2 ³⁸ U	о` О Ю	» u
NB16-356A and N	IB16-356B Lo	ng Pond	Bay Fo	rmatio	n (UT	- W.	4199E,	494729	9N; Grie	1 Zoi	ie 19T)												
NB16-356B-01	174100000	4.9	0.8	6.4	20	14	70	1416	97.69	-	1.843 0.088	0.152	0.003	0.070	0.0889	0.0040	1376	82	1056	31	911	17 6	4.1
NB16-356B-02	17400000	8.9	2.7	3.3	470	42	6	140	87.29	ŝ	1.720 0.250	0.163	0.004	0.686	0.0754	0.0085	1160	190	993	66	971	24 8	0.6
NB16-356B-03	106900000	6.2	7.1	0.9	58	18	31	267	92.97	-	1.547 0.072	0.097	0.002	0.436	0.1132	0.0045	1849	68	951	31	598	12 6	2.9
NB16-356B-04	168300000	5.0	3.9	1.3	122	26	21	159	88.69	5	0.820 0.340	0.096	0.004	0.874	0.0550	0.0230	1480	320	540	180	590	25 10	9.3
NB16-356B-05	175500000	1.8	1.3	1.4	2	12	600	3288	97.37	_	1.010 0.062	0.092	0.002	0.017	0.0796	0.0047	1150	120	701	32	565	12 8	0.6
NB16-356B-06	178700000	14.5	3.1	4.6	3	11	367	45233	98.17	-	3.375 0.084	0.238	0.004	0.699	0.1033	0.0013	1682	23	1497	20	1376	1 7	9.6
NB16-356B-08	188200000	16.5	0.9	19.4	11	17	155	7827	99.52	_	1.234 0.037	0.130	0.003	0.500	0.0699	0.0015	919	45	816	17	788	[4 8	3.8
NB16-356B-09	165100000	11.8	0.2	72.6	71	28	39	603	96.91	-	1.239 0.060	0.105	0.003	0.281	0.0875	0.0036	1360	80	816	27	643	5 7	8.8
NB16-356B-10	152500000	15.1	1.0	15.0	2550	110	4	40	55.47	ŝ	1.610 0.250	0.122	0.004	0.644	0.0940	0.0100	1460	200	946	100	739	1 7	8.1
NB16-356B-11	169100000	8.0	3.5	2.3	73	23	32	409	96.10	_	1.300 0.150	0.102	0.002	0.450	0.0922	0.0095	1370	190	824	62	626	1 7	5.9
NB16-356B-13	173700000	12.1	0.4	34.1	371	42	П	143	87.20	о Э	0.890 0.130	0.102	0.002	0.503	0.0633	0.0085	920	200	644	67	628	12 9	7.5
NB16-356B-14	150500000	10.4	0.8	13.1	1546	80	ŝ	38	53.98	ŝ	1.060 0.470	0.101	0.004	0.756	0.0700	0.0210	1860	190	660	260	621	22 9	4.1
NB16-356B-15	120000000	4.6	1.6	2.9	232	31	13	103	79.09	ŝ	2.140 0.570	0.151	0.007	0.863	0660.0	0.0230	1820	240	1240	120	906	94	2.8
NB16-356B-16	120700000	2.9	2.9	1.0	629	73	12	28	56.70	3	0.800 1.400	0.111	0.012	0.858 -	0.0200	0.1200	2470	540	1060	360	677	88	3.9
NB16-356B-17	185800000	1.6	0.7	2.4	605	68	11	39	65.10	ŝ	1.000 1.400	0.253	0.013	0.849	0.1080	0.0330	2080	330	1640	250	1454	55 5	9.2
NB16-356B-18	191500000	10.7	9.0	1.2	214	33	15	231	91.65	3	0.170 0.170	0.106	0.003	0.751	0.0690	0.0100	1150	190	674	92	648	5 9	6.1
NB16-356B-19	182800000	7.0	0.1	96.8	14	17	121	2093	99.17	_	1.004 0.036	0.108	0.002	0.178	0.0686	0.0021	873	63	705	18	659	9 []	3.5
NB16-356B-20	192700000	8.3	2.0	4.1	59	24	41	710	97.45	_	1.520 0.110	0.128	0.004	0.895	0.0873	0.0036	1354	79	933	42	776	3 5	4.4
NB16-356B-21	162500000	11.6	1.5	7.7	74	14	19	874	97.02	_	1.918 0.054	0.150	0.003	0.092	0.0926	0.0019	1470	39	1085	19	868	5	8.9
NB16-356B-22	171400000	20.6	0.9	23.4	399	35	6	257	92.74	ŝ	1.085 0.072	0.119	0.002	0.585	0.0653	0.0036	834	98	736	37	725	3	8.5
NB16-356B-23	193700000	12.2	0.2	49.7	50	27	54	2484	98.29	-	3.660 0.093	0.252	0.006	0.436	0.1077	0.0019	1759	31	1562	20	1450	28	8.7
NB16-356B-24	174600000	2.5	2.2	1.1	333	30	6	48	65.10	3	.990 0.740	0.117	0.006	0.841	0.0570	0.0360	1950	360	680	370	711	36 10	4.6
NB16-356B-25	183900000	7.1	0.0	150.4	11	14	127	2782	99.66	-	.939 0.036	0.109	0.002	0.361	0.0631	0.0020	697	68	671	19	668	3 9	9.5
NB16-356B-26	164200000	1.3	0.7	1.8	έ	10	-333	4310	60.66	-	.829 0.051	0.093	0.002	0.015	0.0642	0.0039	680	130	605	28	573	3 9	4.7
NB16-356B-27	167600000	2.5	2.1	1.2	6	10	111	943	98.40	-	.879 0.039	0.091	0.002	0.069	0.0706	0.0029	906	90	637	21	559	0 8	7.7
NB16-356B-28	168000000	11.8	0.3	34.2	32	11	34	1416	98.70	-	.988 0.026	0.102	0.002	0.018	0.0704	0.0013	928	39	697	13	623	0 8	9.5
NB16-356B-29	147500000	10.0	11.1	0.9	1843	97	ŝ	70	78.18	ŝ	5.770 0.520	0.316	0.008	0.567	0.1328	0.0075	2122	95	1917	83	1774	35 8	1.5
NB16-356B-30	157000000	2.7	2.1	1.3	136	18	13	81	78.99	3	).680 0.510	0.096	0.005	0.889	0.0340	0.0350	1920	300	600	270	589	6 6	8.2
NB16-356B-31	167000000	5.4	5.4	1.0	311	29	6	87	79.29	3	0.360 0.360	0.108	0.004	0.775	0.0620	0.0210	1380	280	680	170	662	6 03	7.4
NB16-356B-32	156900000	12.8	0.1	112.2	86	16	19	584	96.85	_	1.315 0.042	0.110	0.002	0.029	0.0868	0.0026	1331	59	850	18	670	0 7	8.9
NB16-356B-33	175900000	5.8	4.7	1.2	0	12	n.d.	23310	99.56	_	.910 0.033	0.106	0.002	0.109	0.0629	0.0020	682	71	656	17	647	6 0]	8.7
NB16-356B-34	161000000	4.2	1.2	3.4	1	11	1100	25750	99.54	_	1.731 0.051	0.170	0.003	0.227	0.0738	0.0017	1021	47	1018	19	1010	l6 9	9.8
NB16-356B-35	175000000	13.0	0.9	13.8	1233	57	5	79	77.63	ŝ	1.870 0.340	0.160	0.005	0.630	0.0866	0.0081	1360	170	1053	120	956	30 6	6.4
NB16-356B-36	168400000	14.9	5.1	2.9	504	41	8	274	92.24	ŝ	3.420 0.170	0.236	0.006	0.629	0.1053	0.0028	1705	51	1503	40	1365	30 7	8.4
NB16-356B-37	163300000	13.4	0.5	28.2	-7	6	-126	58620	98.84	_	1.196 0.038	0.119	0.002	0.643	0.0722	0.0014	980	40	266	18	727	2 9	1.4
NB16-356B-38	162200000	1.7	1.2	1.4	6	10	111	666	99.53	-	.841 0.054	0.099	0.002	0.181	0.0619	0.0038	590	130	612	30	608	2 9	9.3
NB16-356B-39	143700000	6.8	0.1	53.2	- <del>3</del>	15	-500	25060	99.12	-	.975 0.044	0.106	0.002	0.380	0.0654	0.0026	762	87	689	23	648	9 []	4.0
NB16-356B-40	139900000	10.9	1.0	11.1	73	15	21	573	96.93	_	1.372 0.051	0.114	0.002	0.375	0.0856	0.0026	1316	59	875	22	869	11 7	9.7

			Meast	rred o	oncentr	ations						Iso	otopic r	atios				Calo	culated a	ıges (M	a)		ĺ
Sample	90 Zr (cps)	U (ppm)	Th (ppm)	Th/	U ²⁰⁴ Pb (cps)	±2σ	% error	$^{206}{\rm Pb/}$	%Pb ³	C4	$^{207}Pb/_{235}U_{\pm 2\sigma}$	²⁰⁶ Pb/ ²³⁸ U	±2σ	٩	$^{207}\mathrm{Pb/}$	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²³⁵ U	±2σ	²⁰⁶ Pb/	F2σ c	%
NB16-356B-41	178800000	2.4	1.0	2	5 26	17	65	763	98.55	-	2.840 0.130	0.217	0.006	0.594	0.0961	0.0032	1538	61	1360	33	1267	29 8	30.0
NB16-356B-42	108600000	3.2	3.0	-	.1 150	27	18	99	74.70	3	0.310 0.540	0.089	0.005	0.892	0.0150	0.0400	1650	410	390	320	546	31 14	ŧ0.0
NB16-356B-43	160600000	10.2	0.6	16	9 6	6	155	7521	99.32	-	1.064  0.027	0.114	0.002	0.370	0.0674	0.0012	853	36	735	13	694	11 9	94.4
NB16-356B-44	183500000	4.2	3.3	1	.3 69	24	35	240	93.45	г	1.595 0.076	0.103	0.002	0.144	0.1152	0.0050	1865	81	965	30	629	14 6	5.2
NB16-356B-45	15800000	14.2	1.9	~	4 970	130	13	69	76.00	3	0.930 0.160	0.104	0.002	0.712	0.0679	0.0095	1220	170	658	78	637	11 9	96.8
NB16-356B-46	163200000	7.3	0.7	10	.2 281	26	6	135	87.36	3	1.160 0.240	0.129	0.004	0.403	0.0636	0.0084	1120	150	743	120	782	25 5	57.7
NB16-356B-47	127300000	8.5	8.9	-	.0 245	26	11	110	83.80	3	0.750 0.160	0.094	0.002	0.767	0.0590	0.0110	1350	150	543	93	577	13 10	)6.2
NB16-356B-48	172600000	5.6	2.5	2	2 4	12	300	6028	99.78	-	0.969 0.030	0.114	0.002	0.296	0.0622	0.0015	667	52	687	15	695	12 10	01.1
NB16-356B-49	180300000	28.5	9.2	33	.1 92	24	26	1276	98.54	г	1.057 0.034	0.105	0.002	0.335	0.0736	0.0016	1021	45	731	17	645	9 8	38.2
NB16-356B-50	194700000	23.5	0.2	125	.2 21	28	133	4843	99.47	г	0.945 0.035	0.107	0.002	0.100	0.0661	0.0023	799	73	675	18	652	12 9	9.6
NB16-356B-51	132900000	10.0	3.3	3	.1 77	32	42	761	97.50	-	2.984 0.100	0.212	0.005	0.133	0.1050	0.0035	1708	60	1402	25	1239	24 6	58.2
NB16-356B-52	161800000	12.5	2.9	4	.3 99	23	23	209	95.67	1	2.215 0.079	0.155	0.005	0.250	0.1056	0.0045	1693	76	1182	24	929	26 5	51.5
NB16-356B-53	137600000	11.2	0.9	12	8 1023	70	~	99	71.38	3	1.770 0.440	0.138	0.004	0.740	0.0890	0.0150	1510	250	960	190	835	23 5	51.7
NB16-356B-54	179600000	16.9	6.7	5	5 116	16	14	1334	96.73	3	3.260 0.140	0.230	0.004	0.660	0.1041	0.0020	1693	36	1473	31	1333	22 7	75.9
NB16-356B-55	133200000	87.6	55.2	1	.6 3260	200	9	77	76.05	3	0.688 0.120	0.077	0.002	0.553	0.0650	0.0077	970	170	531	63	480	10 9	90.3
NB16-356B-56	175800000	19.8	0.5	40	.2 87	17	20	1051	97.96	-	1.294  0.044	0.118	0.002	0.264	0.0799	0.0020	1182	50	841	20	719	11 8	35.5
NB16-356B-57	168400000	16.1	2.8	ŝ	7 77	14	18	861	97.98	1	1.170 0.028	0.109	0.002	0.441	0.0781	0.0011	1144	27	786	13	667	10 8	34.8
NB16-356B-58	173200000	8.3	0.1	16	.8 13	11	85	2502	60.66	-	0.915 0.028	0.099	0.002	0.324	0.0668	0.0016	814	49	658	15	611	10 9	92.8
NB16-356A-01	109900000	154.1	110.1	1	.4 -7	11	-157	-5113	99.76	г	4.682 0.110	0.3184	0.0053	0.407	0.1067	0.0024	1737	42	1764	19	1782	26 9	96.7
NB16-356A-02	93100000	506.4	31.0	16	.3 9	20	222	10726	99.02	-	4.019 0.099	0.2763	0.0044	0.394	0.1048	0.0025	1708	44	1637	20	1573	22 9	91.8
NB16-356A-03	115400000	458.0	8.8	52	.0 4	12	300	9100	99.73	-	0.907 0.026	0.1068	0.0019	0.197	0.0620	0.0017	667	58	655	14	654	11 9	9.6
NB16-356A-04	110000000	437.7	193.9	5	.3 53	17	32	1496	99.16	ч	3.290 0.130	0.2452	0.0055	0.927	0.0965	0.0025	1547	48	1470	30	1413	29 9	91.7
NB16-356A-05	104200000	459.0	184.6	7	.5 -7	11	-157	-17800	99.75	-	6.450 0.180	0.3724	0.0086	0.916	0.1246	0.0025	2022	36	2041	23	2040	41 9	98.0
NB16-356A-06	110100000	510.0	1.9	264	2 2	12	600	20500	99.79	г	0.926 0.025	0.1098	0.0017	0.325	0.0610	0.0016	627	57	664	13	671	10 10	01.1
NB16-356A-07	72000000	337.7	247.7	-	4 115	15	13	152	88.58	3	0.720 0.220	0.0953	0.0030	0.754	0.0480	0.0170	1450	220	430	150	586	18 13	36.3
NB16-356A-08	107800000	55.9	42.8	-	.3 7	10	143	595	99.73	Ч	0.862 0.057	0.1033	0.0023	0.030	0.0609	0.0042	530	140	621	32	633	13 10	01.9
NB16-356A-09	107800000	123.1	83.0	-	5-5	12	-240	-1990	67.00	Ч	0.912 0.038	0.1093	0.0021	0.278	0.0604	0.0025	576	89	654	20	699	12 10	)2.2
NB16-356A-10	95400000	161.7	143.7	-	.1 -9	17	-189	-1278	98.87	-	0.956 0.053	0.1010	0.0027	0.347	0.0685	0.0038	850	110	678	28	620	16 9	91.4
NB16-356A-11	96400000	310.7	163.2	1	9 19	15	79	2303	77.66	1	2.178 0.071	0.1996	0.0047	0.763	0.0789	0.0020	1164	50	1172	23	1173	26 9	8.5
NB16-356A-12	109000000	140.1	118.1	1	2 1	11	1100	10480	99.72	Ч	0.862 0.037	0.1028	0.0019	0.087	0.0610	0.0028	590	97	627	21	631	11 10	9.0
NB16-356A-13	107800000	178.0	191.4	0	9 6	6	134	2094	99.57	Ч	0.868 0.033	0.1026	0.0018	0.012	0.0616	0.0025	620	89	632	18	630	11 9	9.6
NB16-356A-14	108000000	191.1	252.9	0	.8	12	200	2375	99.65	ч	0.840 0.030	0.1013	0.0017	0.060	0.0601	0.0022	585	81	617	16	622	10 10	0.8
NB16-356A-15	108900000	408.9	246.8	1	.7 -3	10	-333	-19827	77.66	г	2.135 0.047	0.1974	0.0030	0.291	0.0783	0.0017	1152	46	1159	15	1161	16 9	98.8
NB16-356A-16	9590000	104.8	41.1	2	.5 -4	13	-325	-2715	98.95	-	1.496 0.078	0.1473	0.0042	0.410	0.0738	0.0036	1022	95	923	32	885	24 8	36.2
NB16-356A-17	108400000	344.0	509.0	0	7 -7	10	-143	-3457	99.70	-	0.837 0.025	0.1006	0.0019	0.194	0.0604	0.0019	605	71	616	14	618	11 10	0.3
NB16-356A-18	129100000	566.6	862.0	0	.7 99	18	18	465	96.20	3	0.790 0.110	0.0967	0.0019	0.510	0.0592	0.0080	800	180	595	56	595	11 10	0.0
NB16-356A-19	106100000	75.0	73.4	1	.0 10	11	110	1948	99.24	-	6.290 0.170	0.3634	0.0063	0.482	0.1268	0.0034	2050	46	2019	26	1998	30 9	96.3
NB16-356A-20	105800000	46.3	0.5	89	.0 3	11	367	1330	06.66 (	-	1.024 $0.064$	0.1202	0.0032	0.140	0.0618	0.0040	590	130	705	32	731	19 10	3.7

			Measur	ed cone	centrat	ions							Isotopic	ratios				Calcı	ulated ag	ges (Ma			I
Sample	⁹⁰ Zr (cps)	U (ppm)	Th , (ppm)	Th/U ²	⁰⁴ Pb (cps)	±2σ	% error	²⁰⁶ Pb/ ²⁰⁴ Pb ²	%Pb ³	C ⁴ 20	⁷ Pb/	² ±2σ	$^{06}Pb/_{238}U_{\pm 2\sigma}$	β	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	2σ ±2σ	²⁰⁷ Pb/ ²³⁵ U	2α ±2σ	³⁶ Pb/ ± ²³⁸ U [±]	2σ cc	» u
NB16-356A-21	109000000	76.3	60.2	1.3	10	12	120	576	99.49	1 0	.876 0	.045 (	0.1029 0.0022	2 0.052	0.0621	0.0033	610	110	633	24	631	13 99	9.7
NB16-356A-22 NB16-356A-23	88300000 108800000	433.6 1097.0	304.7 12.0	91.6	3 27	12	67 400	30620	98.65 99.89	1 1	0 190.0	036 (	0.1042 0.0019	9 0.050 7 0.495	0.0627	0.0027	960 695	42 4	716 699	10	639 702	10 100	9.2
NB16-356A-24	90100000	452.0	18.5	24.4	15	14	93	2513	99.34	-	.218 0	.041	0.1268 0.0025	5 0.283	0.0696	0.0024	900	71	807	19	769	14 85	5.4
NB16-356A-25	108300000	100.7	44.4	2.3	0	111	.d.	n.d.	99.73	1 4	.051 0	.110 (	0.2989 0.0052	2 0.237	0.0988	0.0026	1591	50	1641	22	1685	26 93	3.2
NB16-356A-26	108900000	58.8	32.4	1.8	8-	10	-131	-583	99.55	1	.870 0	.050 (	0.1014 0.0023	3 0.259	0.0626	0.0036	620	120	628	27	622	13 99	9.0
NB16-356A-27	109400000	304.3	241.4	1.3	-12	12	-100	-1899	19.60	1	.851 0	.025 (	0.1014 0.0016	5 0.160	0.0612	0.0018	626	64	624	14	623	6	9.8
NB16-356A-28	110300000	151.1	128.7	1.2	6	11	122	1262	99.56	1 0	.869 0	.030 (	0.1020 0.0019	9 0.255	0.0622	0.0022	652	75	633	16	626	11 98	8.9
NB16-356A-29	108900000	178.2	129.2	1.4	-2	6	-541	-7829	99.29	1 0	.880 0	.034 (	0.0994 0.0019	090.0	0.0643	0.0025	730	87	638	18	611	11 95	5.7
NB16-356A-29b-1	109000000	81.1	55.9	1.5	-12	12	-100	-535	99.83	1 0	898 0	.055 (	0.1081 0.0027	7 0.435	0.0605	0.0033	550	110	642	29	661	16 103	3.0
NB16-356A-30	11040000	555.1	10.9	50.9	67	15	22	969	97.69	1	.261 0	.044 (	0.1124 0.0017	7 0.396	0.0813	0.0026	1225	65	825	19	687	10 83	3.2
NB16-356A-31	125800000	218.0	64.1	3.4	8	17	213	6163	99.15	1 4	.250 0	.160 (	0.2883 0.0079	0.780	0.1078	0.0029	1757	49	1681	31	1632	39 9.	1.5
NB16-356A-32	109300000	1491.0	8.4	176.9	14	11	79	8864	99.84	1 0	.966 0	019 (	0.1121 0.0016	5 0.411	0.0628	0.0012	697	42	686	10	685	10 99	9.8
NB16-356A-33	108800000	96.3	56.0	1.7	4-	11	-275	-3533	99.58	1 2	.144 0	.077 (	0.2008 0.0037	7 0.307	0.0779	0.0028	1117	70	1158	25	1179	20 93	3.0
NB16-356A-34	108700000	157.9	233.0	0.7	-2	10	-500	-5820	99.47	1 0	869 0	.031 (	0.1020 0.0018	3 0.024	0.0624	0.0025	648	85	632	17	626	11 99	9.0
NB16-356A-35	109200000	325.3	93.9	3.5	8	6	115	4890	99.10	1	.789 0	.046 (	0.1644 0.0029	0.611	0.0792	0.0018	1176	48	1042	17	981	16 8.	1.9
NB16-356A-36	108900000	153.8	80.8	1.9	194	26	13	229	94.35	3 5	.950 0	.410 (	0.3662 0.0053	3 0.574	0.1168	0.0075	1880	120	1929	64	2011	25 89	9.2
NB16-356A-37	107300000	517.0	110.5	4.7	86	16	19	528	97.29	3 0	.961 0	.110 (	0.1173 0.0024	1 0.641	0.0588	0.0067	888	120	659	64	715	14 108	8.5
NB16-356A-38	125100000	778.3	678.1	1.1	39	14	36	1654	98.95	1	.027 0	.027 (	0.1065 0.0019	0.083	0.0706	0.0021	937	60	717	14	652	11 9	1.0
NB16-356A-39	107100000	122.9	116.4	1.1	0	111	.d.	n.d.	98.66	1 0	.883 0	.038 (	0.1074 0.0023	3 0.371	0.0596	0.0024	548	89	638	20	657	13 103	3.0
NB16-356A-40	9340000	251.7	121.8	2.1	-13	12	-92	-3605	99.80	1 3	.585 0	) 960.	0.2737 0.0051	0.403	0.0954	0.0025	1530	48	1545	21	1559	26 97	7.9
NB16-356A-41	107500000	139.6	102.9	1.4	-15	11	-73	-1434	99.70	1 2	.363 0	.063 (	0.2130 0.0037	7 0.393	0.0813	0.0022	1217	52	1229	19	1244	20 97	7.9
NB16-356A-42	107400000	414.9	611.0	0.7	40	16	40	888	98.01	1	.295 0	.047 (	0.1183 0.0019	0.402	0.0797	0.0028	1165	67	840	21	721	11 85	5.8
NB16-356A-43	105600000	158.5	139.5	1.1	-2	13	-650	-5775	99.64	1 0	.863 0	.036 (	0.1030 0.0019	0.290	0.0615	0.0026	615	89	628	19	632	11 100	0.7
NB16-356A-44	108600000	79.5	30.8	2.6	-13	11	-85	-1265	99.32	1 3	.951 0	.110 (	0.2828 0.0052	2 0.272	0.1021	0.0029	1651	53	1624	22	1605	26 90	6.8
NB16-356A-45	121200000	242.5	97.4	2.5	è.	12	-400	-14140	99.55	1 2	0 869.	.071 (	0.2269 0.0041	0.343	0.0870	0.0023	1353	52	1327	20	1318	22 9(	6.7
NB16-356A-46	108100000	645.0	30.1	21.4	9	12	200	10400	99.81	1	.179 0	.026 (	0.1315 0.0020	0.304	0.0654	0.0015	778	49	790	12	796	12 97	7.6
NB16-356A-47	106400000	75.6	30.8	2.5	12	11	92	943	99.36	1 2	.288 0	.088	0.2074 0.0040	0.035	0.0806	0.0032	1177	76	1202	27	1214	21 95	5.4
NB16-356A-47b-1	107800000	154.4	23.7	6.5	-	11	1100	22560	99.59	1 2	.183 0	.062 (	0.2006 0.0032	2 0.068	0.0794	0.0024	1164	60	1173	20	1179	17 98	8.3
NB16-356A-48	106800000	519.0	202.6	2.6	1100	110	10	96	83.10	3 2	.960 0	.180 (	0.2333 0.0043	3 0.635	0.0903	0.0051	1441	95	1382	48	1351	23 94	4.4
NB16-356A-49	107700000	194.9	53.0	3.7	-4	10	-249	-4708	09.60	1	.159 0	.035 (	0.1297 0.0023	3 0.184	0.0651	0.0020	758	65	627	16	786	13 95	5.6
NB16-356A-50	108000000	436.2	110.6	3.9	1	11	1100	59900	99.75	1	0 066.	.073 (	0.1876 0.0052	2 0.896	0.0769	0.0018	1110	48	1106	25	1107	28 99	9.7
NB16-356A-51	125400000	269.4	170.7	1.6	10	15	150	6700	99.73	1	.726 0	.120 (	).3166 0.0061	0.511	0.1088	0.0027	1776	45	1770	22	1773	30 99	9.5
NB16-356A-52	108800000	95.2	48.8	2.0	~	11	157	1011	99.62	1 0	.841 0	.044 (	0.1010 0.0019	0.050	0.0602	0.0032	580	110	614	25	620	11 10	1.0
NB16-356A-53	108100000	122.2	90.7	1.3	-3	10	-333	-3047	99.50	1 0	901 0	.038 (	0.1047 0.0020	0.374	0.0629	0.0026	665	88	652	21	642	12 98	8.4
NB16-356A-54	107800000	401.1	90.5	4.4	8	10	128	7560	99.81	1 2	0 670.	.047 (	0.1952 0.0033	3 0.424	0.0773	0.0018	1128	43	1140	16	1149	18 97	7.9
NB16-356A-55	106800000	297.9	224.5	1.3	4-	10	-250	-17500	99.70	1 5	.034 0	.110 (	0.3256 0.0052	2 0.209	0.1122	0.0023	1832	36	1824	18	1817	25 99	9.2
NB16-356A-56	8860000	877.0	39.4	22.3	22	16	73	3427	99.75	1	.180 0	.037 (	0.1300 0.0022	2 0.280	0.0653	0.0020	776	68	790	17	162	15 97	7.2
NB16-356A-57	107500000	135.2	78.7	1.7	~	11	157	7014	98.41	1 ##	0 ####	.270 (	0.4979 0.0082	2 0.647	0.1907	0.0038	2746	32	2687	20	2604	35 94	4.1

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			Measu	red co	ncentra	vtions				1	1	I	sotopic	ratios				Calc	ulated a	ges (Ma	(	
Sample	⁹⁰ Zr (cps)	U (ppm)	Th (ppm)	Th/U	₁ ²⁰⁴ Pb (cps)	±2σ	% error	²⁰⁶ Pb/ %F	b³ C⁴	1 ²⁰⁷ P	b/ ±2σ J	²⁰⁶ Pb/ ²³⁸ U	±2σ	٩	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²³⁵ U	±2σ	.06Pb/ ± 2 ³⁸ U	2σ % con
NB16-356A-58	106300000	134.9	138.8	1.0	8 (	11	138	1259 99	.86 1	0.8	50 0.03	9 0.1035	5 0.002	1 0.327	0.0595	0.0026	542	94	620	21	635	12 102.4
NB16-356A-59	121500000	161.0	87.6	1.6	89	14	-156	-1500 99	49 1	0.9	55 0.04:	5 0.1101	0.002	5 0.073	0.0632	0.0032	670	110	678	23	673	14 99.3
NB16-356A-60	129700000	494.0	13.1	37.7	7 16	20	125	2625 99	49 1	0.9	64 0.03	7 0.1089	0.002	1 0.145	0.0643	0.0025	737	86	684	19	666	12 97.4
NB16-356A-60a	90100000	244.3	189.4	1.5	3 21	19	90	2781 99	.65 1	5.8	80 0.17	0 0.3554	1 0.006	8 0.398	0.1201	0.0034	1953	50	1957	25	1960	32 99.4
NB16-356A-61	132200000	678.0	14.5	46.8	3 5	22	440	11660 99	.69 1	0.9	20 0.04	1 0.1080	0.002	0 0.052	0.0611	0.0030	661	89	661	22	661	12 100.0
NB16-356A-62	104700000	118.1	111.3	1.1	1 8	11	138	1114 99	.62 1	0.9	40 0.04	3 0.1082	2 0.001	9 0.282	0.0627	0.0027	648	95	668	22	662	11 99.2
NB16-356A-63	123900000	510.0	28.0	18.2	2 399	61	15	135 86	.00 3	1.2	00 0.17	0 0.1194	4 0.00 ₂	6 0.592	0.0708	0.0094	1140	170	787	75	727	15 92.4
NB16-356A-64	130300000	761.0	45.3	16.8	3 22	17	77	3186 99	.23 1	1.0	87 0.03:	5 0.1146	5 0.002	6 0.455	0.0687	0.0020	886	60	746	17	669	15 93.7
NB16-356A-65	88700000	118.0	82.0	1.4	187	23	12	140 90	.40 3	4.1.	20 0.70	0 0.303(	0.011	0 0.673	0.0950	0.0160	1590	270	1590	150	1705	53 91.2
NB16-356A-66	106900000	67.0	42.3	1.6	5 4	10	250	1225 99	.76 1	0.8	37 0.04	6 0.1016	5 0.002	3 0.080	0.0598	0.0034	520	120	611	26	624	13 102.1
NB16-356A-67	106800000	167.7	97.1	1.5	I	11	-1100	-34600 99	.67 1	3.9	78 0.08	7 0.2881	0.004	6 0.306	0.0995	0.0022	1609	42	1628	18	1632	23 97.4
NB16-356A-68	109100000	234.6	234.3	1.0	6- (	6	-109	-2214 99	.67 1	0.0	31 0.03	1 0.1106	5 0.002	1 0.441	0.0608	0.0019	609	68	666	16	676	12 101.5
NB16-356A-69	107600000	317.7	338.7	5.0	0 6	10	n.d.	n.d. 99	.65 1	0.8	61 0.02	3 0.1021	0.001	6 0.276	0.0611	0.0017	636	61	632	13	627	10 99.2
NB16-356A-70	106200000	86.0	30.0	2.5	) 12	10	83	1835 98	.87 1	6.5	10 0.17	0 0.3599	9 0.006	7 0.532	0.1305	0.0033	2097	44	2043	23	1981	32 94.5
NB16-356A-71	103900000	60.6	38.6	1.6	5 13	10	77	349 99	.15 1	0.9	75 0.05	3 0.1075	5 0.002	5 0.137	0.0662	0.0038	730	120	688	28	658	15 95.6
NB16-356A-72	113400000	64.5	74.3	5.0	9 -2	15	-750	-2510 99	.35 1	0.0	34 0.06	9 0.1077	7 0.003	9 0.189	0.0632	0.0049	640	160	664	36	659	23 99.2
NB16-356A-73	104900000	205.6	59.7	3.4	4 5	12	240	3844 99	51 1	1.2	33 0.04.	3 0.1319	0.002	4 0.525	0.0671	0.0020	839	68	812	19	798	14 96.0
NB16-356A-74	111900000	227.7	281.0	3.0	8 25	13	52	679 98	.71 1	0.9	68 0.04.	3 0.1010	0.001	8 0.025	0.0694	0.0032	869	95	684	22	620	10 90.6
NB16-356A-75	91800000	142.5	155.3	5.0	9 12	12	100	810 99	.24 1	0.8	96 0.04	5 0.1029	0.002	4 0.111	0.0638	0.0037	680	120	646	24	631	14 97.7
NB16-356A-76	109600000	113.5	93.4	1.2	3	10	333	2970 99	59 1	0.9	16 0.04	2 0.1067	7 0.002	3 0.343	0.0620	0.0027	626	93	655	22	653	13 99.7
NB16-356A-77	93400000	222.0	62.0	3.6	5 4	15	375	11850 97	.89 1	5.4	40 0.21	0 0.3136	5 0.008	1 0.835	0.1252	0.0031	2028	44	1887	33	1757	40 85.4
NB16-356A-78	129300000	794.0	8.4	94.5	5 248	72	29	294 93	.80 2	0.9	80 0.13	0 0.1104	1 0.001	9 0.438	0.0655	0.0068	880	150	697	56	675	11 96.9
NB16-356A-79	106000000	255.0	115.2	2.2	2	13	163	7185 99	92 1	4.6	56 0.09	9 0.3171	0.004	8 0.403	0.1060	0.0023	1728	39	1758	18	1775	23 96.2
NB16-356A-80	127400000	232.6	141.9	1.6	5 -14	20	-143	-1204 99	73 1	0.7	60 0.04	1 0.0930	0.002	0 0.177	0.0593	0.0033	550	120	572	24	573	12 100.2
NB16-356A-81	105400000	675.0	50.6	13.3	3 41	13	32	1505 99	.13 1	1.2	99 0.03	0 0.1303	3 0.002	0 0.307	0.0718	0.0017	679	48	844	13	789	11 80.1
NB16-356A-81b-1	104800000	143.2	39.7	3.6	5 0	12	n.d.	n.d. 99	.68 1	2.4	53 0.06	4 0.2185	5 0.003	7 0.308	0.0812	0.0021	1214	52	1256	19	1274	19 93.6
NB16-356A-82	109200000	131.7	73.1	1.6	۶- ۲-	11	-157	-1376 99	.58 1	0.8	35 0.03;	3 0.0999	0.001	9 0.177	0.0604	0.0024	578	86	613	18	614	11 100.1
NB16-356A-83	89700000	197.4	187.0	1.1	l -4	15	-375	-3233 99	.25 1	0.8	98 0.04	3 0.1014	1 0.002	5 0.306	0.0640	0.0030	711	100	648	23	622	15 96.0
NB16-356A-84	104300000	54.6	41.3	1.5	3 -11	10	-93	-359 99	32 1	0.8	85 0.05	8 0.1007	7 0.002	3 0.197	0.0636	0.0042	630	130	634	31	618	14 97.5
NB16-356A-84b-1	117200000	63.2	55.2	1.1	l 15	14	93	329 99	.65 1	0.8	74 0.06	0 0.1049	0.003	1 0.039	0.0607	0.0047	550	160	632	33	643	18 101.7
NB16-358A Ross Is	and Format	ion (UT)	M - 680	619E,	494415	:0N; G	rid Zoı	ne 19T)														
NB16-358A-01	183900000	688.8	740.0	5.0	8 (	11	138	24225 99	.85 1	4.5.	21 0.1	3 0.3079	0.01	2 0.823	0.1062	0.0008	1734	14	1733	24	1730	58 99.9
NB16-358A-02	173700000	75.3	46.9	1.6	5 3.1	9.3	300	2132 99	.68 1	0.8	12 0.0:	5 0.0975	0.00	4 0.055	0.0606	0.0037	550	120	598	29	600	23 100.3
NB16-358A-03	171500000	227.8	193.3	1.2	2 14	14	100	1694 99	.74 1	1.0	0.0 0.0	4 0.1154	1 0.00	5 0.398	0.0632	0.0019	700	63	705	21	704.1	26 99.9
NB16-358A-04	165900000	90.3	27.3	3.5	3 6	12	200	2708 99	.68 1	2	24 0.1	1 0.2064	1 0.00	8 0.494	0.0787	0.003	1158	70	1188	35	1209	45 94.7
NB16-358A-05	179700000	228.9	211.9	1.1	l 15.8	9.6	61	1299 99	.65 1	0.8	23 0.0	3 0.0987	0.00	4 0.213	0.0605	0.0017	602	58	608	17	606.6	22 99.8
NB16-358A-06	162900000	198.2	230.6	5.0	) 2	11	550	8480 99	.76 1	0.7.	78 0.0	3 0.0969	00.0	4 0.306	0.0583	0.0018	524	70	583	19	596.3	22 102.3
NB16-358A-07	193000000	409.8	8.1	50.7	7	13	186	5901 99	.72 1	0.8	98 0.0	3 0.106	5 0.00	4 0.404	0.0617	0.0014	653	49	650	17	649.5	23 99.9

			Measu	ired co	ncentra	ations							Isoto	pic ratios					Calcu	lated ag	es (Ma			I
Sample	⁹⁰ Zr (cps)	U (ppm)	Th (ppm)	Th/U	1 ²⁰⁴ Pb (cps)	±2σ	% error	$^{206}\text{Pb/}$	%Pb ³	C ⁴ 20	⁷ Pb/ ±. ³⁵ U	2σ ^{206.} 23	Pb/ _ U*	:2σ ρ	²⁰⁷ F	∓ qai	2σ ²¹	⁰⁶ Pb/ ±	2σ 2	⁷⁷ Pb/ ₁	² ±2σ	⁶ Pb/ ±.	ς - 2α	% uo
NB16-358A-08	181000000	456.2	458.4	1.0	) 13	11	85	3385	69.66	1	.891 0	0.03 0.1	043 0	.004 0.2	89 0.0	623 0.	0014	673	51	646	17	639.5	23 9	0.6
NB16-358A-09	187500000	730.0	120.4	6.1	1 3	10	333	91333	98.66	1	7.75 0	0.26 0.4	1073 0	.016 0.9	44 0.1	384 0.	0013	2206	16	2199	30	2202	73 9	9.6
NB16-358A-10	162700000	560.0	288.0	1.5	9 3	12	400	34100	96.66	1	2.302 0	0.07 0.2	122 0	.008 0.2	86 0.0	791 0.	0012	1171	29	1212	21 1	240.4	42 9	3.8
NB16-358A-11	176800000	214.0	118.1	1.6	3 12	13	108	1662	99.62	1	0.85 0	0.04 0.1	017 0	.004 0.2	31 0.	061 (	0.002	614	69	623	19	624.5	23 10	0.2
NB16-358A-12	213100000	415.0	199.5	2.1	1 28	18	64	4221	69.66	1 4	1.119 0	0.13 0.	.292 0	.012 0.5	91 0.1	029 0.	0017	1675	30	1657	26	1651	59 9	8.0
NB16-358A-13	187500000	153.2	123.1	1.2	2 20	11	55	695	99.51	1 6	0.786 0	0.04 0.0	946 0	.004 0.2	0.0 0.0	607 0.	0022	597	81	589	19	582.5	21 9	8.9
NB16-358A-14	175000000	366.2	356.7	1.(	) 9.2	8.1	88	12576	99.79	1 5	5.834 0	0.17 0.3	3541 0	.013 0.6	99 0.1	201 0.	0011	1956	16	1950	25	1954	64 9	9.5
NB16-358A-15	180000000	378.5	402.5	0.5	) 14	16	114	2100	99.55	1 6	.678 0	0.03 0.0	841 0	.004 0.4	68 0.0	594 (	0.002	564	72	529	18	521	22 9	8.5
NB16-358A-16	178100000	204.8	170.7	1.2	2 -0.4	9.8	-2450	-93350	99.66	-	2.16 0	0.07 0.1	984 0	.008 0.4	03 0.0	793 0.	0015	1170	37	1166	23	1167	41 9	9.6
NB16-358A-17	195100000	437.1	132.2	3.5	3 2	13	650	66500	98.91	1 5	5.159 0	0.15 0.3	3166 0	.012 0.7	93 0.1	188 0.	0008	1937	13 1	845.4	24	1773	59 8	9.9
NB16-358A-18	182000000	225.5	278.7	3.0	3 7	14	200	2883	99.67	1 6	0.789 0	0.04 0.0	952 0	.004 0.4	65 0.0	603 0.	0021	596	75	589	20	586.4	22 9	9.6
NB16-358A-19	169900000	658.0	637.0	1.(	) 15.8	8.8	56	3595	99.72	1 6	.824 0	0.03 0.	0 860.	.004 0.3	53 0.0	615 (	100.0	653	34	610.7	15	602.4	22 9	8.6
NB16-358A-20	170600000	183.6	297.0	0.6	5 16	10	63	679	99.47	1 6	0 797 0	0.03 0.0	935 0	.004 0.0	42 0.0	621 0.	0023	643	80	593	20	576.2	21 9	7.2
NB16-358A-21	158600000	163.9	41.3	4.(	) 25	14	56	690	99.53	1	1.03 0	0.05 0.1	167 0	.005 0.2	53 0.	064 0.	0024	742	74	717	24	711	27 9	9.2
NB16-358A-22	179200000	82.8	36.2	2.5	3 2.1	6	429	2036	99.72	1 6	.409 0	0.03 0.0	539 0	.002 0.3	73 0.0	548 (	0.004	330	150	343	24	338.4	13 9	8.7
NB16-358A-23	175000000	68.1	142.8	0.5	5 10	10	100	596	99.55	1	0.79 0	0.06 0.0	932 0	.004 0.2	58 0.0	614 (	0.004	580	140	584	33	574.5	22 9	8.4
NB16-358A-24	182500000	348.4	136.5	2.6	5 4.6	9.1	198	27893	99.61	1 6	.968	0.2 0.3	821 0	.014 0.6	.0 66	132 0.	0012	2123	15	2106	25	2086	67 5	8.3
NB16-358A-25	14130000	129.2	72.8	1.6	3 19	12	63	312	93.47	1 6	.807 0	0.06 0.0	1559 G	.003 0.2	61 0.1	046 0.	0075	1670	130	595	36	350.4	16 5	8.9
BL15-001 Balls Lai	ke Formatior	עTU) ו	- 26628	8E, 50	11710	l; Grid	Zone	20T)																
BL15-01-001	280200000	481.1	97.8	0.2	2 -4	11	275	-9108	99.75	1 6	.467 0	0.0 10.0	625 5	E-04 0.1	91 0.0	535 0.	0011	340	47	388.6	~	391	3 10	0.6
BL15-01-002	271500000	305.0	141.7	0.5	5 10	12	120	6250	99.83	1	751 0	0.02 0.1	725 0	.001 0.3	71 0.0	729 0.	8000	1008	23 1	026.9	7.6 1	025.7	7.1 9	6.6
BL15-01-003	273100000	256.0	227.0	0.5	<u>7-</u> 6	13	186	-4671	99.70	1 6	.917 0	0.02 0.1	0.88 0	.001 0.3	0.0 20	611 0.	0013	643	44	662	10	665.4	6.5 10	0.5
BL15-01-004	256800000	61.3	50.3	3.0	3 -15	21	140	-987	99.49	1	362	0.1 0.2	2086 0	.004 0.2	25 0.0	825 0.	0039	1231	92	1228	29	1225	21 9	9.8
BL15-01-005	289200000	607.0	57.7	0.1	l -21	12	57	-2338	99.76	1 6	.499 0	0.01 0.0	651 6	E-04 0.2	26 0.0	553 0.	0012	435	44	410.8	6.8	406.8	3.6 9	0.6
BL15-01-006	275600000	567.2	375.8	0.7	-4-	11	275	-11150	99.72	1	0.5 0	0.01 0.0	659 5	E-04 0.0	21 0.0	549 (	0.001	402	40	411.4	5.6	411.1	3.2 9	6.6
BL15-01-007	305600000	258.2	304.9	1.2	2 -10	23	230	-2068	99.52	1 6	.508 0	0.03 0.0	657 8	E-04 0.1	68 0.0	557 0.	0028	420	110	416	18	410.3	4.8 9	8.6
BL15-01-008	258600000	688.0	222.2	0.3	3 2	15	750	26325	99.76	1 6	.501 0	0.01 0.0	661 6	E-04 0.0	76 0.	055 (	0.001	411	44	412	6.2	412.4	3.3 10	0.1
BL15-01-009	268700000	358.1	121.7	0.3	3 -15	17	113	-1861	99.61	1 6	.505 0	0.02 0.0	655 1	E-03 0.2	26 0.0	563 0.	0016	453	62	414.7	9.8	408.9	5.7 9	8.6
BL15-01-010	311900000	1054.6	20.2	0.0	) 1	21	2100	149600	06.66	1	0.983 0	0.02 0.1	132 0	.002 0.6	61 0.0	627 0.	8000	697	28	694.8	8.4	691.3	8.9 9	9.5
BL15-01-011	282400000	190.9	124.6	0.7	7 1	18	1800	20250	99.55	1 6	0.716 0	0.02	.088 0	001 0.1	16 0.	059 (	0.002	554	71	549	14	543.8	6.4 9	9.1
BL15-01-012	255800000	145.6	77.4	0.5	5 -13	20	154	-2195	99.82	1	.676 0	0.06 0.1	693 0	.002 0.1	85 0.	072 0.	0022	166	58	1002	20	1008	13 10	0.6
BL15-01-013	248200000	255.6	122.9	0.5	5 -15	18	120	-4373	99.82	1	652 0	0.05 0.2	251 0	.002 0.2	24 0.	085 0.	0016	1311	35	1314	14	1309	12 9	9.6
BL15-01-014	272600000	275.9	103.1	0.4	4 -10	13	130	-8130	99.83	1 3	3.061 0	0.03 0.2	9463 0	.002 0.2	62 0.0	898 (	0.001	1422	21 1	423.1	8.2	1419	11 9	9.7
BL15-01-015	281500000	303.7	273.0	0.5	11 6	13	118	2285	99.66	1 6	).526 0	0.0 10.0	683 7	E-04 0.0	81 0.0	558 0.	0013	429	52	428.8	7.9	426	4.2 9	9.3
BL15-01-016	275500000	92.3	42.0	0.5	5 18	20	111	563	99.75	2	0.72 0	0.02 0.0	904 0	.002 0.7	64 0.0	579 0.	9000	525	23	550	8.7	557.9	10 10	1.4
BL15-01-017	244700000	122.0	99.0	3.0	3 11	22	200	834	99.77	1 0	.508 0	0.03 0.0	)659 C	.001 0.1	79 0.0	554 0.	0036	390	140	415	22	411.5	8.8	9.2
BL15-01-018	25060000	214.4	166.9	3.0	3 -14	16	114	-1823	99.64	1 0	.888 0	0.02 0.1	051 0	.001 0.0	03 0.0	611 0.	0018	648	64	646	13	644	6.9 9	9.7
BL15-01-019	272200000	306.8	90.5	0.3	3 -2	12	600	-30480	99.79	1	0 969"	0.02	.168 0	.001 0.2	21 0.0	728 (	001	1006	28 1	007.2	8.5 1	001.2	7.6 9	9.4

			Measu	red c	oncentr	ations							Isot	opic ra	tios				Calcı	ulated ag	ges (Mi	(1		Í
Sample	⁹⁰ Zr (cps)	U (ppm)	Th (ppm)	Th/L	J ²⁰⁴ Pb (cps)	±2σ	% error	²⁰⁶ Pb/ ²⁰⁴ Pb ²	%Pb ³	C4	²⁰⁷ Pb/ : ²³⁵ U :	t2σ	⁰⁶ Pb/ ²³⁸ U	±2σ	β	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ : ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²³⁵ U	±2σ	²⁰⁶ Pb/ ²³⁸ U	±2σ ⁹	% uo
BL15-01-020	269800000	110.1	29.6	0.	3 5	13	260	) 516(	97.21	-	3.590 0	.410	0.218	0.019	0.984	0.1106	0.0051	1768	06	1420	110	1250	100 8	8.0
BL15-01-021	28700000	610.7	428.0	0.	7 4	16	400	14010	99.84	1	0.594	0.01 (	0.0764 (	6E-04	0.364	0.0565	0.001	468	38	473	7.1	474.3	3.6 10	0.3
BL15-01-022	25660000	37.3	16.2	0	4 -3	15	500	) -2453	99.54	Ч	1.701	0.09 (	).1688	0.003	0.394	0.0729	0.0035	1009	90	1009	32	1005	17 9	9.6
BL15-01-023	260100000	522.0	289.4	0	6 11	15	136	3545	99.74	г	0.49	0.01 (	0.0646	6E-04	0.176	0.0551	0.0011	405	47	404.6	6.8	403.3	3.8 9	6.7
BL15-01-024	277500000	183.9	101.3	0	6 6	11	183	3205	5 99.51	-	0.717	0.02 (	0.0885	0.001	0.129	0.0588	0.0017	567	64	550	12	547.3	6.4 9	9.5
BL15-01-025	26560000	376.5	155.9	0	4 11	21	191	2682	99.67	-	0.507	0.01 (	).0666 {	8E-04	0.026	0.0555	0.0015	418	61	417.4	7.9	415.4	4.8 9	9.5
BL15-01-026	282800000	300.0	56.5	0.	2 11	12	109	3382	99.54	г	0.899	0.02 (	0.1027	0.001	0.43	0.0634	0.0013	725	45	650	10	630.3	6.6 9	7.0
BL15-01-027	274400000	282.6	83.7	0.	3 1	13	1300	138140	95.30	1	10.32 0	.110	0.415	0.004	0.801	0.1812	0.0012	2664	11	2466	10	2236	19 9	0.7
BL15-01-029	274400000	553.4	96.4	0.	2 -13	12	92	: -3397	7 99.81	1	0.504	0.01 (	).0667	5E-04	0.162	0.0549	0.0009	406	36	414	5.4	416	3.1 10	0.5
BL15-01-030	271800000	603.5	140.2	0.	2 9	19	211	5145	99.64	-	0.488	0.01 (	0.0637	7E-04	0.182	0.056	0.0014	450	55	403.4	8.6	397.8	4.4 9	8.6
BL15-01-031	273600000	231.0	36.0	0.	2 5	14	280	18100	98.46	г	5.882	0.07 (	).3332	0.003	0.605	0.1279	0.0011	2068	15	1958.7	9.8	1854	15 9	4.7
BL15-01-032	275800000	109.9	118.6	Ι.	1 2	23	1150	) 2184(	99.79	г	5.196	0.09	0.332	0.003	0.103	0.1136	0.002	1866	32	1851	14	1850	15 9	6.6
BL15-01-033	26560000	68.1	23.7	0.	3 -3	15	500	) -6427	99.45	1	2.992	0.06 (	).2423	0.004	0.181	0.0903	0.0021	1419	45	1403	16	1398	18 9	9.6
BL15-01-034	273800000	331.3	85.4	0.	3 -4	12	300	) -24200	99.56	1	3.199	0.04 (	0.2476	0.002	0.636	0.0937	0.0009	1502	18	1455.9	9.6	1425.8	12 9	7.9
BL15-01-035	27300000	1017.1	555.3	0.	5 -14	11	52	-5693	99.80	-	0.51	0.01 (	).0667	5E-04	0.265	0.0556	0.0007	440	29	418.4	4.5	415.9	2.8 9	9.4
BL15-01-036	284300000	222.3	88.7	0.	4 -2	15	750	-8775	5 99.59	-	0.504	0.01 (	0.0654	8E-04	0.133	0.0559	0.0017	436	66	413.6	9.3	408.4	4.7 9	8.7
BL15-01-037	284400000	131.6	108.6	0.	8 10	13	130	) 1344	99.62	-	0.665	0.02 (	0.0835	0.001	0.092	0.0578	0.0017	520	99	518	12	516.9	6.3 9	9.8
BL15-01-038	270900000	175.8	83.9	0.	5 2	12	600	7295	99.82	ч	0.54	0.02 (	3 8690.0	8E-04	0.022	0.0557	0.0017	426	67	437	10	434.6	5	9.5
BL15-01-039	270700000	60.0	52.1	0.	9 4	20	500	5105	99.58	г	3.99	0.13 (	0.2881	0.005	0.303	0.1006	0.0028	1644	56	1634	26	1632	23 9	6.6
BL15-01-040	271700000	174.6	142.0	0.	8 -5	13	260	-2786	99.75	г	0.515	0.02 (	0.0673 7	7E-04	0.152	0.0557	0.0018	422	69	422	11	419.8	4.3 9	9.5
BL15-01-041	23650000	116.8	92.7	0.	8 12	18	150	1063	\$ 99.56	-	0.859	0.04 (	0.1017	0.001	0.255	0.0608	0.0026	630	92	627	19	624.2	8	9.6
BL15-01-042	262400000	353.4	224.5	0	6 8	13	163	3316	5 99.71	1	0.498	0.02 (	0.0651 7	7E-04	0.071	0.0556	0.002	418	75	409	11	406.4	4.3 9	9.4
BL15-01-043	309500000	305.6	44.0	0.	1 -6	23	383	3 -4287	99.68	-	0.506	0.02 (	0.0657	9E-04	0.324	0.0555	0.002	413	79	415	12	410.2	5.3 9	8.8
BL15-01-044	300200000	606.0	28.2	0	0 -2	15	750	) -39600	12.66 (	-	0.922	0.03 (	0.1078	0.003	0.782	0.0628	0.0013	721	47	662	17	660	15 9	9.7
BL15-01-045	274600000	302.2	132.9	°.	4 5	12	240	4742	99.73	-	0.507	0.01 (	).0666	6E-04	0.064	0.0552	0.0012	414	50	417	7.5	415.7	3.6 9	9.7
BL15-01-046	279800000	234.6	81.5	0.	3 -7	11	157	-4611	90.76	-	966.0	0.02 (	0.1142	0.001	0.234	0.0633	0.0012	718	39	702	10	697.2	5.9 9	9.3
BL15-01-047	274200000	337.9	197.4	0.	6 -4	10	250	) -6645	5 99.73	г	0.508	0.01 (	0.0669 (	6E-04	0.146	0.0549	0.0012	396	49	416.4	7.7	417.5	3.6 10	0.3
BL15-01-048	279500000	105.0	57.7	0.	5 6	15	250	2005	99.48	1	0.8	0.03 (	0.0966	0.001	0.098	0.0603	0.0027	568	98	598	18	594.2	7 9	9.4
BL15-01-049	275900000	473.9	115.7	0.	2 11	15	136	12900	98.66 (	-	3.21	0.04 (	0.2539	0.002	0.714	0.0914	0.0007	1456	14	1458.5	8.7	1458.3	11 10	0.0
BL15-01-050	265100000	590.5	694.0	-	2 -18	12	67	-2511	99.79	1	0.501	0.01 (	).0663 (	6E-04	0.156	0.0546	0.0009	393	38	412	5.7	413.8	3.7 10	0.4
BL15-01-051	29600000	52.1	71.0	1.	4 -3	14	467	-1820	0.99.67	-	0.71	0.05 (	0.0883	0.002	0.017	0.0583	0.0041	510	150	550	28	545	13 9	9.1
BL15-01-052	244300000	125.5	63.5	0.	5 -1	27	2700	-11740	99.74	-	0.646	0.04 (	0.0821	0.002	0.042	0.0567	0.004	480	160	516	26	509	11 9	8.6
BL15-01-053	275200000	185.7	29.8	0.	2 5	13	260	3956	8 99.67	ч	0.727	0.02 (	0.0892	9E-04	0.139	0.0589	0.0014	576	51	555.1	9.9	550.9	5.1 9	9.2
BL15-01-054	269100000	264.5	163.6	0	6 12	13	108	3 1716	99.64	г	0.508	0.01	0.067	7E-04	0.131	0.0547	0.0015	391	62	416.4	9.2	417.8	4.1 10	0.3
BL15-01-055	280100000	993.0	116.4	0.	1 4	13	325	19850	99.84	1	0.515	0.01 (	0.0672 (	6E-04	0.386	0.0552	0.0007	417	27	421.4	4.5	419.4	3.4 9	9.5
BL15-01-056	25630000	121.8	97.9	0.	8 20	16	80	) 454	1 99.67	7	0.503	0.01 (	0.0678	0.001	0.856	0.0543	0.0006	380	28	413	9.3	422.9	8.1 10	12.4
BL15-01-057	265400000	803.8	422.9	0.	5 -2	13	650	-32675	99.80	п	0.54	0.01 (	3.0698	5E-04	0.027	0.0556	0.000	439	37	438.4	5.5	435	3.2 9	9.2
BL15-01-058	25860000	495.0	62.8	0.	1 -8	17	213	-4493	89.66	1	0.482	0.01 (	0.0633	7E-04	0.212	0.0548	0.0014	420	56	400	8	395.6	4.1 9	8.9
BL15-01-059	27940000	140.0	125.0	0.	9 3	13	433	327(	17.66 (	1	0.441	0.02	0.059	9E-04	0.011	0.0543	0.0023	370	89	370	12	369.2	5.5 9	9.8

			Measui	red cc	ncentr	ations							Isot	opic r	atios				Calc	culated a	ges (M	a)	
Sample	⁹⁰ Zr (cps)	U (ppm)	Th (ppm)	Th/U	J ²⁰⁴ Pb (cps)	±2σ	% error	²⁰⁶ Pb/ ²⁰⁴ Pb ²	%Pb ³	C4	²⁰⁷ Pb/ ²³⁵ U	±2σ	²⁰⁶ Pb/ ²³⁸ U	±2σ	θ	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²³⁵ U	±2σ	²⁰⁶ Pb/ ²³⁸ U	$\pm 2\sigma \frac{\%}{con}$
BL15-01-060	281600000	409.3	261.9	0.6	5 13	14	108	2411	99.44	-	0.508	0.01	0.0628	6E-04	0.012	0.0577	0.0013	526	51	417.5	7.5	392.4	3.6 94.(
BL15-01-061	258800000	565.0	498.0	0.0	9 14	17	121	2886	99.76	-	0.473	0.01	0.0626	6E-04	0.265	0.0547	0.0009	394	39	392.8	5.8	391.1	3.6 99.6
BL15-01-062	281000000	51.1	22.8	0.4	4 -11	14	127	-930	99.41	г	1.711	0.06	0.1697	0.002	0.084	0.0731	0.0027	1012	74	1010	23	1010	13 100.0
BL15-01-063	296200000	267.3	83.5	0	3 -1	16	1600	-21440	99.57	1	0.518	0.02	0.067	8E-04	0.139	0.0566	0.002	452	78	423	13	418.2	4.9 98.9
BL15-01-064	290400000	134.4	80.5	0.6	5 12	14	117	1321	99.50	ч	0.807	0.03	0.0974	0.001	0.158	0.0603	0.002	605	76	599	16	599	7.6 100.0
BL15-01-065	280400000	1351.8	333.5	0	2 17	13	76	5541	99.64	7	0.441	0	0.0595	4E-04	0.739	0.0538	0.0002	362.9	6.5	370.7	2.3	372.6	2.7 100.5
BL15-01-066	274600000	75.6	30.7	0.4	4 1	14	1400	15390	99.58	г	1.759	0.04	0.1727	0.002	0.193	0.0732	0.0019	1012	50	1031	17	1028	12 99.7
BL15-01-067	296500000	944.0	784.0	9.0	8 6	15	250	12750	99.86	г	0.509	0.01	0.0666	6E-04	0.308	0.0552	0.0009	414	38	417.3	5.8	415.5	3.5 99.6
BL15-01-068	271100000	162.1	31.5	.0	2 1	11	1100	12430	99.62	1	0.502	0.02	0.0659	7E-04	0.044	0.0545	0.0017	380	71	412	10	411.2	4.3 99.8
BL15-01-069	277500000	243.6	182.7	0.8	8 11	14	127	1919	99.71	1	0.568	0.01	0.0737	8E-04	0.306	0.0557	0.0012	428	50	456.2	8.3	458.8	4.8 100.6
BL15-01-070	295100000	79.8	55.3	0.:	7 8	14	175	3144	99.20	1	3.541	0.07	0.2595	0.004	0.276	0.0995	0.002	1613	35	1539	16	1487	18 96.6
BL15-01-071	287200000	725.6	152.3	0	2 12	19	158	4673	69.66	г	0.507	0.01	0.0661	6E-04	0.083	0.0562	0.0012	453	49	416.3	7.4	412.5	3.7 99.1
BL15-01-072	273600000	218.3	248.7	1.	1 5	11	220	3420	99.74	г	0.513	0.02	0.0671	7E-04	0.004	0.0556	0.0018	419	72	419	10	418.9	4.1 100.0
BL15-01-073	275400000	111.5	98.8	0.5	L- 6	11	157	-3220	99.63	1	1.766	0.05	0.1732	0.002	0.112	0.0735	0.002	1026	54	1034	16	1029.5	9.96 9.6
BL15-01-074	250400000	195.2	209.8	1.	1	12	1200	19770	99.55	1	0.729	0.02	0.0895	0.001	0.104	0.0587	0.002	542	78	557	14	552.3	6.5 99.2
BL15-01-075	264400000	113.0	44.7	0.4	4 21	19	90	578	96.96	2	0.727	0.05	0.093	0.005	0.906	0.0573	0.0017	499	67	553	26	573	27 103.6
BL15-01-076	277000000	321.3	227.7	0	7 -7	14	200	-3403	99.76	г	0.467	0.01	0.0623	8E-04	0.247	0.0544	0.0015	375	60	389	8.8	389.8	4.5 100.2
BL15-01-077	308800000	272.5	80.9	0.	3 -4	19	475	-5575	99.77	г	0.514	0.02	0.067	0.001	0.07	0.056	0.0027	430	110	420	16	418	6.1 99.5
BL15-01-078	254600000	921.0	147.7	0.	2 23	21	16	2930	99.83	7	0.466	0.01	0.0632	7E-04	0.74	0.0535	0.0006	348	25	388.2	4.6	395.3	4 101.8
BL15-01-079	277400000	111.9	67.0	0.6	5 4	14	350	2990	99.47	Ч	0.737	0.02	0.0899	0.001	0.199	0.0598	0.002	581	74	559	14	554.8	8.2 99.2
BL15-01-080	25960000	45.3	34.1	0.5	8 10	15	150	573	99.45	-	0.945	0.04	0.1114	0.002	0.196	0.0629	0.003	720	100	681	23	681	12 100.0
BL15-01-081	273500000	961.0	111.9	0	1 -6	13	217	-12317	99.78	-	0.502	0.01	0.0659	5E-04	0.134	0.0556	0.0007	435	30	412.7	3.7	411.2	2.9 99.6
BL15-01-082	271700000	151.3	178.0	1.	2 -2	19	950	-8710	99.50	ч	0.829	0.03	0.0997	0.002	0.089	0.0607	0.0027	631	89	611	19	612.5	9.6 100.2
BL15-01-083	269200000	403.0	265.0	0.:	7 11	13	118	5436	98.85	ч	1.453	0.05	0.1384	0.003	0.912	0.0764	0.0013	1105	34	910	22	835	3.19 91.8
BL15-01-084	282300000	58.0	55.1	1.(	0 1	15	1500	6110	99.58	Ч	0.734	0.05	0.0899	0.003	0.106	0.0596	0.0043	560	150	555	28	555	15 100.0
BL15-01-085	280700000	198.7	46.0	0.	2 3	13	433	4990	69.66	Ч	0.476	0.01	0.0631	7E-04	0.186	0.0552	0.0017	394	67	395	10	394.6	4.4 99.9
BL15-01-086	261200000	348.0	66.6	0.	2 18	15	83	3818	99.46	7	1.681	0.02	0.1684	0.002	0.943	0.0726	0.0004	1003	9.7	1000.7	8.4	1003.4	9.2 100.3
BL15-01-087	282000000	104.5	23.2	0.	2 9	14	156	5240	99.80	1	6.691	0.09	0.3799	0.004	0.424	0.128	0.0017	2076	23	2072	11	2075	18 100.1
BL15-01-088	272000000	81.3	46.0	0.6	5 5	14	280	4836	98.55	-	3.763	0.08	0.2608	0.004	0.73	0.106	0.0014	1727	24	1589	16	1493	20 94.(
BL15-01-089	286400000	138.3	94.2	0.:	7 -4	15	375	-2720	99.68	1	0.518	0.02	0.067	0.001	0.098	0.0555	0.0025	440	93	422	15	417.8	6 99.(
BL15-01-090	280200000	95.9	30.3	0	3 4	15	375	2598	99.44	1	0.769	0.03	0.0933	0.001	0.292	0.0601	0.0023	607	86	577	17	574.9	7.6 99.6
BL15-01-091	284700000	277.8	243.0	0.5	9 -3	14	467	-10770	99.76	г	0.827	0.02	0.0991	0.001	0.145	0.0608	0.0015	621	52	611	10	609.3	6.9 99.7
BL15-01-092	268300000	176.8	21.3	0	1 8	14	175	1615	99.77	-	0.491	0.02	0.0646	8E-04	0.004	0.0551	0.0019	395	70	406	11	403.5	4.8 99.4
BL15-01-093	293900000	376.0	223.0	0.6	5 -11	12	109	-2713	99.56	-	0.513	0.02	0.0671	7E-04	0.162	0.0561	0.0018	453	70	420	10	418.7	4.1 99.7
BL15-01-094	242200000	91.7	55.8	0.6	5 1	21	2100	9860	99.46	ч	0.819	0.05	0.0979	0.002	0.149	0.0609	0.0033	600	120	605	26	602	11 99.5
BL15-01-095	275400000	201.4	72.5	0.4	4 -13	12	92	-1631	99.65	Ч	0.747	0.02	0.091	8E-04	0.038	0.0595	0.0016	587	59	566	Π	561.6	4.8 99.2
BL15-01-096	278900000	291.2	52.4	0.	2 4	11	275	5308	99.57	Ч	0.487	0.01	0.0633	6E-04	0.2	0.0564	0.0014	461	53	402.4	7.9	395.8	3.9 98.4
BL15-01-097	294900000	97.1	54.5	0.6	5 8	21	263	1136	99.55	г	0.615	0.03	0.079	0.001	0.104	0.0569	0.0028	480	110	488	17	490.2	8.2 100.5
BL15-01-098	296600000	206.1	136.3	0.5	7 -2	18	006	-11025	09.66	1	0.719	0.03	0.0902	0.001	0.013	0.0589	0.0023	541	87	552	16	556.7	7.7 100.9

			Measui	red con	icentrat	tions							Isotc	pic rat	so				Calcu	llated ag	es (Ma	0		
Sample	⁹⁰ Zr (cps)	U (ppm)	Th (ppm)	Th/U	²⁰⁴ Pb (cps)	±2σ	% error	$^{206}{\rm Pb}/$ $^{204}{\rm Pb}^{2}$	%Pb ³	$C^4$	⁰⁷ Pb/ ± ²³⁵ U ±	²⁰ 2σ 20	⁵ Pb/ : ³⁸ U	±2σ	β	⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	$\pm 2\sigma$	⁰⁷ Pb/ _	±2σ	⁵⁶ Pb/ ± ²³⁸ U ±	τ ₃	% uo
BL15-01-099	278300000	210.5	101.9	0.5	6	14	156	1773	99.67		0.5 (	0.01 0.	0654 8	E-04 (	.356	0.056	0.0015	437	63	412	10	408.5	4.6 9	9.2
BL15-01-100	279600000	296.0	184.7	0.6	-2	12	600	-11115	99.80	1	0.489 (	0.01 0.0	0647 7	E-04 (	.081 (	0.0556	0.0015	424	60	403.5	6	404.5	3.9 10	0.2
BL15-01-101	265700000	222.1	100.8	0.5	ή	14	280	-13300	99.72	1	3.31 (	0.04 0.	2585 (	0.002 (	.198 (	0.0935	0.0013	1501	25	1484	9.9	1482	12 9	9.9
BL15-01-102	274700000	132.6	67.9	0.5	-2	12	600	-4900	99.71	1	0.49 (	0.02	0639 8	E-04 (	.013 (	0.0561	0.002	425	77	403	11	399.5	4.6 9	9.1
BL15-01-103	293700000	493.0	280.0	0.6	1	19	1900	56500	99.78	-	0.8 (	0.01	0964 (	001 (	.234 (	0.0605	0.0011	620	39	596.5	7.4	593	6 9	9.4
BL15-01-104	273300000	120.7	151.9	1.3	ιċ	11	220	-2620	99.38	1 (	0.767 (	0.03 0.	0927 (	001 (	0.038 (	0.0604	0.0023	604	81	576	15	571.6	7.4 9	9.2
BL15-01-105	278600000	388.8	167.5	0.4	ю	13	433	10080	99.59	1	0.515 (	0.01	0668 7	E-04 (	.073 (	0.0564	0.0013	467	53	421.9	6.9	416.5	3.9 9	8.7
BL15-01-106	272500000	300.5	116.4	0.4	4	13	325	5673	99.65	1	0.492 (	10.0	0.065 6	E-04 (	.138 (	0.0553	0.0014	411	54	406.7	7.3	405.9	3.7 9	9.8
BL15-01-107	292100000	243.8	39.2	0.2	ċ	11	367	-6263	99.54	1	0.509 (	0.01	0655 8	E-04 2	E-04	0.057	0.0018	487	68	416.7	9.2	408.9	4.9 9	8.1
BL15-01-108	281500000	244.1	93.1	0.4	8	10	125	2331	99.78	1	0.493 (	0.01	0647 6	E-04	0.09 (	0.0553	0.0015	426	63	408.3	9.4	403.9	3.9 9	8.9
BL15-01-109	269800000	408.0	21.3	0.1	\$- \$	13	163	-3800	99.76	1	0.495 (	0.01	0655 5	E-04 (	0.081 (	0.0546	0.001	405	47	407.4	6.9	408.8	3.3 10	0.3
BL15-01-110	278400000	219.6	53.4	0.2	11	12	109	2267	99.45	1	0.831 (	0.04 0.	0957 (	0.003 (	.795 (	0.0627	0.0016	695	53	609	20	589	18 9	6.7
BL15-01-111	278200000	182.5	11.3	0.1	-4	11	275	-19275	99.45	1	6.304 (	0.06 0.	3602 (	0.003 (	.462 (	0.1272	0.001	2058	14	9.6103	7.6	1983	14 9	8.2
BL15-01-112	274900000	174.7	85.1	0.5	ċ-	13	433	-6423	99.64	1	0.793 (	0.02 0.	) 9960	0.002 (	.382 (	0.0595	0.0016	590	60	591	13	594.4	9.2 10	0.6
BL15-01-113	268900000	148.0	20.2	0.1	12	13	108	2427	99.38	1	1.868 (	0.03 0.	1739 (	0.002 (	.222 (	0.0778	0.0014	1136	36	1068	12 1	033.3	9.1 9	6.8
BL15-01-114	27200000	173.0	105.4	0.6	~	14	200	2519	99.62	1	0.724 (	0.02 0.	0892 (	0.001 (	.132 (	0.0589	0.0014	562	49	553.1	9.4	550.7	6 9	9.6
BL15-01-115	273400000	226.4	108.3	0.5	7	14	700	37300	99.87	-	3.975 (	0.05 0.	2882 (	0.002 (	.339 (	0.1001	0.0011	1623	20 1	629.1	9 1	632.5	11 10	0.2
BL15-01-116	267500000	285.0	260.0	0.9	-2	13	650	-10860	69.66	-	0.51 (	0.01	0669 7	E-04 (	.184 (	0.0553	0.0013	418	54	418.7	8.8	417.1	4.3 9	9.6
BL15-01-117	282400000	31.2	26.3	0.8	3	12	400	2133	10.66	-	1.975 (	0 60.0	1794 (	.003 (	.216 (	0.0795	0.0037	1150	95	1107	33	1066	19 9	6.3
¹ after Hg correct	ion																							
² in counts per se	cond																							

³ radiogenic ⁴ Correction factor: 1 = threshold ²⁰⁴Pb cps for no correction (80 cps); 2 = threshold % for ²⁰⁴Pb-based correction (21 % error); 3 = threshold % for ²⁰⁸Pb-based correction (98.5 % radiogenic Pb)

		Meä	asured	concer	itratior	IS						Isotc	pic rati	os				Calcul	lated age	es (Ma)	_	
⁹⁰ Zr (cps	t) U (ppm)	Th (ppm)	Th/U	²⁰⁴ Pb (cps)	±2σ	% error	$^{206}{\rm Pb}/$	$%Pb^{3}$	$C^4$	⁰⁷ Pb/ ± ²³⁵ U	2σ ²⁰⁶ 2	⁵ Pb/ : ³⁸ U	<del>1</del> 2σ	٩	²⁰⁵ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁵ Pb/ ± ²⁰⁶ Pb	$2\sigma^{20}$	⁷ Pb/ ± ³³⁵ U ±	-2σ 2 ⁽²	⁶ Pb/ ± ³⁸ U ±	2σ % con
2763000	00 191.4	85.98	0.45	2	12	600.0	21255	99.70	-	1.960 0.	029 (	).186	0.002 (	.043	0.0761	0.0013	1092	33	1102	10	1100	9.99.8
2679000	00 249.6	154.3	0.62	-4	13	325.0	-13650	99.72	-	1.954 0.	029 (	0.186	0.002 (	.069	0.0763	0.0011	1101	30	1099	10	1097	8 99.8
2736000	00 270	152.4	0.56	-11	13	118.2	-5371	99.78	-	1.942 0.	025 (	).185	0.001 (	.179	0.0762	0.0010	1100	26	1095	6	1095	8 100.0
2776000	00 400	227.6	0.57	9	13	216.7	14798	99.88	1	1.950 0.	021 (	0.186	0.001 (	.386	0.0760	0.0007	1092	19	1099	~	1102	7 100.3
2801000	00 193.24	89.22	0.46	5	12	240.0	8470	99.72	-	1.967 0.	031 (	0.185	0.002 (	.372	0.0769	0.0011	1114	28	1104	11	1095	9 99.2
2767000	00 241.3	144.07	0.60	10	12	120.0	5308	99.79	-	1.950 0.	026 (	).186	0.001 (	0.287	0.0763	0.0010	1101	26	1101	6	1097	8 99.7
2754000	00 197.1	126.3	0.64	8	13	162.5	5394	99.79	1	1.948 0.	024 (	).186	0.002 (	.303	0.0761	0.0010	1096	26	1098	8	1097	9 100.0
2881000	00 204.86	102.77	0.50	ċ	15	300.0	-9038	99.73	-	1.950 0.	028 (	0.186	0.002 (	0.050	0.0759	0.0012	1092	31	1098	10	1098	9 100.0
3 2678000	00 122.1	42.27	0.35	9	П	183.3	4345	99.68	-	1.954 0.	036 (	0.187	0.002 (	0.148	0.0762	0.0015	1102	38	1100	13	1103	10 100.2
4 2945000	00 205.7	103.56	0.50	2	16	800.0	22880	99.73	-	1.957 0.	034 (	).185	0.002 (	0.164	0.0771	0.0014	1128	33	1100	12	1097	9 99.7
5 2779000	00 313.8	189	09.0	9	12	200.0	11420	99.83	-	1.940 0.	024 (	0.186	0.001	.442	0.0759	0.0008	1089	22	1095	8	1101	8 100.5
6 2647000	00 285.9	162.68	0.57	ŗ,	14	280.0	-12270	99.82	-	1.960 0.	022 (	0.187	0.002 (	.242	0.0759	6000.0	1093	25	1101	8	1105	9 100.3
7 2735000	00 211.5	135.02	0.64	7	14	200.0	6489	99.75	-	1.957 0.	031 (	).186	0.002 (	0.170	0.0762	0.0012	1102	30	1101	11	1098	8 99.7
8 2837000	00 230.9	83.8	0.36	-8	14	175.0	-6246	99.79	-	1.946 0.	025 (	0.185	0.001	.184	0.0763	0.0010	1099	27	1098	8	1094	8 99.7
e - 1 2557000	00 856	73.9	0.086	1	15	1500.0	52600.00	99.71	-	0.393 (	0.01 0.	0528 0	0004	.019	0.0531	0.0011	332	47	336.5	5.9	331.4	2.6 98.5
e - 10 2682000	00 901.4	95.26	0.106	13	12	92.3	4234.62	99.76	-	0.398 (	0.01 0.	0536 0	.0004 (	0.082	0.0536	0.0009	346	36	339.6	4.5	336.7	2.5 99.1
e - 2 2628000	00 627.3	65	0.104	5	14	280.0	7752.00	99.72	-	0.394 (	0.01 (	0.053 0	.0005 (	0.034	0.0537	0.001	352	43	336.9	5.1	333	2.8 98.8
e - 3 2586000	00 805	68.2	0.085	8	12	150.0	6050.00	99.81	-	0.389 (	0.01 0.	0538 0	.0005 (	0.35	0.0526	0.001	303	45	333	5.3	337.6	3 101
e - 4 2743000	00 605.7	56.71	0.094	2	14	700.0	18825.00	99.72	-	0.391 (	0.01 0.	0529 0	.0004 (	0.034	0.0535	0.0011	353	44	334.7	5.3	332	2.7 99.2
e - 5 2732000	00 896	100.57	0.112	ŗ,	12	240.0	-11154.00	99.78	-	0.393 (	0.01 0.	0532 0	.0004 (	.244	0.0534	0.0008	340	34	336.6	4.4	334.3	2.4 99.3
e - 6 2639000	00 585.2	51.42	0.088	9-	14	233.3	-5990.00	99.80	1	0.389 (	0.01 0.	0533 0	.0005 (	0.201	0.0527	0.0011	305	46	333.3	9	334.9	2.8 100
e - 7 2717000	00 689.8	64.09	0.093	8	12	150.0	5282.50	99.80	-	0.39 (	0.01 0.	0531 0	.0004 (	.142	0.0533	0.0008	340	34	334.3	4.4	333.7	2.5 99.8
2721000	00 2195.3	268.5	0.122	1	12	1200.0	136000.00	99.84	-	0.397	0 0.	0535 0	.0004 (	.184	0.0538	0.0006	368	23	339.4	3	336.2	2.3 99.1
e - 9 2730000	00 470.2	38.11	0.081	-12	11	91.7	-2392.50	99.72	-	0.393 (	0.01 (	0.053 0	.0005	.066	0.0537	0.0012	353	50	336.3	5.7	333.1	3 99
1148000	00 144	84.24	1.71	7	11	157.1	2873	99.55	-	1.945 0.	054 0.	1854 0	.0033 (	0.200	0.0751	0.0022	1062	57	1094	19	1096	18 94.7
1215000	00 134.2	86.64	1.55	10	12	120.0	2000	99.66	-	1.921 0.	056 0.	1867 0	.0032 (	0.272	0.0741	0.0022	1028	59	1085	19	1103	17 90.4
1222000	00 238.6	107.4	2.22	-5	11	-220.0	-7160	99.60	-	1.978 0.	048 0.	1859 0	.0029 (	0.257	0.0770	0.0019	1111	50	1106	17	1099	16 99.6
1275000	00 173	65.1	2.66	5	12	240.0	5186	99.57	-	1.961 0.	057 0.	1850 0	.0035 (	0.218	0.0772	0.0024	1113	61	1100	20	1094	19 98.4
1185000	00 362	243.5	1.49	~	11	157.1	7657	99.76	-	1.929 0.	044 0.	1850 0	.0028 (	.310	0.0756	0.0017	1078	47	1090	15	1094	15 98.0
1184000	00 204.1	95.3	2.14	8	11	137.5	3863	99.74	-	1.982 0.	052 0.	1885 0	.0030	.396	0.0761	0.0019	1086	52	1107	18	1113	16 96.5
1171000	00 348.9	195.1	1.79	ė	10	-333.3	-17090	99.70	-	1.963 0.	046 0.	1855 0	.0028 (	.406	0.0767	0.0017	1107	46	1102	16	1097	15 99.4
1141000	00 325.3	198	1.64	15	11	73.3	3106	99.72	-	1.975 0.	043 0.	1860 0	.0027 (	.367	0.0776	0.0017	1131	43	1108	14	1100	15 96.5
1128000	00 318.7	196.5	1.62	-20	11	-55.0	-2233	99.83	1	1.919 0.	047 0.	1854 0	.0029 (	.518	0.0753	0.0017	1069	47	1086	16	1096	16 97.1
0 1136000	00 283.8	178.1	1.59	-5	Π	-220.0	-8070	99.74	-	1.939 0.	044 0.	1856 0	.0027	0.285	0.0759	0.0018	1085	46	1094	15	1097	15 98.5
1 1133000	00 300.7	195.3	1.54	2	10	471.4	20424	99.83	-	1.941 0.	045 0.	1864 0	.0028 (	.378	0.0753	0.0017	1068	47	1094	16	1102	15 95.8
2 1118000	00 248.1	136.5	1.82	10	10	98.0	3466	99.67	-	1.957 0.	044 0.	1861 0	.0028 (	.199	0.0763	0.0018	1095	48	1100	15	1100	15 99.1
3 1146000	00 276.2	181.9	1.52	13	10	76.9	3068	99.70	-	1.963 0.	051 0.	1860 0	.0030	.473	0.0765	0.0019	1100	49	1101	17	1100	16 99.6
4 1122000	00 320.1	212.2	1.51	20	10	50.0	2250	99.66	-	1.956 0.	046 0.	1855 0	.0028 (	0.182	0.0770	0.0019	1113	49	1099	16	1097	15 98.2

Table A4. U-Pb geochronologic data for zircon reference materials analyzed at the University of New Brunswick.

			Me	asured	concen	tration	s					Ι	sotopic	ratios				Calcu	ılated ag	ges (Ma			I
Sample	⁹⁰ Zr (cps)	U (mqq)	Th (ppm)	Th/U	²⁰⁴ Pb (cps)	±2σ	% error	$^{206}{ m Pb/}_{ m 204}{ m Pb}^2$ %	Pb ³ C	4 ²⁰⁷ Pl	o/ ±2σ J	r ²⁰⁶ Pb/ ²³⁸ U	±2σ	β	²⁰⁷ Pb/ ²⁰⁶ Pb	±2σ	²⁰⁷ Pb/ ²⁰⁶ Pb	$\pm 2\sigma$	²⁰⁷ Pb/ ²³⁵ U	$\pm 2\sigma$	³⁶ Pb/	.2σ [%]	
FC-1 - 15	111500000	211.4	109	1.94	-1	11	-1100.0	-29670 9	99.6	1 1.94	48 0.04	7 0.1865	0.002	1310	0.0763	0.0020	1091	52	1096	16	1102	16 99	0.6
FC-1 - 16	109500000	207.2	128.9	1.61	-4	12	-300.0	-7075 9	9.59	1 1.95	53 0.05	1 0.1849	0.002	28 0.265	0.0769	0.0020	1106	53	1097	18	1094	15 99	9.0
FC-1 - 17	109800000	285.3	178.4	1.60	~	10	142.9	5654 9	9.76	1 1.95	59 0.04	2 0.1868	0.002	29 0.165	0.0758	0.0017	1082	47	1100	15	1104	16 97	2.0
FC-1 - 18	110900000	324	190.3	1.70	12	11	91.7	3760 9	9.80	1 1.94	49 0.04	4 0.1863	0.002	28 0.357	0.0755	0.0017	1075	45	1097	15	1101	15 96	5.5
FC-1 - 19	108400000	733.2	504.2	1.45	Ŋ	11	220.0	19760 9	9.83	1 1.95	50 0.03	9 0.1854	1 0.00	27 0.427	0.0762	0.0015	1096	40	1098	13	1096	15 99	9.6
Plesovice - 1	112300000	485	40.6	11.95	-4	11	-275.0	-4955 9	9.94	1 0.40	0.01	2 0.0554	0.00(	9 0.22(	0.0522	0.0016	279	68	344	6	348	5 101	1.2
Plesovice - 2	112200000	407.1	37.07	10.98	2	11	550.0	8125 9	9.78	1 0.40	0.01	4 0.0540	0.00(	9 0.223	0.0536	0.0019	332	75	341	10	339	5 99	9.4
Plesovice - 3	118200000	393.8	31.31	12.58	9	Π	183.3	2690 9	9.85	1 0.37	79 0.01	4 0.0518	0.00(	9 0.128	0.0533	0.0020	321	81	326	10	326	5 100	0.0
Plesovice - 4	110800000	909.7	6.99	9.11	ċ	11	-220.0	-7284 9	9.80	1 0.39	91 0.01	0 0.0535	0.00(	8 0.085	0.0532	0.0014	325	58	335	4	336	5 100	0.2
Plesovice - 5	107100000	505.8	44.29	11.42	-12	12	-100.0	-1643 9	9.78	1 0.40	0.01	3 0.0541	0.000	8 0.177	0.0540	0.0018	352	71	342	6	339	5 99	9.3
Plesovice - 6	111900000	376.3	30.01	12.54	6	Ξ	122.2	1654 9	06.6	1 0.39	95 0.01	6 0.0542	0.000	9 0.161	0.0530	0.0021	306	84	337	12	340	6 100	6.0
Plesovice - 7	106100000	842.9	88.8	9.49	14	12	85.7	2343 9	9.74	1 0.40	3 0.01	0 0.0542	0.000	8 0.178	0.0537	0.0014	346	60	343	8	341	5 99	9.2
Plesovice - 8	104100000	706.6	67.2	10.51	8	12	150.0	3370 9	9.78	1 0.39	95 0.01	2 0.0541	0.00	9 0.295	0.0535	0.0016	332	99	339	6	340	6 100	0.2
Plesovice - 9	107400000	652.6	59.51	10.97	4	11	275.0	6335 9	9.92	1 0.39	95 0.01	2 0.0544	0.00	9 0.148	0.0528	0.0017	304	69	337	6	342	5 101	l.4
Plesovice - 10	115200000	869.6	131.3	6.62	11	16	145.5	3095 9	9.72	1 0.40	0.01	8 0.0538	0.001	0 0.054	0.0546	0.0026	371	110	344	13	338	6 98	3.2
Plesovice - 11	117200000	647.7	59.9	10.81	9	13	216.7	4253 9	9.95	1 0.35	3 0.01	6 0.0545	0.00	0 0.146	0.0524	0.0021	290	88	336	12	342	6 101	8.I
FC-1 - 1	172400000	229.7	136.5	1.683	7.8	9.3	119.2	4655.13 9	69.6	1 1.95	57 0.0	6 0.186	0.00	0.283	0.0761	0.0013	1089	34	1099	21 1	8.660	38 98	3.2
FC-1 - 2	173600000	217.8	100.7	2.163	6.6	8.3	125.8	5381.82 9	9.72	1 1.93	33 0.0	6 0.1856	0.00	0.272	0.076	0.0015	1082	41	1090	22 1	097.1	38 98	3.4
FC-1 - 4	164700000	694	328	2.116	0.6	9.4	1566.7	189666.67 9	9.81	1 1.96	55 0.0	6 0.1863	0.006	9 0.47¢	0.0764	0.0008	1102	21	1102.9	19 1	101.2	38 99	9.8
FC-1 - 5	165700000	469.9	282.6	1.663	2.9	8.9	306.9	26068.97 9	9.86	1 1.93	35 0.0	6 0.1857	0.006	9 0.48¢	0.0759	0.0009	1087	24 ]	1092.4	20 1	097.8	37 99	9.1
FC-1 - 6	166000000	270.9	151.8	1.785	2.5	9.1	364.0	17420.00 9	9.76	1 1.95	58 0.0	6 0.1858	3 0.00	9 0.375	0.0766	0.0011	1104	28	1100	20 1	098.3	38 99	9.6
FC-1 - 7	164700000	333.6	192.9	1.729	6.1	9.8	160.7	8814.75 9	9.77	1 1.95	52 0.0	6 0.1863	3 0.00	9 0.189	0.0754	0.0011	1071	31	1098	20 1	101.3	38 95	2.7
FC-1 - 8	162100000	327.9	144.2	2.274	-1.4	7.2	-514.3	-36500.00 9	9.74	1 1.95	51 0.0	6 0.1855	0.006	59 0.23E	0.0764	0.0011	1101	28 ]	1099.2	21 1	096.9	38 99	9.7
FC-1 - 9	160500000	201.7	102.15	1.975	-	10	1000.0	31230.00 9	9.70	1 1.9	95 0.0	6 0.1861	0.00	0.281	0.0762	0.0015	1088	40	1096	22 1	100.1	38 98	8.4
FC-1 - 10	158700000	346	214.6	1.612	4.1	9.1	222.0	12948.78 9	9.77	1 1.95	59 0.0	6 0.186	900.0	9 0.44 ²	0.0764	0.0011	1100	30	1100	20 1	099.5	38 99	9.8
FC-1 - 11	157400000	348.6	217	1.606	8.3	8.8	106.0	6383.13 9	9.78	1 1.94	44 0.0	6 0.1856	0.006	9 0.447	0.0761	0.0011	1092	29	1095	21 1	097.3	38 99	9.3
FC-1 - 12	159300000	147.7	110.2	1.34	5.3	9.5	179.2	4369.81 9	9.71	1 1.96	55 0.0	7 0.1868	0.00	71 0.306	0.0759	0.0015	1082	40	1104	22	1104	38 96	5.7
FC-1 - 13	155600000	387	240	1.613	10	10	100.0	5750.00 9	9.74	1 1.94	46 0.0	6 0.1853	900.0	9 0.23 ⁵	0.0762	0.0011	1095	29	1096.1	20	095.7	38 99	9.7
FC-1 - 14	158400000	326.4	203.5	1.604	5.7	8.4	147.4	8954.39 9	9.81	1 1.95	56 0.0	6 0.1863	3 0.006	01.0 69	0.0757	0.0012	1087	29	1099.5	19 1	101.4	38 9	98
FC-1 - 15	155700000	251	124.5	2.016	12.3	9.5	77.2	3126.83 9	9.73	1 1.94	49 0.0	6 0.1856	0.006	9 0.16 <del>0</del>	0.0762	0.0013	1094	33	1097	20 1	097.6	38 99	9.4
FC-1 - 16	158300000	281.3	155.1	1.814	5.5	9.1	165.5	8090.91 9	9.70	1 1.95	52 0.0	6 0.1858	0.006	9 0.20 <u>0</u>	0.076	0.0012	1090	31	1098	21 1	098.7	38 98	3.6
FC-1 - 17	155900000	262.1	148.3	1.767	11	11	100.0	3717.27 9	9.78	1 1.96	66 0.0	6 0.1867	0.00	0.274	0.0758	0.0013	1086	34	1105	20 1	103.1	38 97	7.3
FC-1 - 18	152900000	386.5	210.7	1.834	6.7	9.1	135.8	8552.24 9	9.76	1 1.93	35 0.0	6 0.1848	3 0.00	0.442	0.0769	0.0011	1113	29	1092	20 1	092.8	38 97	7.1
FC-1 - 19	157700000	268	162.8	1.646	8	8.7	108.8	5262.50 9	9.75	1 1.95	59 0.0	6 0.1864	1 0.00	0.248	8 0.0763	0.0011	1096	29	1100.6	20 1	101.9	38 99	9.2
FC-1 - 20	154700000	175.4	85.6	2.049	5.8	7.8	134.5	4641.38 9	69.6	1 1.94	49 0.0	6 0.1857	0.00	0.276	0.0756	0.0014	1074	37	1099	21 1	097.9	38 96	5.3
Plesovice - 1	172700000	730.8	68.2	10.72	18.3	9.8	53.6	1814.75 9	9.84	1 0.35	37 0.0	1 0.0531	0.00	0.01	0.0528	0.0013	304	53	331.7	9.8	333.4	12 10	01
Plesovice - 1	177600000	730.3	68.1	10.72	19	11	57.9	1789.47 9	9.85	1 0.35	35 0.0	1 0.0531	0.00	0.022	0.0526	0.0014	295	58	330.5	10	333.3	12 10	01

		Меа	sured c	oncentr	ations							Isoto	pic ratios					Calcula	ted ages	(Ma)		
s) U Th $Th^{2W}Pb$ $\pm 2\sigma$ % error (ppm) (ppm) (cps)	$ \begin{array}{cc} Th & Th \\ (ppm) & Th/U & {}^{204}Pb & \pm 2\sigma & \% \ error \\ (cps) & \\ \end{array} $	Th/U ²⁰⁴ Pb ±2σ % error (cps)	⁰⁴ Pb ±2σ % errot (cps)	2σ % erroi	erroi		²⁰⁶ Pb/ %	Pb ³ C	,4 ²⁰⁷ ]	Pb/ ±2 ⁵ U	206 231 231	Pb/8U	2σ β	207	Pb/ ± Pb 4	2σ ²¹	⁰⁷ Pb/ ±	2σ ²⁰⁷ I 235	Pb/ ±2 ⁵U	206 23	Pb/ ±2 ⁸ U	8 8 6
00 604.5 54.1 11.17 7.1 9 126.	54.1 11.17 7.1 9 126.	11.17 7.1 9 126.	7.1 9 126.	9 126.	126.8	~	3921.13 9	9.71	1 0.4	403 0.	.02 0.0	)539 (	0.002 0.0	0.0	545 0.	0015	373	59 34	43.4	11 3	38.2	2 98
000 604.5 54.1 11.17 7 11 157.1	54.1 11.17 7 11 157.1	11.17 7 11 157.1	7 11 157.1	11 157.1	157.1		4150.00 9	9.81	1 0.5	398 0.	02 0	.054 (	0.002 0.0	0.0 88	537 0.	0016	340	65 33	39.6		339	2 99.
000 61//9 54.16 11.41 15 12 80.0 000 619 54.41 11.38 13 11 84.6	54.16 11.41 15 12 80.0 54.41 11.38 13 11 84.6	11.41 15 12 80.0 11.38 13 11 846	15 12 80.0 13 11 846	12 80.0 11 84.6	80.0 84.6		9 73.61 54 9	9.92 9.90	1 0.	383 0. 382 0.	0.0 10.0	)529 (	0.002 0.0	82 0.0	1525 0. 1526 0	0011	300	53 55 47 32	28.4 28.3 0	10 10 10 10	32.3	2 10
00 665.7 59.31 11.22 3.2 9.1 284.4	59.31 11.22 3.2 9.1 284.4	11.22 3.2 9.1 284.4	3.2 9.1 284.4	9.1 284.4	284.4		9575.00 9	9.78	1 0.5	376 0.0	01 0.0	0.213 0.	0019 0.0	82 0.0	531 0.	0013	317	52 32	23.3 9	.6 3	22.3	2 99.
00 665.7 59.3 11.23 3.3 9 272.7	59.3 11.23 3.3 9 272.7	11.23 3.3 9 272.7	3.3 9 272.7	9 272.7	272.7		9287.88 9	9.76	1 0.3	375 0.	0.0 0.0	0.513 0.	0019	0.1 0	.053 0.	0013	314	52 32	23.1 9	.6 3	22.4	2 99.
00 585 51 11.47 4.5 9.8 217.8	51 11.47 4.5 9.8 217.8	11.47 4.5 9.8 217.8	4.5 9.8 217.8	9.8 217.8	217.8		6044.44 9	9.81	1 0.2	392 0.	0.0 0.0	)532 (	0.002 0.2	36 0.0	536 0.	0014	342	56 33	35.3	11 3	34.2	2 99.
00 587 51.3 11.44 10.5 9.4 89.5	51.3 11.44 10.5 9.4 89.5	11.44 10.5 9.4 89.5	10.5 9.4 89.5	9.4 89.5	89.5		2571.43 9.	9.76	1 0.5	393 0.	.01 0.0	)529 (	0.002 0.1	.65 0.0	541 0.	0013	360	51 33	36.1	10 3	32.3	2 98.
00 559 48.7 11.48 8 10 125.0	48.7 11.48 8 10 125.0	11.48 8 10 125.0	8 10 125.0	10 125.0	125.0		3161.25 9	9.85	1 0	.39 0.	.01 0.0	)536 (	0.002 0.3	38 0	.053 0.	0013	314	54 33	33.8	10 3	36.4	2 10
00 559 48.7 11.48 8 10 125.0	48.7 11.48 8 10 125.0	11.48 8 10 125.0	8 10 125.0	10 125.0	125.0		3161.25 9	9.85	1 0	.39 0.	.01 0.0	)536 (	0.002 0.3	38 0	.053 0.	0013	314	54 33	33.8	10 3	36.4	2 10
00 613.4 52.96 11.58 6.7 9 134.3	52.96 11.58 6.7 9 134.3	11.58 6.7 9 134.3	6.7 9 134.3	9 134.3	134.3		4153.73 9.	9.65	1 0.	397 0.	.01 0.0	0.525 0.	0019 0.0	946 0.0	544 0.	0014	367	57 33	38.8	10 3	29.8	2 97.
00 613.6 52.93 11.59 11 11 100.0	52.93 11.59 11 11 100.0	11.59 11 11 100.0	11 11 100.0	11 100.0	100.0		2634.55 9	9.66	1 0.	394 0.	.02 0.0	)526 (	0.002 0	.08 0	054 0.	0016	350	65 33	36.7	11 3	30.2	2 98.
00 658.4 59.57 11.05 0.1 9.5 9500.0	59.57 11.05 0.1 9.5 9500.0	11.05 0.1 9.5 9500.0	0.1 9.5 9500.0	9.5 9500.0	9500.0		293600.00 9	9.81	1 0.2	391 0.	.01 0.0	)533 (	0.002 0.0	17 0.0	534 0.	0014	327	56 33	34.4	10 3	34.5	2 10
00 658.4 59.57 11.05 0.1 9.5 9500.0	59.57 11.05 0.1 9.5 9500.0	11.05 0.1 9.5 9500.0	0.1 9.5 9500.0	9.5 9500.0	9500.0		293600.00 9	9.81	1 0.3	391 0.	.01 0.0	)533 (	0.002 0.0	0.0	534 0.	0014	327	56 33	34.4	10 3	34.5	2 10
00 791.8 77.53 10.21 1.4 9.2 657.1	77.53 10.21 1.4 9.2 657.1	10.21 1.4 9.2 657.1	1.4 9.2 657.1	9.2 657.1	657.1		25464.29 9	9.91	1 0.5	386 0.	0.0 0.0	)534 (	0.002 0.1	25 0.0	525 0.	0011	295	46 33	30.7 5	.4 3	35.2	2 10
00 791.8 77.53 10.21 1.4 9.2 657.1	77.53 10.21 1.4 9.2 657.1	10.21 1.4 9.2 657.1	1.4 9.2 657.1	9.2 657.1	657.1		25464.29 9	9.91	1 0.2	386 0.	.01 0.0	)534 (	0.002 0.1	25 0.0	525 0.	0011	295	46 33	30.7 5	.4 3	35.2	2 10
00 1185.1 159.2 7.444 11.4 9.3 81.6	159.2 7.444 11.4 9.3 81.6	7.444 11.4 9.3 81.6	11.4 9.3 81.6	9.3 81.6	81.6		4631.58 9	9.81	1 0.	391 0.	0.0 0.0	)533 (	0.002 0.1	38 0.0	533 0.	6000	333	38 33	34.5 8	3.8 3	34.6	2 10
00 1185.1 159.2 7.444 11.4 9.3 81.6	159.2 7.444 11.4 9.3 81.6	7.444 11.4 9.3 81.6	11.4 9.3 81.6	9.3 81.6	81.6		4631.58 9	9.81	1 0.2	391 0.	.01 0.0	)533 (	0.002 0.7	38 0.0	533 0.	6000	333	38 33	34.5 8	3.8 3	34.6	2 10
00 618.1 53.99 11.45 3.2 8.6 268.8	53.99 11.45 3.2 8.6 268.8	11.45 3.2 8.6 268.8	3.2 8.6 268.8	8.6 268.8	268.8		8459.38 9	9.81	1 0.2	391 0.	.01 0.0	)531 (	0.002 0.3	149 0.0	535 0.	0013	333	54 33	34.8	10 3	33.8	2 99.
00 618.1 53.99 11.45 3.2 8.6 268.8	53.99 11.45 3.2 8.6 268.8	11.45 3.2 8.6 268.8	3.2 8.6 268.8	8.6 268.8	268.8		8459.38 9	9.81	1 0.	391 0.	0.0 0.0	)531 (	0.002 0.1	49 0.0	535 0.	0013	333	54 33	34.8	10 3	33.8	2 99.
00 747.9 71.37 10.48 0.6 9.9 1650.0	71.37 10.48 0.6 9.9 1650.0	10.48 0.6 9.9 1650.0	0.6 9.9 1650.0	9.9 1650.0	1650.0		55316.67 9	9.73	1 0	.39 0.	.01 0.0	0.523 0.	0019 0.1	94 0.0	535 0.	0011	337	47 33	33.6 9	.5 3	28.6	2 98.
00 748.6 71.46 10.48 -3 12 -400.0	71.46 10.48 -3 12 -400.0	10.48 -3 12 -400.0	-3 12 -400.0	12 -400.0	-400.0		-11450.00 9	9.73	1 0.	389 0.	.02 0.0	0524 (	0.002 0.1	0.0	535 0.	0014	334	59 33	33.5	11 3	29.5	2 98.
00 473.6 38.91 12.17 15.6 9.9 63.5	38.91 12.17 15.6 9.9 63.5	12.17 15.6 9.9 63.5	15.6 9.9 63.5	9.9 63.5	63.5		1328.21 9	9.93	1 0.	392 0.	.02 0	.054 (	0.002 0.1	08 0.0	528 0.	0015	301	62 33	35.3	11 3	39.2	2 10
00 473.6 38.93 12.17 15.8 9.5 60.1	38.93 12.17 15.8 9.5 60.1	12.17 15.8 9.5 60.1	15.8 9.5 60.1	9.5 60.1	60.1		1312.66 9	9.93	1 0.	392 0.	.02 0	.054 (	0.002 0.1	26 0.0	528 0.	0015	303	61 33	35.2	11 3	38.9	2 10
00 412.2 37.35 11.04 7 13 185.7	37.35 11.04 7 13 185.7	11.04 7 13 185.7	7 13 185.7	13 185.7	185.7		2681.43 9	9.71	1 0.	395 0.	.02 0.0	0527 (	0.002 0.1	54 0.0	543 0.	0022	364	87	337	13 3	31.2	2 98.
00 412.2 37.29 11.05 8.7 9.1 104.6	37.29 11.05 8.7 9.1 104.6	11.05 8.7 9.1 104.6	8.7 9.1 104.6	9.1 104.6	104.6		2086.21 9	9.57	1 0.4	403 0.	.02 0.0	0527 (	0.002 0.0	93 0.0	554 0.	0017	404	66 34	42.9	11 3	30.9	2 96.
00 610.3 54.76 11.14 17.1 8.4 49.1	54.76 11.14 17.1 8.4 49.1	11.14 17.1 8.4 49.1	17.1 8.4 49.1	8.4 49.1	49.1		1560.23 9	9.82	1 0.	388 0.	01 0	.053 (	0.002 0.2	.47 0.0	532 0.	0012	321	49 33	32.3 9	9.8 3	33.1	2 10
00 610.3 54.76 11.14 17.1 8.4 49.1	54.76 11.14 17.1 8.4 49.1	11.14 17.1 8.4 49.1	17.1 8.4 49.1	8.4 49.1	49.1		1560.23 9	9.82	1 0.	388 0.	.01 0	.053 (	0.002 0.2	.47 0.0	532 0.	0012	321	49 33	32.3 9	9.8 3	33.1	2 10
00 612.7 55.4 11.06 6.4 9.2 143.8	55.4 11.06 6.4 9.2 143.8	11.06 6.4 9.2 143.8	6.4 9.2 143.8	9.2 143.8	143.8		4201.56 9	9.71	1 0.	395 0.	.02 0.0	0529 (	0.002 0.2	61 0	.054 0.	0014	352	55 33	37.6	11 3	32.4	2 98.
00 612.7 55.4 11.06 6.4 9.2 143.8	55.4 11.06 6.4 9.2 143.8	11.06 6.4 9.2 143.8	6.4 9.2 143.8	9.2 143.8	143.8		4201.56 9	9.71	1 0.	395 0.	.02 0.0	)529 (	0.002 0.2	61 0	.054 0.	0014	352	55 33	37.6	11 3	32.4	2 98.
00 972.6 105.7 9.202 7.2 8.9 123.6	105.7 9.202 7.2 8.9 123.6	9.202 7.2 8.9 123.6	7.2 8.9 123.6	8.9 123.6	123.6		6025.00 9	9.75	1 0.2	393 0.	0.0 0.0	)532 (	0.002 0.1	74 0.0	533 (	.001	329	44 33	36.3 9	.3 3	33.9	2 99.
00 972.6 105.7 9.202 7.2 8.9 123.6	105.7 9.202 7.2 8.9 123.6	9.202 7.2 8.9 123.6	7.2 8.9 123.6	8.9 123.6	123.6		6025.00 9	9.75	1 0.3	393 0.	0.0 0.0	)532 (	0.002 0.1	74 0.0	533	001	329	44 33	36.3 9	.3 3	33.9	2 99.
00 518.7 43.51 11.92 7.9 8.2 103.8	43.51 11.92 7.9 8.2 103.8	11.92 7.9 8.2 103.8	7.9 8.2 103.8	8.2 103.8	103.8		2849.37 9	9.85	1 0.3	395 0.	.02 0.0	0.248 0.	0021 0.2	21 0.0	531 0.	0014	317	59 33	37.2	11 3	44.1	3 10
00 518.7 43.51 11.92 9 10 111.1	43.51 11.92 9 10 111.1	11.92 9 10 111.1	9 10 111.1	10 111.1	111.1		2608.89 9	9.81	1 0.3	397 0.	.02 0.0	0.246 0.	0021 0	.27 0.0	537 0.	0017	342	69 33	38.6	12 3	42.5	3 10
00 412.1 33.25 12.39 8 10 125.0	33.25 12.39 8 10 125.0	12.39 8 10 125.0	8 10 125.0	10 125.0	125.0		2281.25 ##	###	1 0.5	379 0.	.02 0.0	)538 (	0.002 0.1	14 0.0	513 0.	0016	242	66 32	25.9	11 3	37.5	2 10
00 412.1 33.25 12.39 9 9.1 101.1	33.25 12.39 9 9.1 101.1	12.39 9 9.1 101.1	9 9.1 101.1	9.1 101.1	101.1		1988.89 ##	###	1 0.5	381 0.	.02 0.0	)537 (	0.002 0.0	94 0.0	515 0.	0015	250	62 32	26.8	11 3	37.2	2 10
00 676 62.46 10.82 0.1 7.7 7700.0	62.46 10.82 0.1 7.7 7700.0	10.82 0.1 7.7 7700.0	0.1 7.7 7700.0	7.7 7700.0	7700.0		288900.00 9	9.90	1 0	.38 0.	0.0 0.0	)524 (	0.002 0.0	0.04 0.0	525 0.	0012	292	52 32	26.7 9	9.6 3	29.1	2 10
00 676.3 62.48 10.82 0.9 8.3 922.2	62.48 10.82 0.9 8.3 922.2	10.82 0.9 8.3 922.2	0.9 8.3 922.2	8.3 922.2	922.2		32466.67 9.	9.89	1 0.	378 0.	.01 0.0	0.01	0019 0.0	81 0.0	524 0.	0014	291	57	325	10 3	27.5	2 10

			Meá	sured (	concen	tration	s						Isotopic	ratios				Cai	lculated	ages (N	[a)		
Sample	⁹⁰ Zr (cps)	U U	Th (ppm)	Th/U	²⁰⁴ Pb (cps)	±2σ	% error	²⁰⁶ Pb/ ²⁰⁴ Pb ²	%Pb ³ C	,4 207 23	⁵ Pb/ ±24	σ ²⁰⁶ Pb/ ²³⁸ U	, ±2σ	θ	²⁰⁷ Pb. ²⁰⁶ Pb	/ ±2σ	²⁰⁷ Pł ²⁰⁶ Pł	o/ ±2σ >	²⁰⁷ Pb/ ²³⁵ U	±2σ	²⁰⁶ Pb/ ²³⁸ U	±2σ	%
FC-1 - 2	178400000	4.483	2.003	2.24	0	10	-4800.0	32790	99.59	1	.965 0.05	54 0.180	6 0.0	0.01	0 0.077	1 0.001;	111	8 45	1102	18	1100	16	97.9
FC-1 - 3	171900000	7.397	3.232	2.29	0	10	n.d.	53200	99.75	1 1.	.948 0.0	50 0.18	6 0.0	<b>J</b> 3 0.32	9 0.075	0.001	3 105	32	1096	17	1100	15	97.9
FC-1 - 4	167500000	8.475	4.63	1.83	ċ	6	-193.6	60100	99.74		.977 0.0	47 0.18	6 0.0	<b>)3 0.32</b>	5 0.076	7 0.0010	) 11(	18 27	1107	16	1101	15	9.96
FC-1 - 5	176400000	7.253	4.377	1.66	0	12	n.d.	52590	99.86	1	.920 0.0	47 0.18.	5 0.0	03 0.43	4 0.075	7 0.001.	1 108	32 29	1087	, 16	1091	16	99.1
FC-1 - 6	177500000	3.386	1.572	2.15	۲-	11	-157.1	24700	69.66	1	.920 0.00	60 0.18	7 0.0	0.17	4 0.075	3 0.0020	) 106	51 54	1086	5 21	1102	19	95.8
FC-1 - 7	165300000	6.101	3.499	1.74	9	Ξ	183.3	7118	99.75	1 1	.948 0.0	48 0.18t	6 0.0	<b>33 0.25</b>	1 0.075	4 0.001	1 107	76 32	1096	17	1099	16	96.7
FC-1 - 8	179600000	10.06	6.01	1.67	15	15	100.0	4926	99.83	1	.971 0.04	48 0.188	8 0.0	<b>33 0.30</b>	0 0.076	6 0.001:	3 11(	9 33	1105	17	1109	17	99.5
FC-1 - 10	159800000	4.329	1.805	2.40	ċ	10	-200.0	28890	99.60	1	.948 0.05	55 0.18:	5 0.0	33 0.24	9 0.076	2 0.0016	\$ 105	39 42	1095	19	1093	16	98.7
FC-1 - 12	162500000	2.998	1.302	2.30	Ŋ	10	200.0	4014	99.57	1 1.	931 0.0	59 0.18:	3 0.01	33 0.22	7 0.076	5 0.0013	7 105	3 46	1089	20	1085	17	8.66
FC-1 - 13	154700000	8.257	5.192	1.59	З	10	396.0	21836	99.71		.973 0.0	50 0.188	8 0.01	33 0.11	9 0.076	3 0.001:	3 105	14 34	1105	17	1109	16	98.2
FC-1 - 14	149400000	5.299	3.247	1.63	3	10	293.9	10273	99.63	1	.954 0.05	55 0.18	7 0.0	<b>33 0.09</b>	5 0.076	1 0.001	7 105	33 45	1097	7 19	1103	17	97.5
FC-1 - 15	150200000	3.489	1.752	1.99	4	12	300.0	5648	99.55	1 1.	.982 0.0	70 0.18:	5 0.0	0.13	8 0.077	2 0.002	111	6 60	1106	24	1096	19	0.66
FC-1 - 16	146400000	11.28	7.37	1.53	-2	6	-430.0	70100	99.83		.932 0.04	45 0.18:	5 0.0	33 0.45	2 0.075	7 0.0010	301 (	33 26	1093	15	1095	16	98.6
FC-1 - 17	147300000	6.98	3.56	1.96	2	10	500.0	22500	99.73	1	.965 0.04	48 0.18	7 0.0	<b>J</b> 3 0.38	2 0.076	7 0.0012	3 110	7 31	1104	17	1105	17	99.5
FC-1 - 18	132700000	6.06	2.841	2.13	8	13	162.5	4529	99.64		.946 0.06	66 0.18	4 0.0	0.13 0.13	9 0.075	6 0.0022	2 107	75 56	1095	22	1090	18	9.6
FC-1 - 19	149000000	2.762	1.022	2.70	2	10	633.3	11847	99.40	1	.953 0.06	65 0.18	4 0.0	33 0.12	9 0.077	0 0.0022	2 105	9 57	1096	22	1089	18	6.66
FC-1 - 20	146000000	5.356	3.211	1.67	-2	11	-550.0	34300	99.71		970 0.0	52 0.188	8 0.0	<b>33 0.39</b>	0 0.076	3 0.001	105	36 36	1105	19	1108	16	98.2
FC-1 - 21	148700000	2.796	1.108	2.52	-3	10	-306.3	17890	99.59	1 1	.927 0.00	61 0.18:	5 0.0	03 0.23	9 0.075	4 0.002	) 106	57 50	1087	21	1094	18	96.4
Plesovice - 1	167900000	23.35	1.955	11.94	7	13	185.7	6687	99.81	1 0.	399 0.0	11 0.05	4 0.00	0.52	3 0.053	6 0.001(	) 34	12 41	340	8	340	ŝ	6.66
Plesovice - 2	157500000	31.53	3.043	10.36	19	11	57.9	3175	99.28	1 0.	434 0.0	11 0.05	4 0.0	0.18 0.18	7 0.058	3 0.001	\$ 52	7 48	366	8	338	ŝ	92.5
Plesovice - 3	159400000	17.738	1.775	9.99	2	11	550.0	17270	96.66	1 0.	389 0.0	13 0.05-	4 0.0	01 0.15	7 0.052	1 0.001;	5 27	72 63	333	10	339	5 1(	91.9
Plesovice - 4	157200000	21.165	1.776	11.92	5	10	190.4	7856	99.95	1 0.	.387 0.0	11 0.05-	4 0.0	01 0.11	3 0.052	0 0.001.	2.7	73 49	333	8	338	5 1(	21.7
Plesovice - 5	156400000	18.53	1.499	12.36	1	П	1100.0	35120	99.88	1 0.	.396 0.0	12 0.05-	4 0.0	01 0.20	5 0.053	0 0.001	31	4 54	338	6	339	5 1(	00.1
Plesovice - 6	152500000	40.55	4.885	8.30	15	12	80.0	4975	99.27	1 0.	437 0.0	12 0.05-	4 0.0	01 0.69	2 0.058	6 0.000	\$ 54	17 29	367	8	338	ŝ	91.9
Plesovice - 7	152300000	16.72	1.574	10.62	-4	10	-264.9	30780	99.79	1 0.	.397 0.0	13 0.05-	4 0.0	01 0.37	8 0.053	5 0.001	32	37 51	339	6	337	ŝ	9.66
Plesovice - 8	150400000	17.78	1.736	10.24	4	12	300.0	8128	17.66	1 0.	404 0.0	13 0.05-	4 0.0	01 0.36	0 0.054	5 0.001	37	76 53	344	6	337	ŝ	98.1
Plesovice - 9	148900000	27.41	2.476	11.07	-4	6	-230.0	50200	99.84	1 0.	.393 0.0	11 0.05-	4 0.0	01 0.38	1 0.052	8 0.0010	) 31	9 44	337	8	338	5 1(	00.3
Plesovice - 10	142700000	19.28	2.133	9.04	9	6	143.8	5352	99.79	1 0.	.397 0.0	11 0.05-	4 0.0	01 0.32	9 0.053	6 0.001.	1 34	10 45	339	8	338	9	6.66
Plesovice - 11	139100000	21.34	1.858	11.49	-5	11	-220.0	36520	99.75	1 0.	396 0.0	12 0.05	3 0.0	01 0.30	3 0.053	9 0.001	35	55 49	338	6	335	ŝ	98.9
Plesovice - 12	140600000	15.95	1.321	12.07	-2	10	-500.0	27530	99.75	1 0.	.393 0.0	12 0.05.	3 0.0	01 0.29	0 0.053	7 0.001.	33	<b>39 55</b>	336	6	333	ŝ	99.2
Plesovice - 13	150900000	12.491	1.012	12.34	-	12	-1200.0	23180	99.92	1 0.	389 0.0	14 0.05-	4 0.0	01 0.47	3 0.052	5 0.001:	5 25	6 61	335	Ξ	341	6 1(	01.8
Plesovice - 14	140600000	16.91	1.636	10.34	10	10	100.0	2953	99.86	1 0.	.398 0.0	13 0.05-	4 0.0	01 0.38	8 0.053	3 0.001	32	38 52	339	6	339	ŝ	8.66
Plesovice - 15	13940000	9.581	0.776	12.35	4	6	244.4	4544	99.67	1 0.	400 0.0	15 0.05.	3 0.0	01 0.26	9 0.054	3 0.001	7 35	56 68	341	Ξ	335	9	98.2
¹ after Hg corr	ection																						1
$\frac{1}{2}$ in counts per	second																						

